CleanAir Engineering 500 W. Wood Street Palatine, IL 60067-4975 cleanair.com



Air Products and Chemicals, Inc. 7201 Hamilton Boulevard Allentown, Pennsylvania 18195 AIR QUALITY DIV.

REPORT ON MEASUREMENT SERVICES

Performed for: AIR PRODUCTS AND CHEMICALS, INC. DETROIT HYDROGEN PLANT

HYDROGEN PLANT HEATER STACK

Client Reference No: 4503676698 CleanAir Project No: 12915 Revision 0: April 28, 2016

To the best of our knowledge, the data presented in this report are accurate, complete, error free and representative of the actual emissions during the test program. Clean Air Engineering operates in conformance with the requirements of ASTM D7036-04 Standard Practice for Competence of Air Emission Testing Bodies.

Submitted by,

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AIR PRODUCTS AND CHEMICALS, INC. DETROIT HYDROGEN PLANT

Client Reference No: 4503676698 CleanAir Project No: 12915

REVISION HISTORY

REPORT ON MEASUREMENT SERVICES

DRAFT REPORT REVISION HISTORY

| Revision: | Date | Pages | Comments |
|-----------|----------|-------|-------------------------------------|
| D0a | 04/21/16 | All | Draft version of original document. |
| | | | |
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FINAL REPORT REVISION HISTORY

| Revision: | Date | Pages | Comments |
|-----------|----------|--|-------------------------------------|
| 0 | 04/28/16 | All | Final version of original document. |
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PROJECT OVERVIEW

INTRODUCTION

Air Products and Chemicals, Inc. (Air Products) contracted Clean Air Engineering (CleanAir) to perform emission compliance measurements at the Detroit Hydrogen

CleanAir) to permit Plant in Detroit, Michigan. All testing was conducted in accordance with the regulations see ... States Environmental Protection Agency (USEPA) and the Michigan Department Environmental Quality (DEQ). The permit limits are referenced in Michigan Department of Environmental Quality, Air Quality Division Permit to Install No. 63-08D, issued May 12, 2014.

- S. Young Air Products and Chemicals, Inc.

M. Dziadosz – DEQ

A. Obuchowski - CleanAir

M. Cendana – CleanAir

Test Program Parameters

The testing was performed at the Hydrogen (H_2) Plant Heater Stack on March 15 through 18, 2016, and included the following emissions measurements:

- particulate matter (PM), assumed equivalent to filterable particulate matter (FPM) only
- total particulate matter less than 10 microns (μ m) in diameter (Total PM₁₀), • assumed equivalent to the sum of the following constituents:
 - FPM о
 - condensable particulate matter (CPM) o
- sulfuric acid (H_2SO_4)
- volatile organic compounds (VOC), assumed equivalent to total hydrocarbons (THC) minus the following constituents:
 - methane (CH₄) 0
 - ethane (C_2H_6)
- nitrogen oxides (NO_X)
- carbon monoxide (CO) •
- flue gas composition (e.g., O₂, CO₂, H₂O)
- flue gas flow rate (Q_a)

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PROJECT OVERVIEW

TEST PROGRAM SYNOPSIS

Test Schedule

The on-site schedule followed during the test program is outlined in Table 1-1.

| | Table 1-1: Schedule of Activities | | | | | | | | | |
|---------------|--------------------------------------|------------------------|------------------------|----------|---------------|-------------|--|--|--|--|
| Run Number | Location | Method | Analyte | Date | Start Time | End Time | | | | |
| 1 | H ₂ Plant Heater Stack | USEPA Method 25A/18 | VOC | 03/15/16 | 15:01 | 16:01 | | | | |
| 2 | H ₂ Plant Heater Stack | USEPA Method 25A/18 | VOC | 03/15/16 | 16:11 | 17:11 | | | | |
| 3 | H ₂ Plant Heater Stack | USEPA Method 25A/18 | VOC | 03/16/16 | 08:39 | 10:14 | | | | |
| 4 | H ₂ Plant Heater Stack | USEPA Method 25A/18 | VOC | 03/16/16 | 10:27 | 11:27 | | | | |
| 1 | H ₂ Plant Heater Stack | USEPA Method 5/202 | FPM/CPM | 03/15/16 | 15:18 | 17:28 | | | | |
| 2 | H ₂ Plant Heater Stack | USEPA Method 5/202 | FPM/CPM | 03/16/16 | 09:37 | 12:28 | | | | |
| 3 | H ₂ Plant Heater Stack | USEPA Method 5/202 | FPM/CPM | 03/17/16 | 08:23 | 10:47 | | | | |
| 4 | H ₂ Plant Heater Stack | USEPA Method 5/202 | FPM/CPM | 03/18/16 | 08:05 | 10:19 | | | | |
| 0 | H ₂ Plant Heater Stack | Draft ASTM CCM | Sulfuric Acid | 03/18/16 | 12:35 | 13:35 | | | | |
| 1 | H ₂ Plant Heater Stack | Draft ASTM CCM | Sulfuric Acid | 03/18/16 | 14:30 | 15:30 | | | | |
| 2 | H ₂ Plant Heater Stack | Draft ASTM CCM | Sulfuric Acid | 03/18/16 | 16:14 | 17:14 | | | | |
| 3 | H ₂ Plant Heater Stack | Draft ASTM CCM | Sulfuric Acid | 03/18/16 | 18:00 | 19:00 | | | | |
| 1 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O₂/NOx/CO | 03/18/16 | 12:36 | 12:57 | | | | |
| 2 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O ₂ /NOx/CO | 03/18/16 | 13:09 | 13:30 | | | | |
| 3 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O₂/NOx/CO | 03/18/16 | 13:57 | 14:18 | | | | |
| 4 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O ₂ /NOx/CO | 03/18/16 | 14:30 | 14:51 | | | | |
| 5 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O ₂ /NOx/CO | 03/18/16 | 15:05 | 15:26 | | | | |
| 6 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O₂/NOx/CO | 03/18/16 | 15:36 | 15:57 | | | | |
| 7 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O ₂ /NOx/CO | 03/18/16 | 16:14 | 16:35 | | | | |
| 8 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O ₂ /NOx/CO | 03/18/16 | 16:46 | 17:07 | | | | |
| 9 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O₂/NOx/CO | 03/18/16 | 17:17 | 17:38 | | | | |
| 10 | H ₂ Plant Heater Stack | USEPA Methods 3A/7E/10 | O ₂ /NOx/CO | 03/18/16 | 17:57 | 18:18 | | | | |
| 1 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 12:35 | 12:53 | | | | |
| 2 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 13:10 | 13:21 | | | | |
| 3 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 13:57 | 14:05 | | | | |
| 4 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 14:32 | 14:41 | | | | |
| 5 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 15:05 | 15:15 | | | | |
| 6 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 15:38 | 15:48 | | | | |
| 7 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 16:14 | 16:20 | | | | |
| 8 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 16:45 | 16:56 | | | | |
| 9 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 17:17 | 17:27 | | | | |
| 10 | H ₂ Plant Heater Stack | USEPA Method 2 | Velocity & Flow Rate | 03/18/16 | 18:00 | 18:09 | | | | |

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PROJECT OVERVIEW

Results Summary

Table 1-2 and Table 1-3 summarize the results of the test program. A more detailed presentation of the test conditions and results of analysis are shown on pages 2-1 through 2-15.

Table 1-2:

| Source | | | Average | |
|------------------|------------------------------|-----------------|------------|---------------------------|
| Constituent | (Units) | Sampling Method | Emission | Permit Limit ¹ |
| H 2 Plant Heater | Stack | | | |
| PM | (Ib/MMBtu) | USEPA M-5 | 0.00068 | 0.0034 |
| PM | (Ton/yr) | USEPA M-5 | 1.78 | 6.86 |
| PM ₁₀ | (Ib/MMBtu) | USEPA M-5 / 202 | 0.0024 | 0.010 |
| H_2SO_4 | (Ib/MMBtu) | Draft ASTM CCM | 0.00011 | N/A |
| VOC | (Ib/MMBtu) | USEPAM-25A/18 | < 0.000779 | 0.0055 |
| NOx | (lb/MMBtu) | USEPA M-7E | 0.0073 | 0.013 |
| NOx | (ppmdv @ 0% O ₂) | USEPA M-7E | 6.0 | 60 |
| со | (Ton/yr) | USEPAM-10 | < 1.1 | 13 |

¹ Permit limits obtained from MDEQ Permit to Install No. 63-08D.

Table 1-3: Summary of RATA Results

| Source Constituent (Units) | Reference Method (USEPA) | Relative Accuracy ¹ | Units | Applicable Specification | Specification Limit ² | | | | |
|-------------------------------|-----------------------------|-----------------------------------|-----------|-----------------------------|-------------------------------------|--|--|--|--|
| H 2 Plant Heater Stack | | | | | | | | | |
| Flow rate (dscfh) | M-2 | 12.3 | % of RM | PS6 | 20% of RM | | | | |
| O ₂ (% dv) | M-3A | 0.1 | %dv | PS3 | ± 1.0% dv | | | | |
| H ₂ O (% wv) | M-4 | 11.4 | % of RM | N/A | N/A | | | | |
| NOx (ppmdv) | M-7E | 2.2 | % of RM | PS2 | 20% of RM | | | | |
| NOx (lb/MMBtu) | M-7E | 13.8 | % of RM | PS2 | 20% of RM | | | | |
| NOx (ppmdv @ 0%O2) | M-7E | 1.9 | % of RM | PS2 | 20% of RM | | | | |
| CO (ppmdv) | M-10 | 0.4 | ppmdv | PS4A ³ | ± 5 ppmdv | | | | |
| CO (lb/hr) | M-10 | 0.4 | % of Std. | PS4A ³ | 5% of Standard | | | | |

¹ Relative Accuracy is expressed in terms of comparison to the reference method (% RM) or applicable emission standard (% Std.), equivalent to the permit limit in Table 1-2. The specific expression used depends on the specification limit.

