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Particulate Matter Test

EUBOILER1

Consumers Energy Company J.H. Campbell Plant 17000 Croswell Street West Olive, Michigan 49460 SRN: B2835 FRS: 110000411108

Test Dates: August 2 and 3, 2016

September 23, 2016

Test Performed by the Consumers Energy Company Regulatory Compliance Testing Section – Air Emissions Testing Body Laboratory Services Section Work Order No. 27538841 Revision 0

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TABLE OF CONTENTS

Execu	ative Summary	. iv
1.0	Introduction	1
1.1	Contact Information	2
2.0	Summary of Results	4
2.1	Operating Data	4
2.2	Applicable Permit Information	5
2.3	Results	5
3.0	Source Description	7
3.1	Process	7
3.2	Process Flow Sheet	7
3.3	Materials Processed	8
3.4	Rated Capacity	8
3.5	Process Instrumentation	9
4.0	Sampling and Analytical Procedures	10
4.1	Description of Sampling Train and Field Procedures	10
4.1.	1 Sample Location and Traverse Points	11
4.1.	2 Velocity and Temperature	12
4.1.	3 Molecular Weight	14
4.1.	4 Moisture Content	16
4,1.	5 Emission Rates (USEPA Method 19)	16
4.1.	6 Particulate Matter	17
5.0	Test Results and Discussion	22
5.1	Variations and Upset Conditions	22
5.2	Air Pollution Control Device Maintenance	22
5.3	Field Quality Assurance / Quality Control Procedures	22
5.3.	1 Volumetric Flowrate QA/QC Checks	25
5.3.	2 Dry Gas Meter QA/QC Checks	25



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RENEWABLE OPERATING PERMIT REPORT CERTIFICATION

Authorized by 1994 P.A. 451, as amended. Failure to provide this information may result in civil and/or criminal penalties.

Reports submitted pursuant to R 336.1213 (Rule 213), subrules (3)(c) and/or (4)(c), of Michigan's Renewable Operating Permit (ROP) program must be certified by a responsible official. Additional information regarding the reports and documentation listed below must be kept on file for at least 5 years, as specified in Rule 213(3)(b)(ii), and be made available to the Department of Environmental Quality, Air Quality Division upon request. Source Name Consumers Energy, J.H. Campbell Plant County Ottawa Source Address 17000 Croswell West Olive City ROP No. MI-ROP-B2835-2013a ROP Section No. 1 AQD Source ID (SRN) B2835 Please check the appropriate box(es): Annual Compliance Certification (Pursuant to Rule 213(4)(c)) То Reporting period (provide inclusive dates): From 1. During the entire reporting period, this source was in compliance with ALL terms and conditions contained in the ROP, each term and condition of which is identified and included by this reference. The method(s) used to determine compliance is/are the method(s) specified in the ROP. 2. During the entire reporting period this source was in compliance with all terms and conditions contained in the ROP, each term and condition of which is identified and included by this reference, EXCEPT for the deviations identified on the enclosed deviation report(s). The method used to determine compliance for each term and condition is the method specified in the ROP. unless otherwise indicated and described on the enclosed deviation report(s). Semi-Annual (or More Frequent) Report Certification (Pursuant to Rule 213(3)(c)) Reporting period (provide inclusive dates): From То 1. During the entire reporting period, ALL monitoring and associated recordkeeping requirements in the ROP were met and no deviations from these requirements or any other terms or conditions occurred. 2. During the entire reporting period, all monitoring and associated recordkeeping requirements in the ROP were met and no deviations from these requirements or any other terms or conditions occurred, EXCEPT for the deviations identified on the enclosed deviation report(s). Other Report Certification Reporting period (provide inclusive dates): From NA То NA Additional monitoring reports or other applicable documents required by the ROP are attached as described: Particulate Matter compliance stack test report for the MATS regulation for Unit 1, as required by 40 CFR Part 63.10031(f).

I certify that, based on information and belief formed after reasonable inquiry, the statements and information in this report and the supporting enclosures are true, accurate and complete

Norman J. Kapala	Site Business Manager	616-738-3200
Name of Responsible Official (print or type)	Title	Phone Number
Kmt Apola		7/29/2016
Signature of Responsible Official		Date

* Photocopy this form as needed.

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EXECUTIVE SUMMARY

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Consumers Energy Company (Consumers Energy) Regulatory Compliance Testing Section (RCTS) completed particulate matter (PM) testing at the single dedicated exhaust duct of coalfired boiler EUBOILER1 (Unit 1) in operation at the J.H. Campbell Generating Station located in West Olive, Michigan. The purpose of the test program was to demonstrate qualification as a Low Emitting Electric Generating Unit (LEE) for filterable particulate matter (FPM) per 40 CFR 63, Subpart UUUUU – National Emission Standards for Hazardous Air Pollutants: Coal- and Oil-fired Electric Utility Steam Generating Units (aka Mercury Air Toxics Rule [MATS]). Secondarily, the test program provides a direct comparison between USEPA Method 5 PM results and MATS 5 PM results.

The FPM LEE demonstration requires quarterly sampling over a period of three calendar years. The results of each quarterly test must be less than or equal to 50 percent of the applicable FPM standard listed in Table 2 of the MATS Rule, equating to 0.015 lb/mmBtu. The test program was conducted on August 2 and 3, 2016 in accordance with applicable requirements and sampling, calibration, and quality assurance procedures specified in 40 CFR 60, Appendix A, reference methods (RM) 1, 2, 3A, 4, 5, 19 and MATS method 5. Three 125-minute RM5 tests were performed in sequence with three 125-minute MATS5 tests to measure filterable while the boiler was operating under maximum normal operating load. The results are summarized in the following table.

Run	PM Concentration (gr/dscf)		PM Emission Rate (lb/mmBtu)		late
Kun -	Res	Results		Results	
-	RM5	MATS5	RM5	MATS5	FPM Limit
1	0.00144	0.00134	0.0031	0.0028	-
2	0.00108	0.00124	0.0022	0.0026	
3	0.00113	0.00132	0.0020	0.0021	-
Average	0.00121	0.00130	0.0024	0.0026	0.015

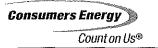
Summary of Results

Each individual run, as well as the average of the three runs, was below the MATS LEE emission rate limit of 0.015 pounds of particulate matter per million British thermal unit heat

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input. The average deviation between the two test method results was also found to be less than ten percent. Detailed results are presented in the PM Results Summary tables at the end of this

Example calculations and calculation data sheets are presented in Appendix A and B. Laboratory data is presented in Appendix B.



1.0 INTRODUCTION

Consumers Energy Company (Consumers Energy) Regulatory Compliance Testing Section (RCTS) completed particulate matter (PM) testing at the single dedicated exhaust duct of coalfired boiler EUBOILER1 (Unit 1) in operation at the J.H. Campbell Generating Station located in West Olive, Michigan. The purpose of the test program was to demonstrate qualification as a Low Emitting Electric Generating Unit (LEE) for filterable particulate matter (FPM) per 40 CFR 63, Subpart UUUUU – National Emission Standards for Hazardous Air Pollutants: Coal- and Oil-fired Electric Utility Steam Generating Units (aka Mercury Air Toxics Rule [MATS]). This test event also fulfills an EPA request to provide a direct comparison between USEPA Reference Method 5 (RM5) PM results and MATS 5 PM results at the source in order to utilize RM5 as the compliance test method for the MATS rule.

The FPM LEE demonstration requires quarterly sampling over a period of three calendar years. The results of each quarterly test must be less than or equal to 50 percent of the applicable FPM standard listed in Table 2 of the MATS Rule (see Table 1-1 below), equating to 0.015 lb/mmBtu. The particulate emission limitations from MATS are presented in Table 1-1 below.

