Report of...

# Boiler MACT Emission Sampling

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Performed for the...

# Michigan Sugar Company

## Sebewaing Michigan

on the

## Wet ESP Exhaust

February 7-9, 2017

Project #: 022.42

By...

Network Environmental, Inc. Grand Rapids, MI



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### AIR QUALITY DIV.

#### I. INTRODUCTION

Network Environmental, Inc. was retained by the Michigan Sugar Company of Bay City, Michigan, to perform emission sampling at their Sebewaing, Michigan facility. The purpose of the sampling was to determine compliance with the National Emission Standard for Hazardous Air Pollutants (NESHAP) 40CFR Part 63 Subpart DDDDD (MACT for Industrial, Commercial, Institutional Boilers and Process Heaters). The following is a list of the compounds sampled and corresponding emission limits:

Compounds Sampled	Emission Limit :
Carbon Monoxide (CO)	160 PPM @ 3% O <sub>2</sub> or 0.14 Lbs/MMBTU of Steam Output
Particulate	4.0 E-02 Lbs/MMBTU of Heat Input <b>or</b> 4.2 E-02 Lbs/MMBTU of Steam Output
Mercury (Hg)	5.7 E-06 Lbs/MMBTU of Heat Input <b>or</b> 6.4 E-06 Lbs/MMBTU of Steam Output
Hydrochloric Acid (HCl)	2.2 E-02 Lbs/MMBTU of Heat Input <b>or</b> 2.5 E-02 Lbs/MMBTU of Steam Output

The test methods used were as follows:

- Carbon Monoxide (CO) U.S. EPA Method 10
- Particulate & Mercury (Hg) U.S. EPA Method 29 (combined with U.S. EPA Method 5)
- Hydrochloric Acid (HCl)) U.S. EPA Method 26A
- Oxygen (O<sub>2</sub>) & Carbon Dioxide (CO<sub>2</sub>) U.S. EPA Methods 3 & 3A
- Exhaust Gas Parameters (air flow rate, temperature, moisture & density) U.S. EPA Methods 1-4

The sampling was performed over the period of February 7-9, 2017 by Stephan K. Byrd, Richard D. Eerdmans and David D. Engelhardt of Network Environmental, Inc. Assisting with the sampling were Mr. Steven Smock and the operating staff of the facility. Mr. Tom Gasloli and Ms. Sharon LeBlanc of the Michigan Department of Environmental Quality (MDEQ) - Air Quality Division were present to observe the sampling and source operation.

#### **II. PRESENTATION OF RESULTS**

#### II.1 TABLE 1 PARTICULATE EMISSION RESULTS SUMMARY WET ESP EXHAUST MICHIGAN SUGAR COMPANY SEBEWAING, MICHIGAN FEBRUARY 8-9, 2017

			Air Flow Rate	Particulate Mass Emission Rate			
Sample	Date	Time	DSCFM <sup>(1)</sup>	Lbs/Hr <sup>(2)</sup> Lbs/MMBTU Heat Input <sup>(3)</sup>		Lbs/MMBTU Steam Output <sup>(4)</sup>	
1	2/8/17	13:42-16:20	48,526	6.65	4.77E-02	4.39E-02	
2	2/9/17	10:10-13:58	50,328	9.06	6.20E-02	6.35E-02	
3	2/9/17	14:53-17:29	51,076	2.16	1.74E-02	1.48E-02	
	Average	9	49,977	5.96	4.23E-02	4.07E-02	

(1) DSCFM = Dry Standard Cubic Feet Per Minute (STP = 68 °F & 29.92 in. Hg)

(2) Lbs/Hr = Pounds of Particulate Per Hour

(3) Lbs/MMBTU Heat Input = Pounds Per Million BTU of Heat Input (Calculated Using U.S. EPA Method 19 With An F-Factor of 9,780 DSCF/MMBTU)

(4) Lbs/MMBTU Steam Output = Pounds Per Million BTU of Steam Output (Calculated Using 151.58 MMBTU/Hr Of Steam Production For Sample One, 142.66 MMBTU/Hr Of Steam Production For Sample Two and 145.87 MMBTU/Hr Of Steam Production For Sample Three.)