² Specification limits obtained from 40 CFR 60, Appendix B, Performance Specifications, unless otherwise noted.

³ For any sources emitting less than 200 ppmv of CO, PS4A applies. The PS4A RA limit is either < 10% of RM, <5% of Standard, or ± 5 ppmv (abs. average difference plus 2.5 x confidence coefficient).</p>

⁴ CO Standard = 13 Ton/yr = 56.9 lb/hr (assuming 8,760 operating hours/year)

Revision 0, Final Report

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PROJECT OVERVIEW

Discussion of Test Program

FPM and CPM Testing – USEPA Method 5/202

For this test program, the PM emission rate is assumed equivalent to FPM emission rate. The PM_{10} emission rate is assumed equivalent to the sum of FPM and CPM emission rates (units of lb/hr, Ton/yr, or lb/MMBtu for all constituents).

The analytical procedures in EPA Method 202 include an ammonium titration of the inorganic sample fractions with pH less than 7.0 to neutralize acids with hygroscopic properties such as H_2SO_4 that may be present in the sample. This step speeds up the sample desiccation process and allows the samples to come to a constant weight prior to weighing. The weight of ammonium added to the sample as a result of the titration is subtracted from the analytical result.

The laboratory performing the gravimetric analysis (Clean Air Analytical Services) has determined that only samples with an initial pH less than 4.5 require a significant amount of ammonium neutralization, resulting in a correction in excess of 0.5 mg. Based on this observation, the laboratory has altered their procedures to read that a sample must have a pH lower than 4.5 in order to be titrated.

Since none of the inorganic sample fractions collected during this test program had a pH less than 4.5, they were not titrated per Clean Air Analytical Services' modified procedure. The sample fraction was observed to come to a constant weight without having to titrate the sample.

Four test runs were performed for a duration of 120 minutes each. Following Run 2, the wind gusts became a safety concern, and the test crew was removed from the test location. The Run 2 sampling train remained on the stack and was retrieved the following day which disallowed a prompt sample train purge and recovery following sampling. Run 2 velocity, flow and moisture measurements are shown in the appendices of the report, but no laboratory analysis was performed. Run 4 was performed to constitute three valid runs.

The final results for each parameter were expressed as the average of three valid runs (Runs 1, 3 and 4) and were below the permit limits for both PM and PM_{10} .

H₂SO₄ Testing – Draft ASTM Controlled Condensation Method

Prior to the first official test run, a 60-minute sample conditioning run was performed on March 18, 2016, in order to minimize the absorption capacity of the front-half components of the sample train (upstream of the H_2SO_4 -collection portion of the sample train). The conditioning run was recovered in the same manner as the official test runs, but is not included in the results.

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Three 60-minute test runs were performed on March 18, 1016. The final result was expressed as the average of three valid runs (Runs 1, 2 and 3).

VOC Testing – USEPA Method 25A and Method 18

Four 60-minute Method 25A test runs for THC were performed concurrently with four 60-minute Method 18 bag collections for CH_4 and C_2H_6 on March 15 and 16, 2016. Run 3 was paused during the test run for approximately 35 minutes because of equipment trouble shooting on a separate sample train. Run 3 was not used in the final results because of the discontinuation in operation. The final results for each parameter were expressed as the average of three valid runs (Run 1, 2 and 4).

VOC emission rate is normally equivalent to THC emission rate, minus CH_4 and C_2H_6 emission rate (units of lb/hr, Ton/yr, or lb/MMBtu for all constituents). For CH_4 and C_2H_6 , a non-detectable result was obtained for all runs, so no correction was made to the THC results. Therefore, VOC emissions are equivalent to THC emissions.

Flow Rate, Moisture, O₂, NO_X, and CO RATA Testing – USEPA Methods 2, 3A, 4, 7E and 10; Performance Specifications 2, 3, 4A and 6

Minute-average data points for O_2 , CO_2 , NO_X and CO (dry basis) were collected over a period of 21 minutes for each relative accuracy test audit (RATA) reference method (RM) run.

The average result for each RM run was calculated and compared to the average result from the facility continuous emissions monitoring system (CEMS) over identical time intervals in order to calculate relative accuracy (RA).

- For O_2 (%dv), RA is expressed as the average absolute difference between the RM and facility CEMS runs. The final result was below the limit of $\pm 1.0\%$ dv set by PS3.
- For NO_X (ppmdv) concentration, RA is expressed as the percent difference between RM and facility CEMS runs. The final result was below the limit of 20% of the RM set by PS2.
- For NO_X (lb/MMBtu) diluent, RA is expressed as the percent difference between RM and facility CEMS runs. The final result was below the limit of 20% of the RM set by PS2.
- For NO_X (ppmdv @ 0% O₂) diluent, RA is expressed as the percent difference between RM and facility CEMS runs. The final result was below the limit of 20% of the RM set by PS2.

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PROJECT OVERVIEW For CO (ppmdv) concentration, the RA limit is expressed as the average • absolute difference between the RM and facility CEMS runs, plus 2.5 times the confidence coefficient. The final result was below the limit of \pm 5 ppmdv set by PS4A, which is applicable to sources that emit less than 200 ppmv of CO. For CO (lb/hr) diluent, RA is expressed as the percent difference between RM and facility CEMs runs. The final result was below the limit of 5% of the standard (permit limit listed in Table 1-3) set by PS4A. CO₂ data was collected only as supplemental information. Facility flow rate CEMS were evaluated using Method 2 as the reference method. A complete flow and temperature traverse was performed during each 21-minute RATA run, converted to units of dry standard cubic feet per hour (dscfh) and then compared to facility CEMS results over the corresponding 21-minute intervals. For flow rate, RA is expressed as the percent difference between RM and facility CEMS data. The final results were below the limit of 20% of the RM set by PS6. Moisture data was used to convert flow rate from dry basis to wet basis and was obtained from concurrently operated Draft ASTM CCM test runs: For RATA Runs 1, 2 and 3, H₂O data was obtained from Draft ASTM CCM • Run 0. For RATA Runs 4, 5 and 6, H₂O data was obtained from Draft ASTM CCM Run 1. For RATA Runs 7, 8 and 9, H₂O data was obtained from Draft ASTM CCM Run 2. For RATA Run 10, H₂O data was obtained from Draft ASTM CCM Run 3. NO_X and CO results from the RATA were converted from units of dry volume-based concentration (ppmdv) to mass-based emission rate units (lb/hr, Ton/yr, and lb/MMBtu) to demonstrate compliance with permit limits. The final results for each parameter were expressed as the average of all 10 RATA runs. The final results were below the permit limits.

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PROJECT OVERVIEW

Calculation of Final Results

Emission results in units of dry volume-based concentration (lb/dscf, ppmdv) were converted to units of lb/MMBtu by first calculating mass-based emissions in units of lb/hr, and then applying the total heat input to the unit over each test interval (MMBtu/hr). Heat input data was provided by Air Products. Flow rates used in calculating lb/hr emissions were obtained in the following manner:

- For Method 5/202, flow rate measurements are incorporated into the sampling procedures.
- For Method 18/25A, flow rate measurements from the most nearly concurrent Method 5/202 test runs were used.
- For Draft ASTM CCM, two flow rate measurements, per Method 2 specifications, was performed concurrently with each test run. An average of the two flow measurements was used with the exception of Run 3, which only used the final flow measurement, Run 10.
- For Method 7E/10, a flow rate measurement, per Method 2 specifications, was performed concurrently with each test run.

General Considerations

All run times listed throughout this report correspond to the plant time utilized by Air Products. Plant time is the time of the Air Products CEMS and data acquisition systems. The plant time is 60 minutes earlier than actual Eastern Time.

End of Section 1 - Project Overview

AIR PRODUCTS AND CHEMICALS, INC. DETROIT HYDROGEN PLANT

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| | R | ES | | L | ГS |
|--|---|----|--|---|----|
|--|---|----|--|---|----|