Table 1-1MATS Rule PM Emission Limit

EGU Subcategory	Pollutant Being Sampled	Emission Limit
Existing Unit, Coal-fired not low rank virgin coal	Filterable Particulate Matter	0.030 lb/mmBtu

The test program was conducted on August 2 and 3, 2016 in accordance with applicable requirements and sampling, calibration, and quality assurance procedures specified in 40 CFR 60, Appendix A, reference methods 1, 2, 3A, 4, 5, 19 and MATS Method 5. As requested by EPA in order to utilize RM5 (in lieu of MATS 5) for PM Compliance, three 125-minute RM5 tests were performed in sequence with three 125-minute MATS5 tests to measure filterable while the boiler was operating under maximum normal operating load.

Consumers Energy	J.H. Campbell EUBOILER1 MATS PM Test Report
· · · · · · · · · · · · · · · · · · ·	Regulatory Compliance Testing Section
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1.1 CONTACT INFORMATION

Figure 1-1 presents the test program organization, major lines of communication, and names and phone numbers of responsible individuals. Table 1-2 presents contact information for these individuals.

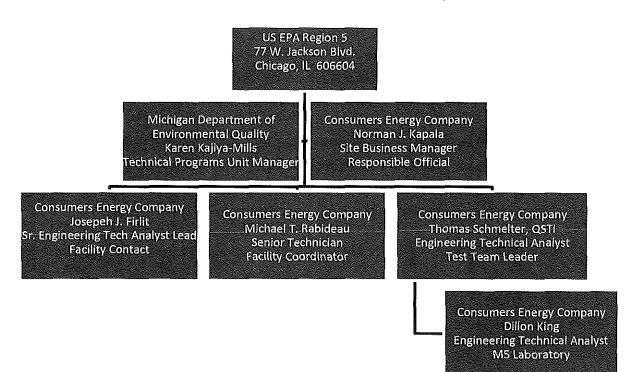


Figure 1-1. Test Program Organization

Table 1-2
Contact Information

Program Role	Contact	Address
EPA Consent Decree Contact	Director, Air Division	U.S. EPA Region 5 77 W. Jackson Blvd. (AE-17J) Chicago, IL 60604
Regulatory Agency Representative	Ms. Karen Kajiya-Mills Technical Programs Unit Manager 517-335-4874 <u>kajiya-millsk@michigan.gov</u>	Michigan Department of Environmental Quality Technical Programs Unit 525 W. Allegan, Constitution Hall, 2 nd Floor S Lansing, Michigan 48933



Table 1-2

Contact Information

Program Role	Contact	Address
Responsible Official Test Facility	Mr. Norman J. Kapala 616-738-3200 Site Business Manager <u>Norman.Kapala@emsenergy.com</u> Mr. Joseph J. Firlit 616-738-3260 Sr. Engineering Tech Analyst Lead	Consumers Energy Company J. H. Campbell Power Plant 17000 Croswell Street West Olive, Michigan 49460 Consumers Energy Company J. H. Campbell Power Plant 17000 Croswell Street
Test Facility	<u>Joseph Firlit@cmsenergy.com</u> Mr. Michael T. Rabideau 616-738-3273 Senior Technician Michael.Rabideau@cmsenergy.com	West Olive, Michigan 49460 Consumers Energy Company J. H. Campbell Power Plant 17000 Croswell Street West Olive, Michigan 49460
Test Team Representative	Mr. Thomas Schmelter, QSTI 616-738-3334 Engineering Technical Analyst <u>Thomas.Schmelter@cmsenergy.com</u>	Consumers Energy Company L&D Training Center 17010 Croswell Street West Olive, Michigan 49460
Laboratory	Mr. Dillon King, QSTI 989-891-5585 Engineering Technical Analyst <u>Dillon.King@cmsenergy.com</u>	Consumers Energy Company Karn-Weadock ESD Trailer #4 2742 N. Weadock Highway Essexville, MI 48732

2.0 SUMMARY OF RESULTS

2.1 OPERATING DATA

Unit 1 has a nominally rated heat input capacity of 2,490 mmBtu/hr and can generate a gross electrical output of approximately 274 megawatts, while firing western subbituminous coal.

During the performance test, the boiler was operated at maximum normal operating load conditions. 40 CFR 63.10007(2) states the maximum normal operating load is generally between 90 and 110 percent of design capacity but should be representative of site specific normal operations. The performance testing was performed while the boiler was operating within the range of 247 MW to 301 MW. A summary of the boiler gross megawatt (MW) electrical generation during each test is provided in Tables 2-1 and 2-2. Refer to Attachment D for detailed operating data.

Table	2-1
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Summary of Boiler Operating Data - MATS Method 5

Date	Run	Sampling Time (EDT)	Boiler (MW)
August 2, 2016	1	11:28 to 13:49	278
August 2, 2016	2	17:20 to 19:30	278
August 3, 2016	3	11:05 to 13:16	278
22 <u>+ </u>		Average	278

Table 2-2

Summary of Boiler Operating Data – Reference Method 5

Date	Run	Sampling Time (EDT)	Boiler (MW)
August 2, 2016	1	8:20 to 10:48	272
August 2, 2016	2	14:48 to 17:00	277
August 3, 2016	3	8:20 to 10:42	277
		Average	276

2.2 APPLICABLE PERMIT INFORMATION

The J.H. Campbell generating station has the State of Michigan Registration Number (SRN) B2835 and operates in accordance with air permit MI-ROP-B2835-2013a. The air permit incorporates federal regulations and reports under Federal Registry System (FRS) identification number 110000411108. EUBOILER1 is the emission unit source identification in the permit and included in the FGBOILER12 flexible group. Incorporated within the permit are the applicable requirements of 40 CFR 63, Subpart UUUUU – National Emission Standards for Hazardous Air Pollutants: Coal- and Oil-fired Electric Utility Steam Generating Units.

In addition to the state issued air permit, Consumers Energy operates Unit 1 in accordance with the requirements in Consent Decree (CD), Civil Action No.: 14-13580, entered between Consumers Energy, the United States Environmental Protection Agency (EPA), and the United States Department of Justice (DOJ) on November 4, 2014. Section VI. of the Consent Decree presents the PM Emission Reduction and Control requirements applicable to the J.H. Campbell Unit 1 boiler and pollution control devices.

The regulatory enforceable particulate matter emissions limits for this source are summarized in Table 2-3.

PM Emission Limit	Units	Applicable Requirement
0.030	lb/mmBtu	Table 2 to Subpart UUUUU of Part 63—
		Emission Limits for Existing EGU's
0.015	lb/mmBtu	Consent Decree Paragraph 144
0.16	lb/1,000 lbs exhaust gas,	MI-ROP-B2835-2013a Section C;
	corrected to 50% excess air	EUBOILER1 Emission Unit Conditions

Table 2-3

EUBOILER1 Regulatory PM Emission Limits

lb/mmBtu: pound of filterable particulate matter per million British thermal unit heat input

2.3 RESULTS

As shown in Table 2-4 below, each individual run, as well as the average of the three runs, was below the MATS LEE emission rate limit of 0.015 pounds of particulate matter per million British thermal unit heat input. Detailed results are presented in the PM Results Summary table at the end of this report.



Run		centration dscf)	PM Emission Rate (lb/mmBtu)		
Kun -	Res	sults	Results MA		MATS5 LEE
	RM5	MATS5	RM5	MATS5	FPM Limit
1	0.00144	0.00134	0.0031	0.0028	
2	0.00108	0.00124	0.0022	0.0026	-
3	0.00113	0.00132	0.0020	0.0021	-
Average	0.00121	0.00130	0.0024	0.0026	0.015

Table 2-4

Summary of Results

It should be noted that the RM 5 results are compared to the MATS emission limit to evaluate compliance, as approved by EPA. Also, it should be noted that results are less than 50% of the MATS FPM emission limit (0.030 lb/mmBtu) and this test will be used to qualify for Low Emitting EGU (LEE) status in the future. Example calculations and calculation data sheets are presented in Appendix A and B. Laboratory data is presented in Appendix B.