(5) Particulate Emission Limit From Part 63 Subpart DDDDD = 4.0E-02 Lbs/MMBTU Of Heat Input <u>OR</u> 4,2E-02 Lbs/MMBTU Of Steam Output

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#### II,2 TABLE 2 **CARBON MONOXIDE (CO)** EMISSION RESULTS SUMMARY WET ESP EXHAUST MICHIGAN SUGAR COMPANY SEBEWAING, MICHIGAN FEBRUARY 8, 2017

		Air Flow	CO Concentration		CO Mass Emission Rate		
Sample	Time	Rate DSCFM <sup>(1)</sup>	PPM <sup>(2)</sup>	PPM @ 3 %O <sub>2</sub> <sup>(3)</sup>	Lbs/Hr <sup>(4)</sup>	Lbs/MMBTU Heat Input <sup>(5)</sup>	Lbs/MMBTU Steam Output <sup>(6)</sup>
1	08:58-09:58		103.8	193.5	22.01	0.161	0.142
2	10:13-11:54	48,773	92.1	171.7	19.53	0.143	0,124
3	12:05-13:09		76.9	143.4	16.31	0.119	0.111
	Average		90.9	169.6	19.28	0.141	0.126

(1) DSCFM = Dry Standard Cubic Feet Per Minute (STP = 68 °F & 29.92 in. Hg). Average of Two (2) Flows Measured on 2/8/17

(2) PPM = Parts Per Million (v/v) On A Dry Basis

(3) PPM @ 3  $\%O_2$  = Parts Per Million (v/v) On A Dry Basis Corrected To 3 Percent Oxygen

(4) Lbs/Hr = Pounds of CO Per Hour

(5) Lbs/MMBTU Heat Input = Pounds Per Million BTU of Heat Input (Calculated Using U.S. EPA Method 19 With An F-Factor of 9,780 DSCF/MMBTU)

(6) Lbs/MMBTU Steam Output = Pounds Per Million BTU of Steam Output (Calculated Using 154.55 MMBTU/Hr Of Steam Production For Sample One, 157.43 MMBTU/Hr Of Steam Production For Sample Two and 146.91 MMBTU/Hr Of Steam Production For Sample Three.)

(7) CO Emission Limit From Part 63 Subpart DDDDD = 160 PPM @ 3 %O2 OR 0.14 Lbs/MMBTU Of Steam Output

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#### II.3 TABLE 3 MERCURY (Hg) EMISSION RESULTS SUMMARY WET ESP EXHAUST MICHIGAN SUGAR COMPANY SEBEWAING, MICHIGAN FEBRUARY 8-9, 2017

			Air Flow Rate	Hg Mass Emission Rate			
Sample	Date	Time	DSCFM <sup>(1)</sup>	Lbs/Hr <sup>(2)</sup>	Lbs/MMBTU Heat Input <sup>(3)</sup>	Lbs/MMBTU Steam Output <sup>(4)</sup>	
1	2/8/17	13:42-16:20	48,526	8.06E-05	5.77E-07	5.32E-07	
2	2/9/17	10:10-13:58	50,328	1.11E-04	7.56E-07	7.75E-07	
3	2/9/17	14:53-17:29	51,076	1.01E-04	8.12E-07	6.92E-07	
	Average		49,977	9.74E-05	7.15E-07	6.66E-07	

(1) DSCFM = Dry Standard Cubic Feet Per Minute (STP = 68 °F & 29.92 in. Hg)

(2) Lbs/Hr = Pounds of Particulate Per Hour

(3) Lbs/MMBTU Heat Input = Pounds Per Million BTU of Heat Input (Calculated Using U.S. EPA Method 19 With An F-Factor of 9,780 DSCF/MMBTU)

(4) Lbs/MMBTU Steam Output = Pounds Per Million BTU of Steam Output (Calculated Using 151.58 MMBTU/Hr Of Steam Production For Sample One, 142.66 MMBTU/Hr Of Steam Production For Sample Two and 145.87 MMBTU/Hr Of Steam Production For Sample Three.)