2-1

| | Ta FPM, CPM and Total PM | able 2-1: In Emission | s (USEPA | M-5/202) | |
|------------------------|---|--------------------------|----------|----------|-------------------|
| Run No. | | 1 | 3 | 4 | Average |
| Date (201 | 6) | Mar 15 | Mar 17 | Mar 18 | |
| Start Time | (approx.) | 15:18 | 08:23 | 08:05 | |
| Stop Time | (approx.) | 17:28 | 10:47 | 10:19 | |
| Process (| Conditions | | | | |
| P₁ H | ydrogen production (Mscf/day) | 59.8 | 58.0 | 59.5 | 59.1 |
| P ₂ A | queous NH3 feed to SCR (lb/hr) | 36.0 | 36.5 | 37.9 | 36.8 |
| P ₃ S | CR Inlet temperature (°F) | 642.5 | 633.4 | 640.7 | 638.9 |
| H _t A | ctual heat input (MMBtu/hr) | 592.7 | 591.6 | 605.3 | 596.5 |
| Cap C | apacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Condi | itions | | | | |
| O2 0 | xygen (dry volume %) | 3.2 | 3.3 | 3.9 | 3.5 |
| CO₂ C | arbon dioxide (dry volume %) | 18.5 | 18.5 | 17.7 | 18.2 |
| | ample temperature (°F) | 322 | 317 | 320 | 320 |
| B _w A | ctual water vapor in gas (% by volume) | 15.4 | 14.9 | 14.2 | 14.8 |
| Gas Flow | Rate | | | | |
| Q _a Ve | olumetric flow rate, actual (acfm) | 229,000 | 225,000 | 227,000 | 227,000 |
| Q _s V | olumetric flow rate, standard (scfm) | 151,000 | 148,000 | 150,000 | 149,000 |
| Q _{std} V | olumetric flow rate, dry standard (dscfm) | 127,000 | 126,000 | 129,000 | 127,000 |
| Sampling | Data | | | | |
| V _{mski} Vi | olume metered, standard (dscf) | 81.35 | 79.40 | 81.77 | 80.84 |
| %I Is | okinetic sampling (%) | 102.9 | 101.8 | 102.4 | 102.3 |
| Laborator | y Data | | | | |
| m _n Te | otal FPM (g) | 0.00161 | 0.00281 | 0.00144 | |
| т _{орм} Та | otal CPM (g) | 0.00468 | 0.00518 | 0.00504 | |
| m _{Part} Te | otal particulate (expressed as PM-10) (g) | 0.00630 | 0.00799 | 0.00648 | |
| n _{MDL} N | umber of non-detectable fractions | N/A | N/A | N/A | |
| DLC D | etection level classification | ADL | ADL | ADL | • |
| FPM Resu | lts | | | | |
| C _{sd} Pa | articulate Concentration (lb/dscf) | 4.37E-08 | 7.80E-08 | 3.88E-08 | 5.35E-08 |
| E _{lb/br} Pr | articulate Rate (Ib/hr) | 0.334 | 0,588 | 0.300 | 0.407 |
| E _{t/y} Pa | articulate Rate (Ton/yr) | 1.46 | 2.58 | 1.31 | 1.78 |
| E _{Hi} Pa | articulate Rate - Heat Input-based (Ib/MMBtu) | 5.63E-04 | 9.94E-04 | 4.95E-04 | 6.84E-04 |
| CPM Resu | lts | | | | |
| C _{sd} Pa | articulate Concentration (lb/dscf) | 1.27E-07 | 1.44E-07 | 1.36E-07 | 1.36E-07 |
| E _{lb/ter} Pa | articulate Rate (Ib/hr) | 0.971 | 1.08 | 1.05 | 1.03 |
| E _{T/y} Pa | articulate Rate (Ton/yr) | 4.25 | 4.75 | 4.59 | 4.53 |
| E _{Hi} Pi | articulate Rate - Heat Input-based (Ib/MMBtu) | 1.64E-03 | 1.83E-03 | 1.73E-03 | 1.73 E- 03 |
| Total Parti | culate (as PM10) Results | | | | |
| C _{sd} Pa | articulate Concentration (lb/dscf) | 1.71E-07 | 2.22E-07 | 1.75E-07 | 1.89E-07 |
| Elb/hr Pa | articulate Rate (ib/hr) | 1.30 | 1.67 | 1.35 | 1.44 |
| E _{T/y} Pa | articulate Rate (Ton/yr) | 5.71 | 7.32 | 5.91 | 6.31 |
| E _{HI} Pa | articulate Rate - Heat Input-based (Ib/MMBtu) | 2,20E-03 | 2.83E-03 | 2.23E-03 | 2.42E-03 |

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Average includes 3 runs.

Detection level classifications are defined as follows:

ADL = Above Detection Level - all fractions are above detection limit

DLL = Detection Level Limited - some fractions are below detection limit

BDL = Below Detection Limit - all fractions are below detection limit

AIR PRODUCTS AND CHEMICALS, INC. DETROIT HYDROGEN PLANT

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| Table 2-2: Uncertainty Analysis – FPM, CPM and Total PM₁₀ (USEPA M-5/202) | | | | | | | | | | |
|--|---|-------------|----------|-------------|---|----------------------|--|--|--|--|
| | | FPM Results | 11 m, 01 | CPM Results | | PM (as PM10) Results | | | | |
| | | (ib/MMBtu) | | (lb/MMBtu) | | (lb/MMBtu) | | | | |
| Nethod | | 5 | | 202 | | 5/202 | | | | |
| Run No. | 1 | 0.0006 | 1 | 0.0016 | 1 | 0.0022 | | | | |
| | 3 | 0.0010 | 3 | 0.0018 | 3 | 0.0028 | | | | |
| | 4 | 0.0005 | 4 | 0.0017 | 4 | 0.0022 | | | | |
| 5D | | 0.0003 | | 0.0001 | | 0.0004 | | | | |
| VG | | 0.0007 | | 0.0017 | | 0.0024 | | | | |
| RSD | | 39.5% | | 5.6% | | 14.6% | | | | |
| 1 | | 3 | | 3 | | 3 | | | | |
| ε | | 0.0002 | | 0.0001 | | 0.0002 | | | | |
| RSE | | 22.8% | | 3.2% | | 8.4% | | | | |
| , | | 95.0% | | 95.0% | | 95,0% | | | | |
| NV | | 4.303 | | 4.303 | | 4.303 | | | | |
| ; + | | 0.0014 | | 0.0020 | | 0.0033 | | | | |
| VG | | 0.0007 | | 0.0017 | | 0.0024 | | | | |
| CI - | | 0.0000 | | 0.0015 | | 0.0015 | | | | |
| г в + | | 0.0028 | | 0.0025 | | 0.0051 | | | | |

AVG (average) is the mean value of the runs; N is the number of individual runs.

SD (standard deviation) and RSD (relative standard deviation) are measures of the variability of individual runs.

SE (standard error) and RSE (relative standard error) are measures of the variability of the average of the runs.

P (probability) is the confidence level associated with the two-tailed Student's t-distribution.

TINV (t-value) is the value of the Student's t-distrubution as a function of P (probability) and N-1 (degrees of freedom).

CI (confidence interval) indicates that if the test is conducted again under the same conditions, the average would be expected to fall within the interval (CI- to CI+) about 95% of the time.

TB+ (upper tolerance bound) is the value below which 95% of future runs are expected to fall (assuming testing at the same conditions).

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| | Table | | | | |
|-----------------------------|---|-----------------|----------|----------|---------|
| | H ₂ SO ₄ Emissions | (Draft ASTM CCM | l) | | |
| Run No | • | 1 | 2 | 3 | Averag |
| Date (2 | 016) | Mar 18 | Mar 18 | Mar 18 | |
| Start Ti | me (approx.) | 14:30 | 16:14 | 18:00 | |
| Stop Ti | me (approx.) | 15:30 | 17:14 | 19:00 | |
| Proces | s Conditions | | | | |
| P ₁ | Hydrogen production (Mscf/day) | 59.0 | 57.8 | 58.0 | 58. |
| P ₂ | Aqueous NH ₃ feed to SCR (lb/hr) | 37.2 | 36.0 | 36.2 | 36. |
| P ₃ | SCR Inlet temperature (°F) | 638.6 | 633.2 | 634.4 | 635. |
| Hi | Actual heat input (MMBtu/hr) | 600.2 | 590.0 | 594.2 | 594. |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,76 |
| Gas Co | nditions | | | | |
| O2 | Oxygen (dry volume %) | 3.9 | 3.5 | 3.5 | 3. |
| CO_2 | Carbon dioxide (dry volume %) | 17.8 | 18.4 | 18.4 | 18. |
| Тs | Sample temperature (°F) | 329 | 327 | 328 | 32 |
| В _w | Actual water vapor in gas (% by volume) | 16.05 | 15.61 | 15.99 | 15.8 |
| Gas Flo | w Rate | | | | |
| $\mathbf{Q}_{\mathrm{std}}$ | Volumetric flow rate, dry standard (dscfm) ¹ | 119,000 | 119,000 | 120,000 | 119,00 |
| Sampli | ng Data | | | | |
| V_{mstd} | Volume metered, standard (dscf) | 25.36 | 25.30 | 25.47 | 25.3 |
| Labora | tory Data (Ion Chromatography) | | | | |
| mn | Total H2SO4 collected (mg) | 0.0760 | 0.1345 | 0.1095 | |
| r Sulfuria | Acid Vapor (H2SO4) Results | | | | |
| C_{sd} | H2SO4 Concentration (lb/dscf) | 6.61E-09 | 1.17E-08 | 9.48E-09 | 9.27E-0 |
| \mathbf{C}_{sd} | H2SO4 Concentration (pprndv) | 0.0260 | 0.0461 | 0.0373 | 0.036 |
| Elbhr | H2SO4 Rate (lb/hr) | 0.0472 | 0.0836 | 0.0680 | 0.066 |
| ETA | H2SO4 Rate (Ton/yr) | 0.207 | 0,366 | 0.298 | 0.29 |
| E _{Hi} | H2SO4 Rate - Heat Input-based (Ib/MMBtu) | 7.87E-05 | 1.42E-04 | 1.14E-04 | 1.12E-0 |

Average includes 3 runs.

¹ Flow rate obtained from the average of the concurrently operated Method 2 test run(s).

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| RESULTS | | | | | | |
|---------------------------------------|-------|--|---|-------------|--|--|
| | | Table 2- Uncertainty Analysis – H₂S | | MA) | | |
| · · · · · · · · · · · · · · · · · · · | | H2SO4 Results | H2SO4 (Brait Aorin Conn) H2SO4 Results | | | |
| | | (ppmdv) | | (Ib/MMBtu) | | |
| Viethod | | ССМ | | ССМ | | |
| Run No. | 1 | 0.0260 | 1 | 7.87E-05 | | |
| | 2 | 0.0461 | 2 | 1.42E-04 | | |
| | 3 | 0.0373 | 3 | 1.14E-04 | | |
| 5D | | 0.0101 | | 3.16E-05 | | |
| AVG | | 0.0364 | | 1.12E-04 | | |
| RSD | 27.6% | | | 28.3% | | |
| 1 | | 3 | | 3 | | |
| θE | | 0.0058 | | 1.82E-05 | | |
| RSE | | 16.0% | 16.3% | | | |
| c | | 95.0% | | 95.0% | | |
| ſINV | | 4.303 | | 4.303 | | |
| C1 + | | 0.0615 | | 1.90E-04 | | |
| AVG | | 0.0364 | | 1.12E-04 | | |
| CI - | | 0.0114 | | 3.31E-05 | | |
| ТВ + | | 0.114 | | 3.53E-04 | | |

AVG (average) is the mean value of the runs; N is the number of individual runs.