3.0 SOURCE DESCRIPTION

The approximate 274 megawatt (MW) gross output Unit 1 electric utility steam generating unit (EGU) is a coal-fired boiler that generates steam to turn a turbine connected to an electricity producing generator.

3.1 PROCESS

Unit 1 is a dry bottom tangentially-fired boiler constructed in 1958 which combusts pulverized sub-bituminous coal as the primary fuel and oil as an ignition/flame stabilization fuel. The source classification code (SCC) is 10100226. Campbell Unit 1 first began providing electricity in 1962. Coal is fired in the furnace where the combustion heats boiler tubes containing water producing steam. The steam is used to turn an engine turbine that is connected to an electricity producing generator. The electricity is routed through the transmission and distribution system to consumers.

3.2 PROCESS FLOW SHEET

The flue gas generated through coal combustion is controlled by multiple pollution control devices. The unit is currently equipped with low nitrogen oxides (NO_x) burners and over fire air (OFA) for NO_x control, an activated carbon injection (ACI) system for mercury (Hg) reduction, a dry sorbent (lime) injection (DSI) system for control of sulfur dioxides (SO₂) and other acid gasses, and a pulse jet fabric filter (PJFF) baghouse to control particulate matter emissions. Refer to Figure 3-1 for the Unit 1 Data Flow Diagram.

As the air enters the PJFF baghouse manifold it is evenly distributed into 8 compartments each containing 1,176 fabric filter bags. A total of 9,408 bags that are 29 feet 6 inches in length are used. Once the gas enters the compartments the velocity decreases and large particles fall out of suspension and are collected within the bottom ash hopper. As the flue gas passes through the fabric filters suspended particles are collected on the exterior surface of the bags. The particles are removed by pulsing clean air through the interior of the bags. The jet of air flexes and reverses the direction of airflow through the bag causing the particles to be released and collected in a hopper below. The clean air exiting the PJFF system enters induced draft fans and is exhausted through a header duct prior to being exhausted to atmosphere through a common approximate 400-feet high stack, shared with EUBOILER2.

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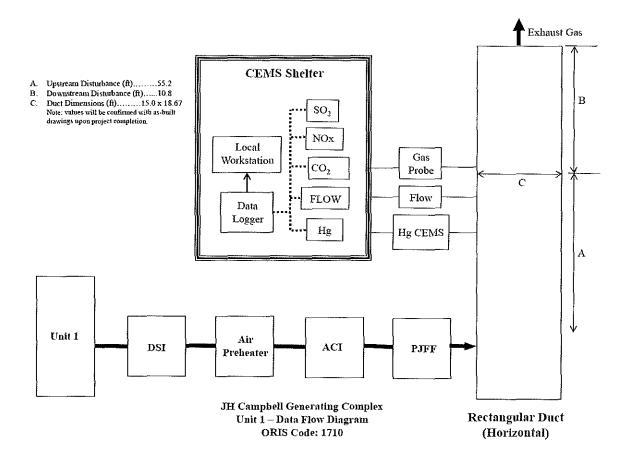


Figure 3-1. Unit 1 Data Flow Diagram

3.3 MATERIALS PROCESSED

Sub-bituminous coal is combusted in the boiler producing heat and steam that is used for electricity generation. The coal arrives via railcar from various mines located in the Western United States. The boiler is classified as a coal-fired unit not firing low rank virgin coal as described in Table 2 to Subpart UUUUU.

3.4 RATED CAPACITY

Unit 1 has a nominally rated heat input capacity of 2,490 mmBtu/hr and can generate a gross electrical output of approximately 274 megawatts. The boiler operates in a continuous manner in order to meet the electrical demands of Midcontinent Independent System Operator, Inc. (MISO)

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and a second	Regulatory Compliance Testing Section
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and Consumers Energy customers. EUBOILER1 is considered a baseload unit because it is designed to operate 24 hours a day, 365 days a year.

During the performance tests, the boiler was operated at maximum normal operating load conditions. 40 CFR 63.10007(2) states the maximum normal operating load will be generally between 90 and 110 percent of design capacity but should be representative of site specific normal operations.

3.5 PROCESS INSTRUMENTATION

The process was continuously monitored by boiler operators and environmental technicians. Due to the various instrumentation systems, the sampling times were correlated to instrumentation times. The continuous emissions monitoring systems records data on Eastern Standard Time (EST). Primary process variables recorded by unit instrumentation are summarized in Table 3-1. Refer to Appendix D for detailed operating data.

Parameter	Run 1	Run 2	Run 3	Average	
Reference Method 5			· · · · · · · · · · · · · · · · · · ·		
6-minute Opacity (%)	0	0	0	0	
Boiler load (MW)	2.72	277	277	276	
Heat input rate	2,705.6	3,024.7	2,811.3	2,847.2	
(mmBtu/hr)					
MATS Method 5					
6-minute Opacity (%)	0	0	0	0	
Boiler load (MW)	278	2.78	278	278	
Heat input rate	2,944.7	2,997.5	2,895.3	2,945.8	
(mmBtu/hr)					

Table 3-1 Summary of Process Instrumentation Data

4.0 SAMPLING AND ANALYTICAL PROCEDURES

Consumers Energy tested for filterable particulate matter using the United States Environmental Protection Agency (USEPA) test methods presented in Table 4-1. Descriptions of the sampling and analytical procedures are presented in the following sections.

Parameter	USEPA			
	Method	Title		
Sampling location	1	Sample and Velocity Traverses for Stationary Sources		
Traverse points	2	Determination of Stack Gas Velocity and Volumetric		
		Flow Rate (Type S Pitot Tube)		
Molecular weight	3A	Determination of Oxygen and Carbon Dioxide		
$(O_2 \text{ and } CO_2)$		Concentrations in Emissions from Stationary Sources		
		(Instrumental Analyzer Procedure)		
Moisture	4	Determination of Moisture Content in Stack Gases		
Filterable particulate	5	Determination of Particulate Matter Emissions from		
matter		Stationary Sources		
Filterable particulate	MATS 5 ^a	Determination of Particulate Matter Emissions from		
matter		Stationary Sources (with a front half filter temperature of		
		320±25°F)		
Emission rate	19	Determination of Sulfur Dioxide Removal Efficiency and		
	-	Particulate Matter, Sulfur Dioxide, and Nitrogen Oxide		
		Emission Rates		

Table 4-1 Test Methods

^a Table 5 to Subpart UUUUU of Part 63-Performance Testing Requirements notes the Method 5 front half temperature shall be 320±25°F

4.1 DESCRIPTION OF SAMPLING TRAIN AND FIELD PROCEDURES

The test matrix presented in Table 4-2 summarizes the sampling and analytical methods performed for the specified parameters during this test program.