(5) Hg Emission Limit From Part 63 Subpart DDDDD = 5.7E-06 Lbs/MMBTU Of Heat Input <u>OR</u> 6.4E-06 Lbs/MMBTU Of Steam Output

#### II.4 TABLE 4 HYDROCHLORIC ACID (HCI) EMISSION RESULTS SUMMARY WET ESP EXHAUST MICHIGAN SUGAR COMPANY SEBEWAING, MICHIGAN FEBRUARY 7, 2017

	Air Flow	HCI	HCI Mass Emission Rate			
Sample Time	Rate DSCFM <sup>(1)</sup>	Concentration Mg/M <sup>3 (2)</sup>	Lbs/Hr <sup>(3)</sup>	Lbs/MMBTU Heat Input <sup>(4)</sup>	Lbs/MMBTU Steam Output <sup>(5)</sup>	
1 09:56-11:09	49,181	0.404	0.0744	4.77E-04	4.56E-04	
2 12:03-13:14	50,739	0.182	0.0347	2.33E-04	2.26E-04	
3 13:43-14:55	50,647	0.140	0.0265	1.88E-04	1.84E-04	
Average	50,189	0.242	0.0452	2.99E-04	2.89E-04	

(1) DSCFM = Dry Standard Cubic Feet Per Minute (STP = 68 °F & 29.92 in. Hg)

(2) Mg/M<sup>3</sup> = Milligrams Per Dry Standard Cubic Meter

(3) Lbs/Hr = Pounds of HCl Per Hour

(4) Lbs/MMBTU Heat Input = Pounds Per Million BTU of Heat Input (Calculated Using U.S. EPA Method 19 With An F-Factor of 9,780 DSCF/MMBTU)

(5) Lbs/MMBTU Steam Output = Pounds Per Million BTU of Steam Output (Calculated Using 163.20 MMBTU/Hr Of Steam Production For Sample One, 153.51 MMBTU Of Steam Production For Sample Two and 143.96 MMBTU Of Steam Production For Sample Three.)

(6) HCl Emission Limit From Part 63 Subpart DDDDD ) = 2.2E-02 Lbs/MMBTU Of Heat Input <u>OR</u> 2.5E-02 Lbs/MMBTU Of Steam Output

#### **III. DISCUSSION OF RESULTS**

The results of the emission sampling are summarized in Tables 1 through 4 (Sections II.1 through II.4). The results are presented as follows:

#### **III.1** Particulate

Table 1 – Particulate Emission Results Summary

- Sample
- Date
- Time
- Air Flow Rate (DSCFM) Dry Standard Cubic Feet Per Minute (STP = 68 °F & 29.92 in. Hg)
- Particulate Mass Emission Rate (Lbs/Hr) Pounds of Particulate Per Hour
- Particulate Mass Emission Rate (Lbs/MMBTU Heat Input) Pounds of Particulate Per Million BTU of Heat Input (Calculated using Equation 19-1 from U.S. EPA Method 19. The F Factor used for the Lbs/MMBTU calculations was 9,780 DSCF/MMBTU.)
- Particulate Mass Emission Rate (Lbs/MMBTU Steam Output) Pounds of Particulate Per Million BTU of Steam Output. The BTU/Lb of steam value used (1200 BTU/Lb of Steam) in these calculations was obtained from a Steam Table using steam operating data supplied by Michigan Sugar. The steam table used can be found in Appendix F. Boiler operating data during the testing can be found in Appendix H.

A more detailed breakdown of each individual particulate sample can be found in Appendix A. It should be noted that a particulate sample was started and aborted before completion of the official three (3) samples. Freeze up occurred after 44 minutes of this aborted sample. While dealing with the freeze up problem, the glass probe liner was inadvertently broken. The entire sampling train was scrapped and sampling was resumed from scratch. The raw data sheet for this sample can be found in Appendix G, but the contents of the entire sampling train were discarded because the sample would not have met any of the official sampling quality assurance criteria.

#### III.2 CO

Table 2 – Carbon Monoxide (CO) Emission Results Summary

- Sample
- Time
- Air Flow Rate (DSCFM) Dry Standard Cubic Feet Per Minute (STP = 68 °F & 29.92 in. Hg)
- CO Concentration (PPM) Parts Per Million (v/v) on a Dry Basis

- CO Concentration (PPM @ 3  $\%O_2$ ) Parts Per Million (v/v) on a Dry Basis Corrected To 3 Percent Oxygen
- CO Mass Emission Rate (Lbs/Hr) Pounds of CO Per Hour
- CO Mass Emission Rate (Lbs/MMBTU Heat Input) Pounds of CO Per Million BTU of Heat Input (Calculated using Equation 19-1 from U.S. EPA Method 19. The F Factor used for the Lbs/MMBTU calculations was 9,780 DSCF/MMBTU.)
- CO Mass Emission Rate (Lbs/MMBTU Steam Output) Pounds of CO Per Million BTU of Steam Output. The BTU/Lb of steam value used (1200 BTU/Lb of Steam) in these calculations was obtained from a Steam Table using steam operating data supplied by Michigan Sugar. The steam table used can be found in Appendix F. Boiler operating data during the testing can be found in Appendix H.