SD (standard deviation) and RSD (relative standard deviation) are measures of the variability of individual runs.

SE (standard error) and RSE (relative standard error) are measures of the variability of the average of the runs.

P (probability) is the confidence level associated with the two-tailed Student's t-distribution.

TINV (t-value) is the value of the Student's t-distrubution as a function of P (probability) and N-1 (degrees of freedom).

CI (confidence interval) indicates that if the test is conducted again under the same conditions, the average would be expected to fall within the interval (CI- to CI+) about 95% of the time.

TB+ (upper tolerance bound) is the value below which 95% of future runs are expected to fall (assuming testing at the same conditions).

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RESULTS

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| | Ta THC, CH₄, C₂H₅, and VOC | able 2-5: CEmissions (| USEPA N | 1-25A/18) | | |
|-------------------|--|---------------------------|-----------|-----------|-----------|-----------|
| Run No. | | 1 | 2 | 3* | 4 | Average |
| Date (20 | 16) | Mar 15 | Mar 15 | Mar 16 | Mar 16 | |
| • | ne (approx.) | 15:01 | 16:11 | 08:39 | 10:27 | |
| | ie (approx.) | 16:01 | 17:11 | 10:14 | 11:27 | |
| Process | s Conditions | | | | | |
| P ₁ | Hydrogen Production (Mscf/day) | 59.8 | 57.1 | 56.0 | 55.8 | 57.6 |
| P ₂ | Aqueous NH ₃ feed to SCR (lb/hr) | 36.0 | 35.5 | 32.3 | 32.4 | 34.6 |
| Pa | SCR Inlet Temperature | 642.5 | 634.1 | 625.8 | 624.7 | 633.8 |
| H, | Actual heat input (MMBtu/hr) | 588.5 | 581.0 | 571.8 | 571.6 | 580.4 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Cor | ditions | | | | | |
| O ₂ | Oxygen (dry volume %) | 3.1 | 3.3 | 3.2 | 3.2 | 3.2 |
| CO2 | Carbon dioxide (dry volume %) | 18.6 | 18.3 | 18.7 | 18.7 | 18.6 |
| Bw | Actual water vapor in gas (% by volume) ¹ | 15.4 | 15.4 | 15.3 | 15.3 | 15.3 |
| Gas Flov | v Rate ² | | | | | |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 127,000 | 127,000 | 118,000 | 118,000 | 124,000 |
| THC Res | ults ³ | | | | | |
| C_{sd} | Concentration (ppmdvas C ₃ H ₈) | <0.531 | <0.531 | <0.530 | <0.530 | <0.530 |
| C_{sd} | Concentration (Ib/dscf) | <6.07E-08 | <6.07E-08 | <6.06E-08 | <6.06E-08 | <6.07E-08 |
| Eibhr | Emission Rate (lb/hr) | < 0.464 | < 0.464 | < 0.429 | < 0.429 | < 0.452 |
| E _{TAr} | Emission Rate (Ton/yr) | < 2.03 | < 2.03 | < 1.88 | < 1.88 | < 1.98 |
| E _{HI} | Emission Rate - Heat input-based (Ib/MMBtu) | <7.89E-04 | <7.99E-04 | <7.50E-04 | <7.50E-04 | <7.79E-04 |
| Methane | e Results ⁴ | | | | | |
| C_{sd} | Concentration (ppmdv) | <0.134 | <0.134 | <0.134 | <0.134 | <0.134 |
| C _{sd} | Concentration (lb/dscf) | <5.58E-09 | <5.58E-09 | <5.58E-09 | <5.58E-09 | <5.58E-09 |
| Ellow | Emission Rate (lb/hr) | < 0.0427 | < 0.0427 | < 0.0394 | < 0.0394 | < 0.0416 |
| E _{T/y} | Emission Rate (Ton/yr) | < 0.187 | < 0.187 | < 0.173 | < 0.173 | < 0.182 |
| EH | Emission Rate - Heat input-based (Ib/MMBtu) | <7.25E-05 | <7.34E-05 | <6.90E-05 | <6.90E-05 | <7.16E-05 |
| Ethane F | Results⁴ | | | | | |
| C_{sd} | Concentration (ppmdv) | <0.107 | <0.107 | <0.107 | <0.107 | <0.107 |
| C_{sd} | Concentration (lb/dscf) | <8.34E-09 | <8.34E-09 | <8.34E-09 | <8.34E-09 | <8.34E-09 |
| Elb/w | Emission Rate (lb/hr) | < 0.0638 | < 0.0638 | < 0.0590 | < 0.0590 | < 0.0622 |
| ETAY | Emission Rate (Ton/yr) | < 0.279 | < 0.279 | < 0.258 | < 0.258 | < 0.272 |
| EH | Emission Rate - Heat input-based (Ib/MMBtu) | <1.08E-04 | <1.10E-04 | <1.03E-04 | <1.03E-04 | <1.07E-04 |
| VOC Res | sults | | | | | |
| Einn | Emission Rate (Ib/hr) | < 0.464 | < 0.464 | < 0.429 | < 0.429 | < 0.452 |
| E _{T/yr} | Emission Rate (Ton/yr) | < 2.03 | < 2.03 | < 1.88 | < 1.88 | < 1.98 |
| EHI | Emission Rate - Heat input-based (Ib/MMBtu) | <7.89E-04 | <7.99E-04 | <7.50E-04 | <7.50E-04 | <7.79E-04 |

Average includes 3 runs, * indicates run not included in average.

.

¹ Moisture data used for ppmwv to ppmdv correction obtained from nearly-concurrent M-5/202 runs.

 $^2\,$ Flow data used in lb/hr calculations was obtained from nearly-concurrent Method 5/202 runs .

³ For THC, '<' indicates a measured response below the detection limit (assumed to be 1% of the instrument calibration span).

⁴ For methane and ethane, '<' indicates a measured response below the analytical detection limit determined by the laboratory.

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RESULTS

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| | NO _x and CO I | Table : Emission | - | A M-7E/1 | 0) | | |
|--------------------|--|---------------------|-----------|-----------|-----------|-----------|-----------|
| Run No. | | 1 | 2 | 3 | 4 | 5 | 6 |
| Date (20 | 016) | Mar 18 | Mar 18 | Mar 18 | Mar 18 | Mar 18 | Mar 18 |
| - | ne (approx.) | 12:36 | 13:09 | 13:57 | 14:30 | 15:05 | 15:36 |
| | ne (approx.) | 12:57 | 13:30 | 14:18 | 14:51 | 15:26 | 15:57 |
| Proces | s Conditions | | | | | | |
| P1 | Hydrogen Production (Mscf/day) | 58.5 | 58.5 | 58.5 | 58.5 | 58.5 | 58.5 |
| P ₂ | Aqueous NH ₃ feed to SCR (lb/hr) | 36.7 | 36.7 | 36.7 | 36.7 | 36,7 | 36.7 |
| P ₃ | SCR Inlet Temperature | 635.9 | 635.9 | 635.9 | 635.9 | 635.9 | 635.9 |
| H | Actual heat input (MMBtu/hr) | 594.5 | 594.5 | 594.5 | 594.5 | 594.5 | 594.5 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | nditions | | | | | | |
| O_2 | Oxygen (dry volume %) | 3.17 | 3.21 | 3.23 | 3.24 | 3.27 | 3.26 |
| CO2 | Carbon dioxide (dry volume %) | 18.4 | 18.4 | 18.4 | 18.4 | 18.3 | 18.4 |
| B,, | Actual water vapor in gas (% by volume) ¹ | 13.0 | 13.0 | 13.0 | 16.0 | 16.0 | 16.0 |
| Gas Flor | w Rate ² | | | | | | |
| \mathbf{Q}_{std} | Volumetric flow rate, dry standard (dscfm) | 120,666 | 122,475 | 121,765 | 118,568 | 119,537 | 117,755 |
| Nitroge | n Oxides Results | | | | | | |
| C _{sd} | Concentration (ppmdv) | 5.11 | 5.38 | 5.06 | 4.90 | 5.15 | 4.69 |
| Csd-x | Concentration @ 0% O ₂ (ppmdv) | 6.03 | 6.36 | 5.99 | 5.80 | 6.11 | 5.55 |
| C_{sd} | Concentration (lb/dscf) | 6.11E-07 | 6.42E-07 | 6.04E-07 | 5.85E-07 | 6.15E-07 | 5.60E-07 |
| E _{ib/m} | Emission Rate (lb/hr) | 4.42 | 4.72 | 4.41 | 4.16 | 4.41 | 3.95 |
| Етлу | Emission Rate (Ton/yr) | 19.4 | 20.7 | 19.3 | 18.2 | 19.3 | 17.3 |
| E _{Hi} | Emission Rate - Heat input-based (lb/MMBtu) | 7.44E-03 | 7.94E-03 | 7.42E-03 | 7.00E-03 | 7.42E-03 | 6.65E-03 |
| Carbon | Monoxide Results ³ | | | | | | |
| C_{sd} | Concentration (ppmdv) | <0.478 | <0.478 | <0.478 | <0.478 | <0.478 | <0.478 |
| C_{sd-x} | Concentration @ 0% O_2 (ppmdv) | < 0.563 | < 0.565 | < 0.565 | < 0.566 | < 0.567 | < 0.566 |
| C_{sd} | Concentration (lb/dscf) | <3.47E-08 | <3.47E-08 | <3.47E-08 | <3.47E-08 | <3.47E-08 | <3.47E-08 |
| Elbhr | Emission Rate (lb/hr) | < 0.252 | < 0.255 | < 0.254 | < 0.247 | < 0.249 | < 0.246 |
| Entyr | Emission Rate (Ton/yr) | < 1.102 | < 1.118 | < 1.112 | < 1.083 | < 1.092 | < 1.075 |
| E _{HI} | Emission Rate - Heat input-based (lb/MMBtu) | <4.23E-04 | <4.30E-04 | <4.27E-04 | <4,16E-04 | <4.19E-04 | <4.13E-04 |

¹ Moisture data obtained from nearly-concurrent Draft ASTM CCM runs.