Table 4-2

Test Matrix

Sampling	No.	Sample/Type	Sampling	Sampling	Sample	Analytical	Analytical
Location	of	Pollutant	Method	Organization	Run	Method	Laboratory
	Runs				Time		
					(min)		
EUBOILER1	3	Sample	Ml	Consumers	+	Field	Consumers
Outlet duct		location and		Energy		measurement	Energy
		traverse points				and area	
						calculations	
		Velocity and	M2	Consumers	125	Velocity head	Consumers
		volumetric		Energy		and temperature	Energy
		flowrate				measurements	
		Molecular	M3A	Consumers	125	Paramagnetic	Consumers
		weight (O ₂		Energy	1	and infrared	Energy
		and CO ₂)				analyzers	
		Moisture	M4	Consumers	125	Gravimetric	Consumers
				Energy			Energy
	3	Filterable	M5	Consumers	125	Gravimetric	Consumers
		particulate		Energy			Energy
		matter					
	3	Filterable	MATS 5	Consumers	125	Gravimetric	Consumers
		particulate		Energy			Energy
		matter					
	3	Emission rate	M19	Consumers	-	Stoichiometric	Consumers
				Energy		calculation	Energy

4.1.1 Sample Location and Traverse Points

The number and location of traverse points for determining exhaust gas velocity and volumetric air-flow was determined in accordance with USEPA Method 1, *Sample and Velocity Traverses for Stationary Sources*. Five test ports are located in the horizontal plane on one side of the common 15 feet by 18 feet 8-inch rectangular duct. The duct has an equivalent duct diameter of 16 feet 7.6 inches. The ports are situated:

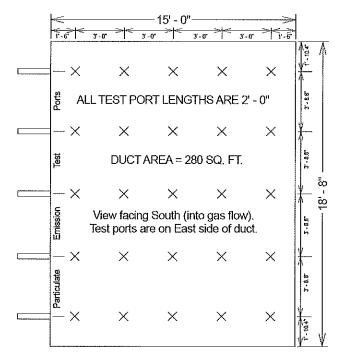
• Approximately 55.2 feet or 3.3 duct diameters downstream of a sound deadening silencer flow disturbance, and

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Count on Us®	September 23, 2016

• Approximately 10.8 feet or 0.6 duct diameters upstream of flow disturbance caused by a curve in the duct as it enters the exhaust stack.

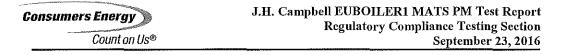
The sample ports are 6-inches in diameter and extend 2 feet beyond the stack wall. The area of the exhaust duct was calculated and the cross-section divided into a number of equal rectangular areas based on distances to air flow disturbances. Flue gas was sampled for four minutes at five traverse points from the five sample ports for a total of 25 sample is presented as Figures 4-1.

Figure 4-1. Unit 1 Duct Cross Section and Test Port/Traverse Point Detail



4.1.2 Velocity and Temperature

The exhaust gas velocity and temperature were measured using USEPA Method 2, *Determination of Stack Gas Temperature and Velocity (Type S Pitot Tube).* The pressure differential (ΔP) across the positive and negative openings of the Pitot tube inserted in the exhaust duct at each traverse point were measured using an "S Type" (Stauscheibe or reverse type) Pitot tube connected to an appropriately sized oil filled inclined manometer. Exhaust gas temperatures were measured using a chromel/alumel "Type K" thermocouple and a temperature indicator. Refer to Figure 4-2 for the Method 2 Pitot tube and thermocouple configuration.



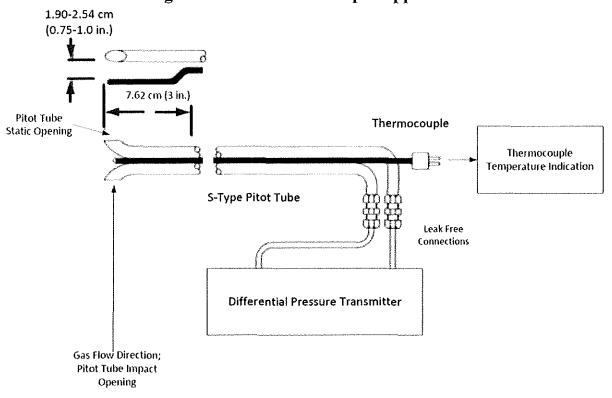


Figure 4-2. Method 2 Sample Apparatus

Flue gas velocity and velocity vector measurements (cyclonic flow evaluation) were measured following the procedures in USEPA Method 2 at the sampling location. Cyclonic flow is defined as a flow condition with an average null angle greater than 20 degrees. The direction of flow can be determined by aligning the Pitot tube to obtain zero (null) velocity head reading—the direction would be parallel to the Pitot tube face openings or perpendicular to the null position. By measuring the angle of the Pitot tube face openings in relation to the stack walls when a null angle is obtained, the direction of flow is measured. If the absolute average of the flow direction angles is greater than 20 degrees, the flue gas is considered to be cyclonic at that sampling location and an alternative location should be found. The cyclonic flow measurements are summarized in Table 4-3.

	Traverse Point Null Angle (°)						
Sample Port	5 (far wall)	4	3	2	1 (near wall)	Average	
A (Bottom)	2	0	0	0	0	0.4	
В	2	8	2	2	2	3.2	
С	5	5	3	8	0	4.2	
D	2	3	3	3	3	2.8	
E (Top)	2	0	0	2	3	1.4	
Average	3	3	2	3	2	2.4	

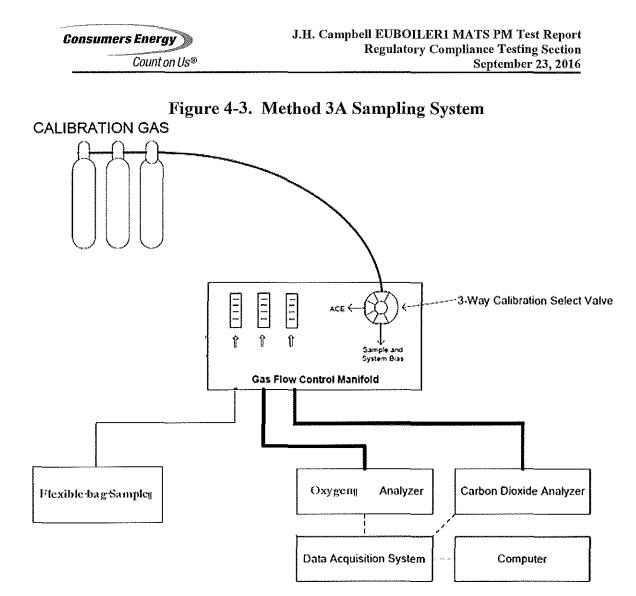
Table 4-3Cyclonic Flow Measurements

The average Pitot tube null angle measured was 2.4 degrees indicating an acceptable sampling location. Refer to Appendix B for Data Sheets documenting the cyclonic flow evaluation.

4.1.3 Molecular Weight

The exhaust gas composition and molecular weight was measured using the sampling and analytical procedures of USEPA Method 3A, *Determination of Oxygen and Carbon Dioxide Concentrations in Emissions from Stationary Sources (Instrumental Analyzer Procedure)*. The flue gas oxygen and carbon monoxide concentrations were used to calculate molecular weight, flue gas velocity, and emissions in lb/mmBtu and lb/1,000 lbs corrected to 50% excess air.

Flue gas was extracted from the stack through a heated stainless steel lined probe and Teflon® sample line into a flexible sample bag. The sample was withdrawn from the flexible bag and conveyed through a gas conditioning system to remove water content before entering paramagnetic and infrared gas analyzers that measure oxygen and carbon monoxide concentrations. Figure 4-3 depicts the Method 3A sampling system.



Prior to sampling flue gas, the analyzers were calibrated by performing a calibration error test where zero-, mid-, and high-level calibration gases are introduced to the back of the analyzers. The calibration error check was performed to evaluate if the analyzers response was within $\pm 2.0\%$ of the calibration gas span. A system-bias and drift test was performed where the zero-and mid- or high- calibration gases are introduced at the inlet to the gas conditioner to measure the ability of the system to respond to within ± 5.0 percent of span.

In lieu of performing a stratification test, the flexible bag samples were collected throughout the particulate matter tests at each of the 25 traverse points.

At the conclusion of each test run, an additional system bias check was performed to evaluate the drift from the pre- and post-test system bias checks. The system-bias checks evaluated if the

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and the second	Regulatory Compliance Testing Section
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analyzers drift is within the allowable criterion of $\pm 3.0\%$ of span from pre- to post-test system bias checks. The measured oxygen and carbon dioxide concentrations were corrected for analyzer drift. Refer to Appendix E for analyzer calibration supporting documentation.