² Flow data used in lb/hr calculations was obtained from nearly-concurrent Method 2 runs.

³ For CO, '<' indicates a measured response below the detection limit (assumed to be 1% of the instrument calibration span).

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| RESULTS |
|---------|
|---------|

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| Table 2-6 (Continued):NOx and CO Emissions (USEPA M-7E/10) | | | | | | | | | |
|--|--|-----------|-----------|-----------|-----------|-----------|--|--|--|
| Run No. | · · · · · · · · · · · · · · · · · · · | 7 | 8 | 9 | 10 | Average | | | |
| Date (20 | 016) | Mar18 | Mar 18 | Mar 18 | Mar 18 | | | | |
| Start Tin | ne (approx.) | 16:14 | 16:46 | 17:17 | 17:57 | | | | |
| Stop Tin | ne (approx.) | 16:35 | 17:07 | 17:38 | 18:18 | | | | |
| Process | s Conditions | | | | | | | | |
| P ₁ | Hydrogen Production (Mscf/day) | 58.5 | 58.5 | 58.5 | 58.5 | 58.5 | | | |
| P ₂ | Aqueous NH₃ feed to SCR (lb/hr) | 36.7 | 36.7 | 36.7 | 36.7 | 36.7 | | | |
| P ₃ | SCR Inlet Temperature | 635.9 | 635,9 | 635.9 | 635.9 | 635.9 | | | |
| Hi | Actual heat input (MMBtu/hr) | 594.5 | 594.5 | 594.5 | 594.5 | 594.5 | | | |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 | 8,760 | | | |
| Gas Cor | nditions | | | | | | | | |
| O ₂ | Oxygen (dry volume %) | 3.29 | 3.30 | 3.24 | 3.25 | 3.25 | | | |
| CO2 | Carbon dioxide (dry volume %) | 18.4 | 18,3 | 18.3 | 18.3 | 18.4 | | | |
| Bw | Actual water vapor in gas (% by volume) ¹ | 15.6 | 15.6 | 15.6 | 16.0 | 15.0 | | | |
| Gas Flow | w Rate ² | | | | | | | | |
| \mathbf{Q}_{std} | Volumetric flow rate, dry standard (dscfm) | 119,687 | 117,947 | 118,612 | 119,576 | 120,000 | | | |
| Nitroger | n Oxides Results | | | | | | | | |
| C _{sd} | Concentration (ppmdv) | 4.76 | 5.08 | 5.06 | 5.12 | 5.03 | | | |
| C _{sd-x} | Concentration @ 0% O ₂ (ppmdv) | 5.65 | 6.03 | 5.99 | 6.06 | 5.96 | | | |
| C_{sd} | Concentration (Ib/dscf) | 5.69E-07 | 6.06E-07 | 6.04E-07 | 6.11E-07 | 6.01E-07 | | | |
| Elio/hr | Emission Rate (Ib/hr) | 4.08 | 4.29 | 4.30 | 4.39 | 4.31 | | | |
| ETAY | Emission Rate (Ton/yr) | 17.9 | 18.8 | 18.8 | 19.2 | 18.9 | | | |
| E _{Hi} | Emission Rate - Heat input-based (lb/MMBtu) | 6.87E-03 | 7.22E-03 | 7.23E-03 | 7.38E-03 | 7.26E-03 | | | |
| Carbon | Monoxide Results ³ | | | | | | | | |
| \mathbf{C}_{sd} | Concentration (ppmdv) | <0.478 | <0.478 | <0.478 | <0.478 | <0.478 | | | |
| C _{ad-x} | Concentration @ 0% O ₂ (ppmdv) | < 0.567 | < 0.567 | < 0.566 | < 0.566 | <0.566 | | | |
| C_{sd} | Concentration (Ib/dscf) | <3.47E-08 | <3.47E-08 | <3.47E-08 | <3.47E-08 | <3.47E-08 | | | |
| Ether | Emission Rate (lb/hr) | < 0.250 | < 0.246 | < 0.247 | < 0.249 | < 0.249 | | | |
| E _{T/y} | Emíssion Rate (Ton/yr) | < 1.093 | < 1.077 | < 1.083 | < 1.092 | < 1.093 | | | |
| E _{Hi} | Emission Rate - Heat input-based (lb/MMBtu) | <4.20E-04 | <4.14E-04 | <4.16E-04 | <4.19E-04 | <4.20E-04 | | | |
| | | | | | | | | | |

Average includes 10 runs.

¹ Moisture data obtained from nearly-concurrent Draft ASTM CCM runs.

² Flow data used in lb/hr calculations was obtained from nearly-concurrent Method 2 runs.

³ For CO, '<' indicates a measured response below the detection limit (assumed to be 1% of the instrument calibration span).

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| | | DIYU | andard i low Mac | e RATA (USEP | A WEZ / F 30/ | |
|--|--|-----------------------------------|--|-----------------------------|-------------------------|---------------------|
| Run No. | Start Time | Date (2016) | RM Flow (dscfh) | CEMS Data | Difference | Difference Perce |
| 1 | 12:36 | Mar 18 | 7,239,973 | 6,326,032 | 913,941 | 12.6 |
| 2 * | 13:09 | Mar 18 | 7,348,479 | 6,350,470 | 998,009 | 13.6 |
| 3 | 13:57 | Mar 18 | 7,305,904 | 6,377,463 | 928,441 | 12.7 |
| 4 | 14:30 | Mar 18 | 7,114,089 | 6,385,676 | 728,413 | 10.2 |
| 5 | 15:05 | Mar 18 | 7,172,209 | 6,391,806 | 780,402 | 10.9 |
| 6 | 15:36 | Mar 18 | 7,065,282 | 6,308,943 | 756,339 | 10,7 |
| 7 | 16:14 | Mar 18 | 7,181,198 | 6,271,290 | 909,909 | 12.7 |
| 8 | 16:46 | Mar 18 | 7,076,810 | 6,292,113 | 784,697 | 11.1 |
| 9 | 17:17 | Mar 18 | 7,116,696 | 6,329,823 | 786,873 | 11.1 |
| 10 | 17:57 | Mar 18 | 7,174,539 | 6,339,291 | 835,248 | 11.6 |
| | Average | | 7,160,744 | 6,335,826 | 824,918 | 11.5 |
| | | | tion of Differences e Coefficient (CC) | 75,030 57,673 | | |
| | • | Jonnaena | e Coemclent (CC) | 57,673 | | |
| | | 43/-1 | | 0.000 | | |
| | | t-Val | ue for 9 Data Sets | 2.306 | • i • | |
| | Referenc | ative Accu e Method | ue for 9 Data Sets Iracy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% | Limit 20.0% Data) | 041316 143 |
| CEMS | Referenc = Contir | ative Accu e Method wous Em | racy (as % of RM) (CleanAir Data) | 12.3% stem (Air Products | 20.0% | 041316 143 |
| CEMS RATA | Referenc = Contir calculatio | ative Accu e Method wous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 143 |
| CEMS | Referenc = Contir calculatio | ative Accu e Method wous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 142 |
| CEMS RATA | Referenc = Contir calculatio | ative Accu e Method wous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 143 |
| CEMS RATA | Reference = Contir calculatio | ative Accu e Method uous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 145 |
| CEMS RATA 8,000 7,000 | Reference = Contir calculation ,000,000,000 | ative Accu e Method uous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 143 |
| CEMS RATA 8,000 7,000 6,000 | Reference = Contir calculatio ,000 | ative Accu e Method uous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 143 |
| CEMS RATA 8,000 7,000 6,000 5,000 | Reference = Contir calculation ,000 | ative Accu e Method uous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 143 |
| CEMS RATA 8,000 7,000 6,000 5,000 4,000 | Reference = Contir calculation ,000 | ative Accu e Method uous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 143 |
| CEMS RATA 8,000 7,000 6,000 5,000 4,000 3,000 | Reference = Contir calculation ,000 | ative Accu e Method uous Em | racy (as % of RM) (CleanAir Data) issions Monitoring Sy | 12.3% stem (Air Products | 20.0% | 041316 143 |

RM Flow (dscfh) -B--- CEMS Data

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| | <u></u> | | | entration RAT | | Diff |
|--|--|---|---|-------------------------------------|--------------------|----------------------|
| Run No. | Start Time | Date (2016) | RM Data (‱v) | CEMS Data (‱v) | Difference (‱v) | Difference Percen |
| 1 | 12:36 | Mar 18 | 13.0 | 16.0 | -3.0 | -22.6% |
| 2 * | 13:09 | Mar 18 | 13.0 | 16.0 | -3.0 | -22.6% |
| 3 | 13:57 | Mar 18 | 13.0 | 16.0 | -3.0 | -22.6% |
| 4 | 14:30 | Mar 18 | 16.0 | 16.0 | 0.0 | 0.3% |
| 5 | 15:05 | Mar 18 | 16.0 | 16.0 | 0.0 | 0.3% |
| 6 | 15:36 | Mar 18 | 16.0 | 16.0 | 0.0 | 0.3% |
| 7 | 16:14 | Mar 18 | 15.6 | 16.0 | -0.4 | -2.5% |
| 8 | 16:46 | Mar 18 | 15.6 | 16.0 | -0.4 | -2.5% |
| 9 10 | 17:17 17:57 | Mar18 Mar18 | 15.6 16.0 | 16.0 16.0 | -0.4 0.0 | -2.5% -0.1% |
| | Average | | 15.2 | 16.0 | -0.8 | -0.17 |
| | | | Bolotivo Ao | | it Deculto | |
| ~ | landard I | | | curacy Test Aud | il Results | |
| | tanoaro i | | f Differences | 1.250269 0.961040 | | |
| 3 | Conf | Idanaa Car | | | | |
| 3 | Conf | idence Coa | | | | |
| 0 | Conf | | 9 Data Sets | 2.306 | | |
| RM=I CEMS | Relative Referenc = Contin | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | | • | |
| RM=I CEMS | Relative Referenc = Contin | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | 041316 1630 |
| RM = I CEMS RATA | Relative Referenc = Contin | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = 1 CEMS RATA 16 14 12 10 | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA 18 16 14 12 10 8 | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA 18 16 14 12 10 8 6 | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA 18 16 14 12 10 8 6 | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM = I CEMS RATA 18 14 14 14 14 14 14 14 14 14 14 14 14 14 | Relative Referenc = Contin calculatio | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |
| RM=1 CEMS RATA 18 14 14 12 10 8 6 6 2 | Relative Referenc = Contin calculation 3.0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 | t-Value for Accuracy (e Method (C uous Emis | 9 Data Sets as % of RM) CleanAir Data) sions Monitorin | 2.306 11.4% ng System (Air Pr | • | |

AIR PRODUCTS AND CHEMICALS, INC. DETROIT HYDROGEN PLANT

Client Reference No: 4503676698 CleanAir Project No: 12915

2-10

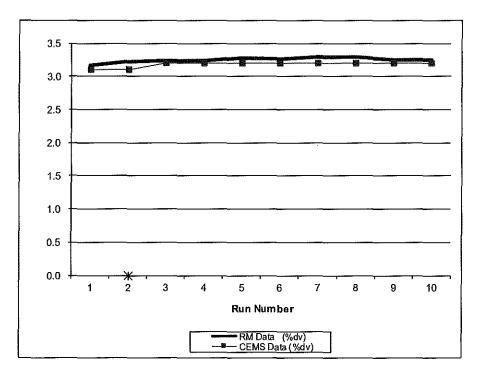
| Run No. | Start Time | Date (2016) | RM Data (%dv) | <u>(USEPA M-34</u> CEMS Data (%dv) | Difference (%dv) | Difference Percent |
|------------|---------------|----------------|------------------|--|---------------------|-----------------------|
| 1 | 12:36 | Mar 18 | 3.2 | 3.1 | 0.1 | 2.1% |
| 2 * | 13:09 | Mar 18 | 3.2 | 3.1 | 0.1 | 3.6% |
| 3 | 13:57 | Mar 18 | 3.2 | 3.2 | 0.0 | 1.0% |
| 4 | 14:30 | Mar 18 | 3.2 | 3.2 | 0.0 | 1.2% |
| 5 | 15:05 | Mar 18 | 3.3 | 3.2 | 0.1 | 2.2% |
| 6 | 15:36 | Mar 18 | 3.3 | 3.2 | 0.1 | 1.9% |
| 7 | 16:14 | Mar 18 | 3.3 | 3.2 | 0.1 | 2.7% |
| 8 | 16:46 | Mar 18 | 3.3 | 3.2 | 0.1 | 2.9% |
| 9 | 17:1 7 | Mar 18 | 3.2 | 3.2 | 0.0 | 1.4% |
| 10 | 17:57 | Mar 18 | 3.3 | 3.2 | 0.1 | 1.7% |
| | Average | | 3.3 | 3.2 | 0.1 | 1.9% |
| | - R | | | curacy Test Aud | it Results | |
| s | | | Differences | 0.021584 | | |
| | Con | fidence Coe | efficient (CC) | 0.016591 | | |

| Avg. Abs. Diff. (%dv) | 0.062 | 1.0 | |
|-----------------------------|----------|-------|--|
| | | Limit | |
| t-Value for 9 Data Sets | 2.306 | | |
| Confidence Coefficient (CC) | 0.016591 | | |

RM = Reference Method (CleanAir Data)

041316 163038

CEMS = Continuous Emissions Monitoring System (Air Products Data) RATA calculations are based on 9 of 10 runs. * indicates the excluded run.



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2-11

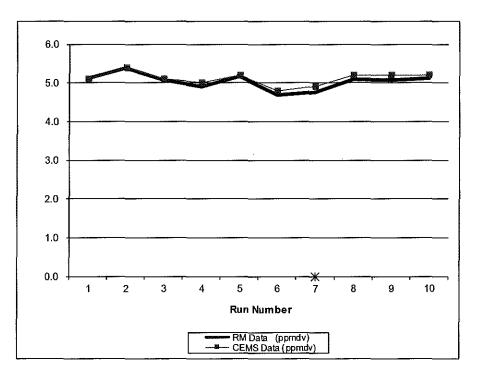
| | Table 2-10: NO _x (ppmdv) Concentration RATA (EPA 7E / PS2) | | | | | | | | |
|------------|--|----------------|--------------------|----------------------|-----------------------|-----------------------|--|--|--|
| Run No. | Start Time | Date (2016) | RM Data (ppmdv) | CEMS Data (ppmdv) | Difference (ppmdv) | Difference Percent | | | |
| 1 | 12:36 | Mar 18 | 5.1 | 5.1 | 0.0 | 0.3% | | | |
| 2 | 13:09 | Mar18 | 5.4 | 5.4 | 0.0 | -0.4% | | | |
| 3 | 13:57 | Mar18 | 5.1 | 5.1 | 0.0 | -0.8% | | | |
| 4 | 14:30 | Mar18 | 4.9 | 5.0 | -0.1 | -2.0% | | | |
| 5 | 15:05 | Mar 18 | 5.2 | 5.2 | 0.0 | -0.9% | | | |
| 6 | 15:36 | Mar 18 | 4.7 | 4.8 | -0.1 | -2.4% | | | |
| 7 * | 16:14 | Mar 18 | 4.8 | 4.9 | -0.1 | -2.9% | | | |
| 8 | 16:46 | Mar 18 | 5.1 | 5.2 | -0.1 | -2.4% | | | |
| 9 | 17:17 | Mar 18 | 5.1 | 5.2 | -0.1 | -2.8% | | | |
| 10 | 17:57 | Mar 18 | 5.1 | 5.2 | -0.1 | -1.6% | | | |
| / | Average | | 5.1 | 5.1 | -0.1 | -1.4% | | | |
| | | | Relative Acc | uracy Test Audi | t Results | | | | |

| Relative Accuracy (as % of R | M) 2.2% | 20.0% | |
|----------------------------------|----------------|-------|--|
| | | Limit | |
| t-Value for 9 Data Se | ets 2.306 | | |
| Confidence Coefficient (C | C) 0.039643 | | |
| Standard Deviation of Difference | es 0.051575 | | |

RM = Reference Method (CleanAir Data)

041316 163038

CEMS = Continuous Emissions Monitoring System (Air Products Data) RATA calculations are based on 9 of 10 runs.* indicates the excluded run.



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RESULTS

2-12

| Run No. | Start Time | Date (2016) | RM Data (Ib/MMBtu) | CEMS Data (Ib/MMBtu) | Difference (Ib/MMBtu) | Difference Percent |
|------------|---------------|----------------|-----------------------|-------------------------|--------------------------|-----------------------|
| 1 * | 12:36 | Mar 18 | 0.007 | 0.006 | 0.001 | 19.3% |
| 2 | 13:09 | Mar 18 | 0.008 | 0.007 | 0.001 | 11.8% |
| 3 | 13:57 | Mar 18 | 0.007 | 0.006 | 0.001 | 19.2% |
| 4 | 14:30 | Mar 18 | 0.007 | 0.006 | 0.001 | 14.3% |
| 5 | 15:05 | Mar 18 | 0.007 | 0.007 | 0.000 | 5.7% |
| 6 | 15:36 | Mar 18 | 0.007 | 0.006 | 0.001 | 9.8% |
| 7 | 16:14 | Mar 18 | 0.007 | 0.006 | 0.001 | 12.7% |
| 8 | 16:46 | Mar 18 | 0.007 | 0.007 | 0.000 | 3.0% |
| 9 | 17:1 7 | Mar 18 | 0.007 | 0.007 | 0.000 | 3.2% |
| 10 | 17:57 | Mar 18 | 0.007 | 0.007 | 0.000 | 5.1% |
| | Average | | 0.007 | 0.007 | 0.001 | 9.4% |