4.1.4 Moisture Content

The exhaust gas moisture content was determined using USEPA Method 4, *Determination of Moisture in Stack Gases* in conjunction with the Method 5 sample apparatus. The sampled gas was pumped through a series of impingers immersed in an ice bath to condense water in the flue gas. The amount of water condensed and collected in the impingers was measured gravimetrically and used to calculate the exhaust gas moisture content.

4.1.5 Emission Rates (USEPA Method 19)

USEPA Method 19, Determination of Sulfur Dioxide Removal Efficiency and Particulate Matter, Sulfur Dioxide, and Nitrogen Oxide Emission Rates, was used to calculate PM emission rates in units of lb/mmBtu. Measured oxygen concentrations and F factors (ratios of combustion gas volumes to heat inputs) were used to calculate emission rates using equation 19-1 from the method. Figure 4-4 presents the emissions calculation used:

Figure 4-4. USEPA Method 19 Equation 19-1

$$E = C_{d}F_{d} \frac{20.9}{(20.9 - \%O_{2d})}$$

Where:

Е	Ξ	Pollutant emission rate (lb/mmBtu)
C_d	=	Pollutant concentration, dry basis (lb/dscf)
F_d	=	Volumes of combustion components per unit of heat content
		9,820 dscf/mmBtu for subbituminous coal from 40 CFR 75, Appendix F,
		Table 1
O_{2d}	_	Concentration of oxygen on a dry basis (%, dry)

Refer to Appendix A for example calculations.

Consumers Energy Count on Us®	J.H. Campbell EUBOILER1 MATS PM Test Report Regulatory Compliance Testing Section September 23, 2016
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4.1.6 Particulate Matter

Filterable particulate matter samples were collected isokinetically by withdrawing a sample of the flue gas through a filter following the procedures of (1) USEPA Method 5, *Determination of Particulate Matter Emissions from Stationary Sources*, and (2) MATS 5.

USEPA Method 5 measures filterable particulate matter (aka PM, FPM) collected on a filter heated to 248±25°F, while MATS 5 measures PM at a filter temperature of 320±25°F.

In a letter received from USEPA on April 12, 2016 in response to a February 10, 2016 request by Consumers Energy, USEPA has approved the use of USEPA Method 5 as an alternative to MATS 5 in order to avoid having to conduct compliance tests using multiple test methods. The approval was granted with the following limitation:

In order to have data directly comparing M5 to MATS M5 at your facility, we request that you perform three additional test runs using MATS M5 during the next scheduled PM compliance test on Units 1 and 2 at Campbell. These three additional MATS M5 runs are to be conducted simultaneously with three of the required M5 runs. Please submit the data from these three simultaneous MATS M5 test runs, along with a copy of the required certification report, including the testing performed using M5, to Ms. Kim Garnett of my staff.

Pursuant to USEPA's conditional approval, two particulate matter sampling trains were employed for this test program, consisting of a Method 5 sampling train and a MATS Method 5 sampling train. However, due to the sampling location configuration, RM5 and MATS 5 runs were performed in sequence rather than being simultaneous, meaning one run was with a USEPA Method 5 sample train, with the next run utilizing the MATS 5 sampling train, and so forth, for a total of 6 runs, 3 with MATS5 and 3 with RM5.

With the exception of the impinger configuration, the MATS 5 and the Method 5 are setup and operated similarly. The flue gas was passed through a nozzle, heated probe, quartz-fiber filter, and into a series of impingers with the configurations presented in Table 4-4. The filter collects filterable particulate matter while the impingers collect water vapor. Figure 4-5 depicts the USEPA Method 5/MATS 5 sampling train.

J.H. Campbell EUBOILER1 MATS PM Test Report
Regulatory Compliance Testing Section
September 23, 2016

	Methou 5/MA15 5 Impinger Contguration							
Impinger Order (Upstream to Downstream)	Impinger Type	Impinger Contents	Amount (gram)					
1	Modified	Water	100					
2	Greenburg-Smith	Water	100					
3	Modified	Empty	0					
4	Modified	Silica gel desiccant	~200-300					

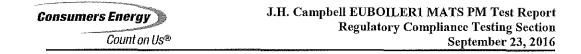
Table 4-4Method 5/MATS 5 Impinger Configuration

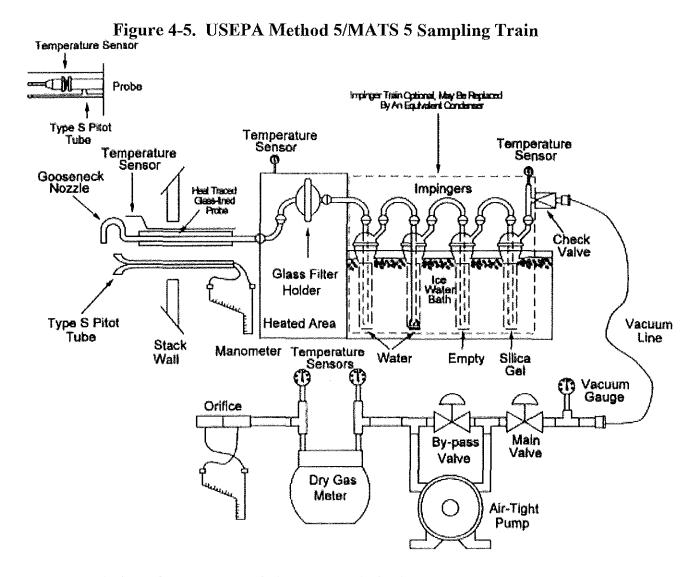
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Prior to testing, representative velocity head and temperature data from a recently performed high load relative accuracy test audit (RATA) was reviewed to calculate an ideal nozzle diameter that would allow isokinetic sampling to be performed. The diameter of the selected nozzle was measured with a micrometer across three cross-sectional chords and used to calculate the cross-sectional area. Prior to testing the nozzle was rinsed and brushed with deionized water and acetone, and connected to the sample probe.

The impact and static pressure openings of the Pitot tube were leak-checked at or above a velocity head of 3.0 inches of water for a minimum of 15 seconds. The sampling trains were leak-checked by capping the nozzle tip and applying a vacuum of approximately 15 inches of mercury. The dry-gas meter was monitored for approximately 1 minute to verify the sample train leakage rate is less than 0.02 cubic foot per minute (cfm). The sample probe will then be inserted into the sampling port to begin sampling. Ice was placed around the impingers and the probe, and filter temperatures were allowed to stabilize to a temperature of $248\pm25^{\circ}F$ before sampling, as applicable. After the desired operating conditions were coordinated with the facility, testing was initiated. Stack and sampling apparatus parameters (e.g., flue velocity head, temperature) were monitored to calculate and sample at the isokinetic rate within 100 ± 10 % for the duration of the test. Refer to Appendix B for field data sheets.





At the conclusion of a test run and the post-test leak check, the sampling apparatus was disassembled and the impingers and filter housing were transported to the recovery area.

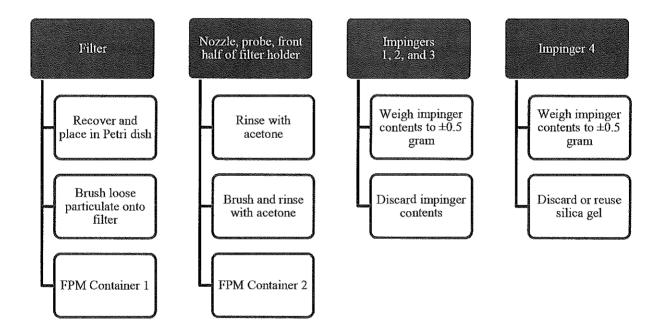
The filter was recovered from the filter housing and placed in a Petri dish, sealed with Teflon tape, and labeled as "FPM Container 1." The nozzle and probe liner, and the front half of the filter housing were triple rinsed with acetone to collect particulate matter. The acetone rinses were collected in pre-cleaned sample containers, sealed with Teflon tape, and labeled as "FPM Container 2." The weight of liquid collected in each impinger, including the silica gel impinger, was measured using an electronic scale; these weights were used to calculate the moisture

Consumers Energy	J.H. Campbell EUBOILER1 MATS PM Test Report
	Regulatory Compliance Testing Section
Count on Us®	September 23, 2016

content of the sampled flue gas. The contents of the impingers were discarded. Refer to Figure 4-6 for the USEPA Method 5 sample recovery scheme.