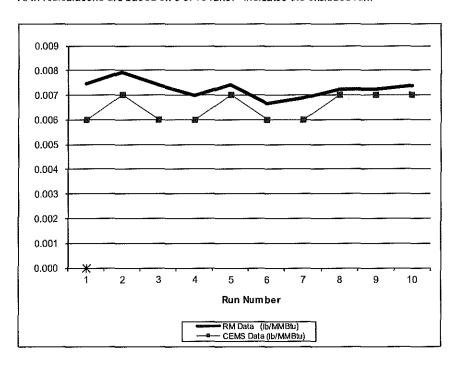
Relative Accuracy Test Audit Results

| Standard Deviation of Differences | 0.000408 | |
|--|----------|-------|
| Confidence Coefficient (CC) | 0.000314 | |
| t-Value for 9 Data Sets | 2.306 | |
| | | Limit |
| Relative Accuracy (as % of RM) | 13.8% | 20.0% |
| Relative Accuracy (as % of Appl. Std.) | 7.7% | 10.0% |
| Appl. Std. = 0.013 lb/MMBtu | | |

RM = Reference Method (CleanAir Data)

042516 154653

CEMS = Continuous Emissions Monitoring System (Air Products Data) RATA calculations are based on 9 of 10 runs, * indicates the excluded run,



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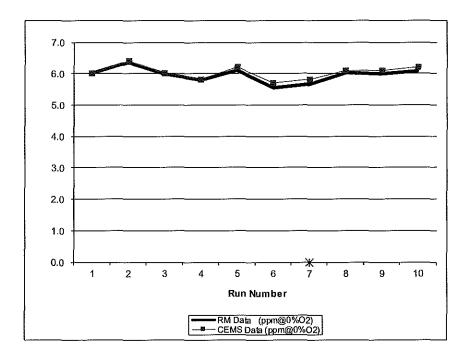
| Run | Start | Date | RM Data | CEMS Data | TA (USEPA M- Difference | Difference |
|-----|----------|------------|------------------|----------------|----------------------------|------------|
| No. | Time | (2016) | (ppm@0%O2) | (ppm@0%O2) | (ppm@0%O2) | Percent |
| 1 | 12:36 | Mar 18 | 6.0 | 6.0 | 0.03 | 0.5% |
| 2 | 13:09 | Mar18 | 6.4 | 6.4 | -0.04 | -0.7% |
| 3 | 13:57 | Mar18 | 6.0 | 6.0 | -0.01 | -0.2% |
| 4 | 14:30 | Mar 18 | 5.8 | 5.8 | 0.00 | 0.0% |
| 5 | 15:05 | Mar 18 | 6.1 | 6.2 | -0.09 | -1.5% |
| 6 | 15:36 | Mar 18 | 5.6 | 5.7 | -0.15 | -2.6% |
| 7* | 16:14 | Mar18 | 5.7 | 5.8 | -0.15 | -2.6% |
| 8 | 16:46 | Mar 18 | 6.0 | 6.1 | -0.07 | -1.2% |
| 9 | 17:17 | Mar 18 | 6.0 | 6.1 | -0.11 | -1.8% |
| 10 | 17:57 | Mar 18 | 6.1 | 6.2 | -0.14 | -2.2% |
| | Average | 1 | 6.0 | 6.1 | -0.06 | -1.1% |
| | | | Relative A | curacy Test Au | dit Results | |
| | Standard | Deviatio | n of Differences | 0,061054 | un Nesuns | |
| | Cor | nfidence (| Coefficient (CC) | 0.046930 | | |
| | | t-Value | for 9 Data Sets | 2,306 | | |

| t-Value for 9 Data Sets | 2,306 | | |
|--|-------|-------|--|
| | | Limit | |
| Relative Accuracy (as % of RM) | 1.9% | 20.0% | |
| Relative Accuracy (as % of Appl. Std.) | 0.2% | 10.0% | |
| Appl. Std. = 60 ppm @0%O2 | | | |

RM = Reference Method (CleanAir Data)

041316 163038

CEMS = Continuous Emissions Monitoring System (Air Products Data) RATA calculations are based on 9 of 10 runs.* indicates the excluded run.



AIR PRODUCTS AND CHEMICALS, INC. DETROIT HYDROGEN PLANT

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| | CO . | (nnmdy) (| | ole 2-13: on RATA (USE | EPA M-10 / PS | 4 A) |
|---|---|--|-----------------------------------|---------------------------|-----------------------|------------------|
| Run No. | Start | Date (2016) | RM Data (ppmdv) | CEMS Data (ppmdv) | Difference (ppmdv) | <u></u> |
| 1 | 12:36 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 2 | 13:09 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 3 | 13:57 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 4 | 14:30 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 5 | 15:05 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 6 | 15:36 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 7 | 16:14 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 8 | 16:46 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 9 | 17:17 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| 10 | 17:57 | Mar 18 | 0.0 | 0.4 | -0.4 | |
| | Average | • | 0.0 | 0.4 | -0.4 | |
| | | | Relative Acc | curacy Test Aud | it Results | |
| .9 | tandard | Deviation o | fDifferences | 0.000 | | |
| | | | efficient (CC) | 0.000 | | |
| | | | 10 Data Sets | 2.262 | | |
| | | | | | Limit | |
| | | | | | | |
| EMS | Referenc = Contin | e Method (0 uous Emis | | 0.4 | 5.0 | 041316 16303 |
| CEMS | Referenc = Contin | e Method (0 uous Emis | CleanAir Data) | ng System (Air Pr | 5.0 | 041316 16303 |
| CEMS | Referenc = Contin | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 04 13 16 16 30 3 |
| CEMS | Referenc = Contin calculatio | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 04 13 16 16 30 3 |
| CEMS RATA | Reference = Contin calculation | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 04 13 16 16 30 3 |
| CEMS RATA ((| Reference = Contin calculatio | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 04 13 16 16 30 3 |
| CEMS RATA ((((| Reference = Contin calculatio | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 041316 16303 |
| CEMS RATA ((((((((((((((((()))))) | Reference = Contin calculation | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 041316 16303 |
| CEMS RATA | Reference = Contin calculation | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 041316 16303 |
| CEMS RATA ((((((((((((((((((| Reference = Contin calculation | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 041316 16303 |
| CEMS RATA ((((((((((((((((((| Reference = Contin calculation 0.5 0.4 0.4 0.3 0.3 0.2 | e Method (0 uous Emis | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 | 041316 16303 |
| CEMS RATA ((((((((((((((((((| Reference = Contin calculation 0.5 0.4 0.4 0.3 0.2 0.2 0.2 | e Method ((nuous Emis ons are bas | CleanAir Data) sions Monitorir | ng System (Air Pr | 5.0 oducts Data) | 04 13 16 16 30 3 |

AIR PRODUCTS AND CHEMICALS, INC. DETROIT HYDROGEN PLANT

Client Reference No: 4503676698 CleanAir Project No: 12915

| CO (lb/hr) Emission Rate RATA (USEPA M-10 / PS4A) Run Start Date RM Data CEMS Data Difference No. Time (2016) (lb/hr) (lb/hr) (lb/hr) 1 12:36 Mar 18 0.0 0.2 -0.2 3 13:57 Mar 18 0.0 0.2 -0.2 3 13:57 Mar 18 0.0 0.2 -0.2 5 15:05 Mar 18 0.0 0.2 -0.2 5 15:05 Mar 18 0.0 0.2 -0.2 5 15:05 Mar 18 0.0 0.2 -0.2 9 17:17 Mar 18 0.0 0.2 -0.2 Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 Confidence Coefficient (CC) 0.000 Limit Mar 18 0.4% 5.0% Appl. Std. = 56.94 lb/hr 0.4% 5.0% Appl. Std. = 50.94 lb/hr 0.4% | | | | | ole 2-14: | | |
|---|--|--|--|---|---------------------------|---------------------|------------|
| No. Time (2016) (lb/hr) (lb/hr) (lb/hr) 1 12:36 Mar 18 0.0 0.2 -0.2 2 13:09 Mar 18 0.0 0.2 -0.2 3 13:57 Mar 18 0.0 0.2 -0.2 4 14:30 Mar 18 0.0 0.2 -0.2 5 15:05 Mar 18 0.0 0.2 -0.2 6 15:36 Mar 18 0.0 0.2 -0.2 7 16:14 Mar 18 0.0 0.2 -0.2 9 17:17 Mar 18 0.0 0.2 -0.2 9 17:17 Mar 18 0.0 0.2 -0.2 Average 0.0 0.2 -0.2 -0.2 Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 Confidence Coefficient (CC) 0.000 -0.2 -0.2 Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% -0.4 Q2 | | _CO (I | lb/hr) Em | ission Rate | <u>∋ RATA (USE</u> | <u>PA M-10 / PS</u> | 4A) |
| 2 13:09 Mar 18 0.0 0.2 -0.2 3 13:57 Mar 18 0.0 0.2 -0.2 4 14:30 Mar 18 0.0 0.2 -0.2 5 15:05 Mar 18 0.0 0.2 -0.2 6 15:36 Mar 18 0.0 0.2 -0.2 7 16:14 Mar 18 0.0 0.2 -0.2 8 16:46 Mar 18 0.0 0.2 -0.2 9 17:17 Mar 18 0.0 0.2 -0.2 10 17:57 Mar 18 0.0 0.2 -0.2 Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. = 56.94 10/hr 04335 50927 Continuous Emissions Monitoring System (Air Products Data) 0.2 | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | |
| 5 15:05 Mar 18 0.0 0.2 -0.2 6 15:36 Mar 18 0.0 0.2 -0.2 7 16:14 Mar 18 0.0 0.2 -0.2 8 16:46 Mar 18 0.0 0.2 -0.2 9 17:17 Mar 18 0.0 0.2 -0.2 10 17:57 Mar 18 0.0 0.2 -0.2 Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. 5.04% 5.0% Appl. Std. 5.04% O4356 5007 EMES = Continuous Emissions Monitoring System (Air Products Data) August colspan="3">August colspan="3"August colspan="3"August colspan="3"August co | | | | | | | |
| 6 15:36 Mar 18 0.0 0.2 -0.2 7 16:14 Mar 18 0.0 0.2 -0.2 8 16:46 Mar 18 0.0 0.2 -0.2 9 17:17 Mar 18 0.0 0.2 -0.2 9 17:57 Mar 18 0.0 0.2 -0.2 Average 0.0 0.2 -0.2 Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 Confidence Coefficient (CC) 0.000 Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. = 56.94 1b/hr 0.4% 5.0% Continuous Emissions Monitoring System (Air Products Data) Attacalculations are based on all 10 runs. | | | | | | | |
| 7 16:14 Mar 18 0.0 0.2 -0.2 8 16:46 Mar 18 0.0 0.2 -0.2 9 17:17 Mar 18 0.0 0.2 -0.2 10 17:57 Mar 18 0.0 0.2 -0.2 Average 0.0 0.2 -0.2 Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 COUDO Limit Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 COUDO Limit Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. = 56.94 lb/hr O4356 5007 Continuous Emissions Monitoring System (Air Products Data) 0.2 O 0.3 O 0.4 O O | | | | | | | |
| | | | | | | | |
| 9 17:17 Mar 18 0.0 0.2 -0.2 10 17:57 Mar 18 0.0 0.2 -0.2 Average 0.0 0.2 -0.2 Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 t-Value for 10 Data Sets 2.262 Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. = 56.94 Ib/hr CM = Reference Method (Clean Air Data) CEMS = Continuous Emissions Monitoring System (Air Products Data) ATA calculations are based on all 10 runs. 0.3 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 | | | | | | | |
| 1017:57Mar 180.00.2-0.2Average0.00.2-0.2Relative Accuracy Test Audit ResultsStandard Deviation of Differences0.000Confidence Coefficient (CC)0.000LimitRelative Accuracy (as % of Appl. Std.)0.4%5.0%Appl. Std. = 56.94 lb/hrOdt336 16997CEMS = Continuous Emissions Monitoring System (Air Products Data)Continuous Emissions Monitoring System (Air Products Data)Odt336 16997Continuous Emissions Monitoring System (Air Products Data)Odt336 16997Continuous Emissions Monitoring System (Air Products Data)Odt336 16997Odt336 16997Continuous Emissions Monitoring System (Air Products Data)Odt336 16997Odt336 16997Odt33 | | | | | | | |
| Average 0.0 0.2 -0.2 Relative Accuracy Test Audit ResultsStandard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 t-Value for 10 Data Sets 2.262 LimitRelative Accuracy (as % of Appl. Std.) 0.4% Appl. Std. = 56.94 lb/hrIM= Reference Method (CleanAir Data)EMS = Continuous Emissions Monitoring System (Air Products Data)RATA calculations are based on all 10 runs.0.30.40.40.40.40.40.40.40.40.40.50.60.712345678910 | | | | | | | |
| Relative Accuracy Test Audit Results Standard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 t-Value for 10 Data Sets 2.262 Limit Relative Accuracy (as % of Appl. Std.) 0.4% Appl. Std. = 56.94 lb/hr CM= Reference Method (CleanAir Data) CM= Reference Method (CleanAir Data) CATA calculations are based on all 10 runs. | <u></u> | | · · · · · · · · · · · · · · · · · · · | | | | |
| Standard Deviation of Differences 0.000 Confidence Coefficient (CC) 0.000 I-Value for 10 Data Sets 2.262 Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. = 56.94 lb/hr RM = Reference Method (CleanAir Data) 04336 50007 EMS = Continuous Emissions Monitoring System (Air Products Data) CATA calculations are based on all 10 runs. 0.3 0.2 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 | | Average | \$ | 0.0 | 0.2 | -0.2 | |
| Confidence Coefficient (CC) 0.000 t-Value for 10 Data Sets 2.262 Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. = 56.94 lb/hr RM = Reference Method (CleanAir Data) 04336 50307 EMS = Continuous Emissions Monitoring System (Air Products Data) RATA calculations are based on all 10 runs. 0.3 0.2 0.2 0.1 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 | | | | Relative Acc | curacy Test Audi | t Results | |
| t-Value for 10 Data Sets 2.262 Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. = 56.94 lb/hr RM = Reference Method (CleanAir Data) RMTA calculations are based on all 10 runs. 0.3 0.2 0.2 0.1 0.4% 5.0% Appl. Std. = 56.94 lb/hr 0.4% 5.0% ATA calculations are based on all 10 runs. 0.3 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 | S | tandard | Deviation of | Differences | 0.000 | | |
| Limit Relative Accuracy (as % of Appl. Std.) 0.4% 5.0% Appl. Std. = 56.94 lb/hr RM = Reference Method (CleanAir Data) EMS = Continuous Emissions Monitoring System (Air Products Data) RATA calculations are based on all 10 runs. 0.3 0.2 0.4% 5.0% Appl. Std. = 56.94 lb/hr 0.4% 5.0% 0.4% 5.0% 0.4 | | Con | fidence Coe | efficient (CC) | 0.000 | | |
| Relative Accuracy (as % of Appl. Std.) Appl. Std. = 56.94 lb/hr Appl. Std. = 56.94 lb/hr Appl. Std. = 56.94 lb/hr $Appl. Std. = 56.94 lb/hrAppl. Std. = 56.94 lb/hrAppl. Std. = 56.94 lb/hr Appl. Std. = 56.94 lb/hrAppl. Std. = 56.94 lb/hr Appl. Std. = 56.94 lb/hrAppl. Std. = 56.94 lb/hrAppl. Std. = 56.94 lb/hr Appl. Std. = 56.94 lb/hrAppl. Std. = 56.94 lb/$ | | | t-Value for 1 | 10 Data Sets | 2.262 | | |
| Appl. Std. = 56.94 lb/hr M = Reference Method (CleanAir Data) EMS = Continuous Emissions Monitoring System (Air Products Data) AATA calculations are based on all 10 runs. 0.3 0.2 0.2 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 | | | | | | Limit | |
| $RA = Reference Method (CleanAir Data) 04336 50007$ $EMS = Continuous Emissions Monitoring System (Air Products Data) (Air Acalculations are based on all 10 runs).$ $0.3 \qquad 0.3 \qquad 0.2 \qquad 0.1 \qquad 0$ | Rela | tive Accu | | | | | |
| EMS = Continuous Emissions Monitoring System (Air Products Data) RATA calculations are based on all 10 runs. 0.3 0.2 0.2 0.2 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 | | ave Accu | ıracy (as % ဖ | of Appl. Std.) | 0.4% | 5.0% | |
| CATA calculations are based on all 10 runs. 0.3 0.2 0.2 0.2 0.2 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.2 0.2 0.1 0.1 0.2 0.1 | | Ap | pl. Std. = 56. | .94 lb/hr | 0.4% | 5.0% | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | Ap Referenc | pl. Std. = 56. e Method (C | .94 lb/hr CleanAir Data) | | | 041316 150 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | CEMS | Ap Reference = Contin | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | CEMS | Ap Reference = Contin | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | CEMS | Ap Reference = Contin | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 0.2 0.1 0.1 0.1 0.0 1 2 3 4 5 6 7 8 9 10 | CEMS RATA | App Reference = Contin calculatio | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 0.2 0.1 0.1 0.1 0.0 1 2 3 4 5 6 7 8 9 10 | CEMS RATA | App Reference = Contin calculatio | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 0.2 0.1 0.1 0.1 0.0 1 2 3 4 5 6 7 8 9 10 | CEMS RATA | App Reference = Contin calculatio | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| $0.1 \\ 0.1 \\ 0.0 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $ | CEMS RATA d | App Reference = Contin calculation | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| $0.1 \\ 0.1 \\ 0.0 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $ | CEMS RATA d | App Reference = Contin calculation | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| $0.1 \\ 0.1 \\ 0.0 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $ | CEMS RATA d | App Reference = Contin calculation | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| | CEMS RATA d | App Reference = Contin calculatio | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| | CEMS RATA d | App Reference = Contin calculatio | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| | CEMS RATA d | App Reference = Contin calculatio | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 0.0 1 2 3 4 5 6 7 8 9 10 | CEMS RATA d C | App Reference = Contir calculation | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 0.0 1 2 3 4 5 6 7 8 9 10 | CEMS RATA d C | App Reference = Contir calculation | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 0.0 1 2 3 4 5 6 7 8 9 10 | CEMS RATA d C | App Reference = Contir calculation | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 1 2 3 4 5 6 7 8 9 10 | | App Reference = Contin calculation 0.3 | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 1 2 3 4 5 6 7 8 9 10 | | App Reference = Contin calculation 0.3 | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| 1 2 3 4 5 6 7 8 9 10 | | App Reference = Contin calculation 0.3 | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| Run Number | | App Reference = Contin calculation | pl. Std. = 56. ce Method (C nuous Emiss | .94 lb/hr CleanAir Data) sions Monitorir | ig System (Air Pr | | 041316 150 |
| | | App Reference = Contin calculation | pl. Std. = 56. The Method (Control of the second s | 94 Ib/hr CleanAir Data) sions Monitorir ed on all 10 run | ng System (Air Pro | oducts Data) | |
| | | App Reference = Contin calculation | pl. Std. = 56. The Method (Control of the second s | 94 Ib/hr CleanAir Data) sions Monitorir ed on all 10 run | ng System (Air Pro | oducts Data) | |
| EMS Data (Ib/hr) | EMS ATA o C C O O O O | App Reference = Contin calculation | pl. Std. = 56. The Method (Control of the second s | 94 Ib/hr CleanAir Data) sions Monitorir ed on all 10 run | ng System (Air Pro ns. | oducts Data) | |

End of Section 2 - Results