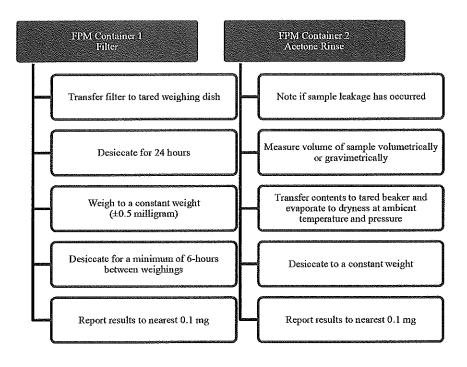
The sample containers, including a filter and acetone blank were transported to the laboratory for analysis. The sample analysis followed USEPA Method 5 procedures as summarized in the analytical scheme presented in Figure 4-7. Refer to Appendix C for laboratory data sheets.

Figure 4-6. USEPA Method 5/MATS 5 Sample Recovery Scheme



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Figure 4-7. USEPA Method 5/MATS 5 Analytical Scheme



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5.0 TEST RESULTS AND DISCUSSION

The purpose of the test program was to demonstrate qualification as a Low Emitting Electric Generating Unit (LEE) for filterable particulate matter (FPM) per 40 CFR 63, Subpart UUUUU – National Emission Standards for Hazardous Air Pollutants: Coal- and Oil-fired Electric Utility Steam Generating Units (aka Mercury Air Toxics Rule [MATS]). This test event also fulfills an EPA request to provide a direct comparison between USEPA Reference Method 5 (RM5) PM results and MATS 5 PM results at the source in order to utilize RM5 as the compliance test method for the MATS rule. Three 125-minute tests were performed following USEPA procedures for each test method. The results of the testing in comparison to MATS emission limits are presented in Table 2-4.

Each individual run, as well as the average of the three runs, was below the MATS LEE emission rate limit of 0.015 pounds of particulate matter per million British thermal unit heat input.

Detailed results are presented in the Reference Method 5 PM Results Summary and MATS 5 PM Results Summary behind the tables tab of this report.

5.1 VARIATIONS AND UPSET CONDITIONS

No sampling procedure or boiler operating condition variations that could have affected the results were encountered during the test program. The process and control equipment were operating under routine conditions and no upsets were encountered.

5.2 AIR POLLUTION CONTROL DEVICE MAINTENANCE

No significant PJFF air pollution control device maintenance had occurred during the three months prior to the testing. Optimization of the air pollution control devices is a continuous process to ensure compliance with regulatory emission limits.

5.3 FIELD QUALITY ASSURANCE / QUALITY CONTROL PROCEDURES

The USEPA reference methods performed state reliable results are obtained by persons equipped with a thorough knowledge of the techniques associated with each method. To that end, factors with the potential to cause measurement errors are minimized by implementing quality control

Consumers Energy	J.H. Campbell EUBOILER1 MATS PM Test Report
	Regulatory Compliance Testing Section
Count on Us®	September 23, 2016

(QC) and assurance (QA) programs into the applicable components of field testing. QA/QC components are included in this test program. Table 5-1 summarizes the primary field quality assurance and quality control activities that were performed. Refer to Appendix E for supporting documentation.



Table 5-1

QA/QC Procedures

QA/QC Activity	Purpose	Procedure	Frequency	Acceptance Criteria	QA/QC Met
M1: Sampling Location	Evaluate if the sampling location is suitable for sampling	Measure distance from ports to downstream and upstream flow disturbances	Pre-test	\geq 2 diameters downstream; \geq 0.5 diameter upstream.	Yes
M1: Duct diameter/ dimensions	Verify area of stack is accurately measured	Review as-built drawings and field measurement	Pre-test	Field measurement agreement with as- built drawings	Yes
M1: Cyclonic flow evaluation	Evaluate the sampling location for cyclonic flow	Measure null angles	Pre-test	<u>≤20°</u>	Yes
M2: Pitot tube inspection	Verify Pitot and thermocouple assembly is free of aerodynamic interferences	Inspection	Pre-test and post-test	Refer to Section 6.1 and 10.0 of USEPA Method 2	Yes
M2: Pitot tube leak check	Verify leak free sampling system	Apply minimum pressure of 3.0 inches of H_2O to Pitot tube	Pre-test and Post-test	± 0.01 in H ₂ O for 15 seconds at minimum 3.0 in H ₂ O velocity head	Yes
M3A: Calibration gas standards	Ensure accurate calibration standards	Traceability protocol of calibration gases	Pre-test	Calibration gas uncertainty ≤2.0%	Yes
M3A: Calibration Error	Evaluates operation of analyzers	Calibration gases introduces directly into analyzers	Pre-test	±2.0% of the calibration span	Yes
M3A: System Bias and Analyzer Drift	Evaluates ability of sampling system to delivery stack gas to analyzers	Calibration gases introduced at sample probe tip, heated sample line, and into analyzers	Pre-test and Post-test	$\pm 5.0\%$ of the analyzer calibration span for bias and $\pm 3.0\%$ of analyzer calibration span for drift	Yes
M5: nozzle diameter measurements	Verify nozzle diameter used to calculate sample rate	Measure inner diameter across three cross-sectional chords	Pre-test	3 measurements agree within ±0.004 inch	Yes
M5: sample rate	Ensure representative sample collection	Calculate isokinetic sample rate	During and post-test	100±10% isokinetic rate	Yes
M5: sample volume	Ensure sufficient sample volume is collected	Record pre- and post- test dry gas meter volume reading	Post test	≥1.70 dscm	Yes
M5: post-test leak check	Evaluate if the sample was affected by system leak	Cap sample train; monitor dry gas meter	Post-test	≤0.020 cfm	Yes
M5: post-test meter audits	Evaluates accurate measurement equipment for sample volume	DGM pre- and post- test; compare calibration factors (Y and Y _{ga})	Pre-test Post-test	±5 %	Yes

5.3.1 Volumetric Flowrate QA/QC Checks

The S-Type Pitot tube used to measure flue gas velocity head pressures was inspected prior to and after emissions testing. The Pitot tube met the specifications of Section 6.1 of USEPA Method 1. Refer to Appendix E for the Pitot tube inspection and certification sheet.

The S-Type Pitot tube and oil-filled incline manometer assembly were evaluated for leaks prior to testing. Testing was performed with leak free assembly. Refer to field data sheets for verification of Pitot tube leak checks.

5.3.2 Dry Gas Meter QA/QC Checks

Table 5-2 summarizes the dry-gas meter calibration checks in comparison to the acceptable USEPA tolerance. Refer to Appendix E for complete DGM calibrations.

Dry- Gas Meter	Pre-test DGM Calibration Factor (Y) (dimensionless)	Post-Test DGM Calibration Check Value (Y _{qa}) (dimensionless)	Difference Between Pre- and Post-test DGM Calibrations (%)	Acceptable Tolerance (%)	Comment
2034	0.999	1.02	-2.3	5	Valid

Table 5-2Dry-gas Meter Calibration QA/QC Audit

5.3.3 Thermocouple QA/QC Checks

Temperature measurements using thermocouples and digital pyrometers were compared to a reference temperature (i.e., ice water bath, boiling water) to evaluate accuracy of the equipment. The thermocouples and pyrometers measured temperature within $\pm 1.5\%$ of the reference temperatures and were within USEPA acceptance criteria. Thermocouple calibration sheets are presented at the bottom of Table 1 after the Tables tab of this report.

5.3.4 Nozzle QA/QC Checks

Prior to testing a micrometer was used to separately measure three different inner diameters of the nozzle. The average of the measurements was used to calculate the sampling velocity and

Consumers Energy	J.H. Campbell EUBOILER1 MATS PM Test Report
	Regulatory Compliance Testing Section
Count on Us®	September 23, 2016

isokinetic sampling rate. The nozzle was inspected for nicks, dents, or corrosion before connecting to the sample probe. Refer to Appendix E for the nozzle calibration sheet.

5.3.5 Oxygen and Carbon Dioxide Analyzer QA/QC Checks

The instrument analyzer sampling apparatus described in Section 4.1 were audited for measurement accuracy and data reliability. The analyzers passed the applicable calibration criteria. The following tables summarize gas cylinders used during this test program and QA/QC audits. Refer to Appendix E for additional calibration data.

Table 5-3				
Calibration Gas Cylinder Information				

Parameter	Gas Vendor	Cylinder Serial Number	Cylinder Value (%)	Expiration Date
N ₂	Airgas	EB0013140	99.9995	2/18/2023
O ₂	Airgas	VC022854D	8.882	9/23/2023
CO ₂		XC033854B	9.837	
O ₂	Airgas	00000100	20.11	1/5/2023
CO ₂		CC220123	19.04	

Table 5-4
Method 3A O ₂ Sampling Train QA/QC Audits

Parameter	Run 1	Run 2	Run 3	Acceptable Tolerance	Comment
Calibration error (%)	≤0.8	≤0.8	≤1.2	±2% of calibration span	Valid
Low-level (zero) gas system bias (%)	0.3	0.3	0.3	≤5% of calibration span	Valid
Upscale gas system bias (%)	0.8	0.8	1.2	≤5% of calibration span	Valid
Low-level (zero) gas analyzer drift (%)	0.3	0.3	0.7	≤3% of calibration span	Valid
Upscale gas analyzer drift (%)	0.2	0.2	0.1	≤3% of calibration span	Valid



Parameter	Run 1	Run 2	Run 3	Acceptable Tolerance	Comment	
Calibration error (%)	≤0.8	≤0.8	≤1.5	±2% of calibration span	Valid	
Low-level (zero) gas system bias (%)	0.6	0.6	0.7	\leq 5% of calibration span	Valid	
Upscale gas system bias (%)	0.1	0.1	0.6	≤5% of calibration span	Valid	
Low-level (zero) gas analyzer drift (%)	0.2	0.2	0.2	\leq 3% of calibration span	Valid	
Upscale gas analyzer drift (%)	1.1	1.1	0.4	≤3% of calibration span	Valid	

Table 5-5Method 3A CO2 Sampling Train QA/QC Audits

5.3.6 QA/QC Blanks

Reagent, field train recovery, and field train proof blanks were analyzed for the parameters of interest. The results of the blanks are presented in the Table 5-6.

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Table 5-6

QA/QC Blanks

Sample Identification	Result (mg)	Comment
Method 5 Acetone Field Blank	0.9	Sample volume was 200 milliliters. Acetone blank corrections were applied.
Method 5 Laboratory Filter Blank	0.1	Reporting limit is 0.1 milligrams.

5.4 LABORATORY QUALITY ASSURANCE / QUALITY CONTROL PROCEDURES

Laboratory quality assurance and quality control procedures were performed in accordance with USEPA Method 5 guidelines. Specific QA/QC procedures include evaluation of reagent and filter blanks and the application of blank corrections, if applicable. Refer to Appendix C for the laboratory data sheets.



6.0 CERTIFICATION

I hereby certify the statements and information in this test report and supporting enclosures are true, accurate, and complete, and the test program was performed in accordance with test methods specified in this report.

Brian C. Pape, QSTI Senior Engineering Technical Analyst Lead Laboratory Services – Regulatory Compliance Testing Section

Report prepared by:

Dillon A. King, QSTI Engineering Technical Analyst I Laboratory Services – Regulatory Compliance Testing Section

Report reviewed by:

Kathryn M. Cunningham Senior Engineer II

Environmental Services - Air Quality Section

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Table

Reference Metho	pliance Testing od 5 PM Results S				
Facility and Source Information					
Customer:	J.H. Campbell				
Source:	EUBOILER1		Unit Load:	l Hig	
Work Order:			32205		
Date:	8/2/2016	8/2/2016	8/3/2016		
Stack Length, inches:	224	224	224		
Stack Width, inches:	180	180	180		
Stack Area, Square Feet:	280.00	280.00	280.00	Ĺ	
Source Pollutant Test Data	Run 1	Run 2	Run 3	Avera	
Barometric Pressure, inches mercury:	29.50	29.50	29.50	29.5	
Meter Calibration Factor:	0.999	0.999	0,999	0.99	
Pitot Tube Calibration Factor:	0.84	0.84	0.84	0.84	
Stack Static Pressure, inches water:	2.50	2.50	2.50	2.50	
Nozzle Diameter, inches:	0.281	0.281	0.281	0.28	
Run Start Time:	8:20	14:48	8:20		
Run Stop Time:	10:43	16:55	10:37	405	
Duration of Sample, minutes:	125	125	125	125	
Meter Leak Rate, ft3/min:	0.000	0.000	0.000	0.00	
Meter Start Volume, cf:	931.81	191.58	465.24	529.5	
Meter Final Volume, cf:	1058.93	326,69	596.31	660.6	
Average Meter Pressure, inches water:	3.57	3.92	3.72	3.74	
Average Meter Temperature, degrees F:	81,9	91.1	83.5	85.5	
Average Square Root Pitot Pressure, inches water:	0.9556 333.0	1.0022	0.9796	0.979	
Stack Gas Temperature, degrees F:					
Source Moisture Data	Run 1	Run 2	Run 3	Avera	
Liquid Volume Collected, grams:	301.4	404.6	339.2	348.4	
Water Vapor Volume at STP, scf:	14.211	19.077	15.993	16.42	
Meter Volume, Actual Cubic Feet:	127.119	135.114	131.077	131.1	
Meter Volume, STP, dscf:	123.0	128.7	126.5	126.0	
Meter Volume, STP, dscm:	3.484	3,645	3.583	3.57	
Total Gas Sampled, scf:	137.24	147.78	142.53 11.22	142.5	
Percent Stack Gas Moisture:	10.35 Run 1	12.91			
Gas Analysis Data		Run 2	Run 3	Avera 42.0	
Percent Carbon Dioxide, dry:	<u>11.49</u> 7.19	<u>13.04</u> 6.70	15.09	13.2	
Percent Oxygen, dry:		80.26	4.70 80.21	6.20 80.6	
Percent Nitrogen:	81.32				
Dry Molecular Weight, Ib/Ib-Mole:	30.125	30.354	30.602 29.188	30.36 28.9	
Molecular Weight, at Stack Condition, lb/lb-Mole: Calculated Fuel Factor, F _o :	28.870	28.759	1.074	28.9	
Fuel F-Factor, Fd:	9820	9820	9820	9820	
Percent Excess Air:	50.35	46.28	28,50	41.7	
	Run 1	46.20 Run 2	<u> 20.00 </u> Run 3	41.7 Avera	
Gas Calculations					
Density Dry at STP, lb/cf:	0.0779	0.0785	0.0791	0.078	
Density Wet at STP (68 deg. F, 29.92 in. Hg), lb/cf:	0.0746	0.0743	0.0755	0.07	
Density Wet at Stack Cond, lb/cf:	0.0493	0.0482	0.0499	0.04	
Pounds of Gas Sampled, Dry:	9.5821	10.1000	10.0110 10.7547	9.89	
Pounds of Gas Sampled, Wet:					
Gas Volumetric Flow Rate Data	Run 1	Run 2	Run 3	Avera	
Average Stack Gas Velocity, ft/s:	66.0	70.0	67.3	67.8	
Stack Gas Flow Rate, ACFM:	1,108,947	1,176,835	1,130,315	1,138,6	
Stack Gas Flow Rate, SCFM:	732,281	761,929	746,768	746,9	
Stack Gas Flow Rate, DSCFM:	656,455	663,573	662,972	661,00	
Percent of Isokinetic Sampling Rate:	97.5	100.9	99.3	99.2	
Gas Concentrations and Emission Rates	Run 1	Run 2	Run 3	Avera	
Filterable PM Weight, mg:	11.47	8.98	9,26	9.90	
Filterable PM, gr/dscf:	0.00144	0.00108	0.00113	0.001	
Filterable PM, lb/hr:	8.09	6.13	6.41	6.88	
	1 0 0024	0.0022	0,0020	0.002	
Filterable PM, Ib/mmBtu:	0.0031				
Filterable PM, lb/mmBtu: Filterable PM, lb/1000 lb gas flow: Filterable PM, lb/1000 lb Gas Flow @ 50% Excess Air:	0.002	0.002	0.002	0.002	

Dry Gas Metering System Calibration Check ¹	Run 1	Run 2	Run 3	Average
Dry Gas Meter Calibration Factor (Y _d):	0.999	0.999	0.999	0.999
Y _{ga} (calculated):	1.03	1.02	1.01	1.02
Assigned Δ H (@ 0.75 SCFM) of the meter system:	1.83	1.83	1.83	1.83
Allowable Y _{ga} (+/-) percent:	5.00	5.00	5.00	5.00
Actual Y _{ds} Deviation, percent:	-2,83	-2.04	-1.41	-2.10
Dry Gas Metering System Thermocouple Calibration Check ²	Reference, °F	Module, °F	Difference	Requirement
Stack	74	74	0	±2° F
Probe	74	74	0	±2° F
-ilter	74	74	0	±2° F
Dryer	74	74	0	±2° F
Auxillary	74	74	0	±2° F

MATS Method 5	PM Summary Au	Services dit Sheet			
Facility and Source Information					
Customer:	J.H. Campbell				
Source:	EUBOILER1		Unit Load:	High	
Vork Order:	0/0/0040		32205		
Date:	8/2/2016 224	8/2/2016 224	8/3/2016 224		
Stack Width, inches:	180		180		
Stack Area, Square Feet:	280.00	280,00	280.00		
Source Pollutant Test Data	Run 1		Run 3	Average	
Barometric Pressure, inches mercury:	29,50	29,50	29,50	29.50	
Aeter Calibration Factor:	0,999	0.999	0.999	0,999	
Pitot Tube Calibration Factor:	0.84	0.84	0.84	0.84	
Stack Static Pressure, inches water:	2.50	2.50	2.50	2.50	
lozzle Diameter, inches:	0.281	0.281	0.281	0.281	
Run Start Time:	11:28	17:20	11:05		
Run Stop Time:	13:49	19:30	13:16		
Duration of Sample, minutes:	125	125	125	125	
/leter Leak Rate, ft3/min:	0.000	0.000	0.000	0.000	
Aeter Start Volume, cf:	61.16	327.42	596.79	328.46	
Neter Final Volume, cf:	190,43	464.67	729.26	461.46	
werage Meter Pressure, inches water:	3.66	4.08	3.74	3.82	
verage Meter Temperature, degrees F:	89.1	93,3	92.8	91.7	
werage Square Root Pitot Pressure, Inches water:	0.9710	1.0274	0.9795	0.9926	
stack Gas Temperature, degrees F:	346,8	353.4	343.9	348.0	
Source Moisture Data	Run 1	Run 2	Run 3	Average	
iquid Volume Collected, milliliters:	0.0	0.0	0.0	0.0	
iquid Volume Collected, grams:	302.7	343.6	335.9	327.4	
Vater Vapor Volume at STP, scf:	14.272	16.201	15.838	15.437	
Aeter Volume, Actual Cubic Feet:	129.272	137.252	132.474	132,999	
Meter Volume, STP, dscf:	123.5	130.3	125.7	126.51	
Ieter Volume, STP, dscm: otal Gas Sampled, scf:	3.498	3.689 146.46	3,561 141,58	3.58 141.94	
Percent Stack Gas Moisture:	10.36	11.06	11.19	10.87	
Gas Analysis Data	Run 1	Run 2	Run 3	Average	
ercent Carbon Dioxide, dry:	12.27	13,10	14.25	13,20	
Percent Oxygen, dry:	6.80	6.62	4.89	6.10	
Percent Nitrogen:	80.94	80.28	80,86	80.69	
Dry Molecular Weight, Ib/Ib-Mole:	30.234	30,361	30,475	30.357	
Iolecular Weight, at Stack Condition, Ib/Ib-Mole:	28.967	28,993	29.080	29.01	
Calculated Fuel Factor, Fo:	1.150	1.090	1.124	1.121	
uel F-Factor, F _d :	9820	9820	9820	9820	
ercent Excess Air:	46.65	45,43	29.71	40,60	
Gas Calculations	Run 1	Run 2	Run 3	Average	
Pensity Dry at STP, lb/cf:	0.0782	0.0785	0.0788	0.0785	
ensity Wet at STP (68 deg. F, 29.92 in. Hg), lb/cf:	0.0749	0,0750	0.0752	0.075	
ensity Wet at Stack Cond, lb/cf:	0.0486	0.0483	0.0490	0.049	
ounds of Gas Sampled, Dry:	9,6541	10.2245	9,9073	9.929	
Pounds of Gas Sampled, Wet:	10.3178	10.9778	10.6438	10.646	
Gas Volumetric Flow Rate Data	Run 1	Run 2	Run 3	Average	
verage Stack Gas Velocity, ft/s:	67.5	71.7	67.9	69.1	
tack Gas Flow Rate, ACFM:	1,134,701	1,205,033	1,140,426	1,160,053	
tack Gas Flow Rate, SCFM:	736,471	775,735	742,801	751,669	
tack Gas Flow Rate, DSCFM:	660,182	689,928 98.2	659,711	669,940	
ercent of Isokinetic Sampling Rate: Gas Concentrations and Emission Rates	97.3 Run 1		99.2 Run 3	98.23	
		Run 2		Average	
ilterable PM Weight, mg:	10.76	10.49	10.78	10,67	
ilterable PM, gr/dscf:	0.00134	0.00124	0.00132	0.00130	
ilterable PM, ibs/hr:	7.60	7.35	7.48	7.48	
ilterable PM, lb/mmBtu: ilterable PM, lb/1000 lb gas flow:	0.0028	0,0026	0.0024	0.0026	
ilterable PM, ib/1000 lb Gas Flow @ 50% Excess Air;	0.002	0.002	0.002	0.002	
ilterable PM, ib/1000 Lb Gas Flow @ 50% Excess Air:	33.31	32,18	32.75	32.75	

MATS Method 5 PI Dry Gas Metering System Calibration Check	Run 1	Run 2	Run 3	T A
				Average
Dry Gas Meter Calibration Factor (Y _d):	0.999	0.999	0.999	0.999
Y _{qa} (calculated):	1.03	1.03	1.02	1.02
Assigned Δ H (@ 0.75 SCFM) of the meter system:	1.83	1.83	1.83	1.83
Allowable Y _{ga} (+/-) 5%:	5.00	5.00	5.00	5.00
Actual Yds Deviation, %:	-2.78	-2.62	-1.62	-2.34
Dry Gas Metering System Thermocouple Calibration Check	Reference, °F	Module, °F	Difference	Requirement
Stack	74	74	0	±2° F
Probe	74	74	0	±2° F
ilter	74	74	0	±2° F
Dryer	74	74	0	±2° F
Auxillary	74	74	0	±2° F