All the CO sample data was calibration corrected using Equation 7E-5 from U.S. EPA Method 7E.

#### III.3 Hg

Table 3 - Mercury (Hg) Emission Results Summary

- Sample
- Date
- Time
- Air Flow Rate (DSCFM) Dry Standard Cubic Feet Per Minute (STP = 68 °F & 29.92 in, Hg)
- Hg Mass Emission Rate (Lbs/Hr) Pounds of Hg Per Hour
- Hg Mass Emission Rate (Lbs/MMBTU Heat Input) Pounds of Hg Per Million BTU of Heat Input (Calculated using Equation 19-1 from U.S. EPA Method 19. The F Factor used for the Lbs/MMBTU calculations was 9,780 DSCF/MMBTU.)
- Hg Mass Emission Rate (Lbs/MMBTU Steam Output) Pounds of Hg Per Million BTU of Steam Output. The BTU/Lb of steam value used (1200 BTU/Lb of Steam) in these calculations was obtained from a Steam Table using steam operating data supplied by Michigan Sugar. The steam table used can be found in Appendix F. Boiler operating data during the testing can be found in Appendix H.

A more detailed breakdown of each individual Hg sample can be found in Appendix A. It should be noted that a Hg sample was started and aborted before completion of the official three (3) samples. Freeze up occurred after 44 minutes of this aborted sample. While dealing with the freeze up problem, the glass probe liner was inadvertently broken. The entire sampling train was scrapped and sampling was resumed from scratch. The raw data sheet for this sample can be found in Appendix G, but the contents of the entire sampling train were discarded because the sample would not have met any of the official sampling quality assurance criteria.

#### III.4 HCl

Table 4 – Hydrochloric Acid (HCI) Emission Results Summary

- Sample
- Time
- Air Flow Rate (DSCFM) Dry Standard Cubic Feet Per Minute (STP = 68 °F & 29.92 in. Hg)
- HCI Concentration (Mg/M<sup>3</sup>) Milligrams Per Dry Standard Cubic Meter
- HCl Mass Emission Rate (Lbs/Hr) Pounds of HCl Per Hour
- HCI Mass Emission Rate (Lbs/MMBTU Heat Input) Pounds of HCI Per Million BTU of Heat Input (Calculated using Equation 19-1 from U.S. EPA Method 19. The F Factor used for the Lbs/MMBTU calculations was 9,780 DSCF/MMBTU.)
- HCI Mass Emission Rate (Lbs/MMBTU Steam Output) Pounds of HCI Per Million BTU of Steam Output. The BTU/Lb of steam value used (1200 BTU/Lb of Steam) in these calculations was obtained from a Steam Table using steam operating data supplied by Michigan Sugar. The steam table used can be found in Appendix F. Boiler operating data during the testing can be found in Appendix H.

A more detailed breakdown of each individual HCI sample can be found in Appendix A. It should be noted that during HCI samples 1 & 2, the filter was replaced at the half way mark of each sample. The sampling trains were re-leak checked after the filter replacement. The extra sample volume incurred due to the middle leak check was subtracted from the total sample volume when performing the final calculations.

#### **III.5** Emission Limits

National Emission Standard for Hazardous Air Pollutants (NESHAP) 40CFR Part 63 Subpart DDDDD (MACT for Industrial, Commercial, Institutional Boilers and Process Heaters) has established the following emission limits for this source:

Compound	Emission Limit
 Carbon Monoxide (CO)	160 PPM @ 3% O <sub>2</sub> or 0.14 Lbs/MMBTU of Steam Output
 Particulate	4.0 E-02 Lbs/MMBTU of Heat Input <b>or</b> 4.2 E-02 Lbs/MMBTU of Steam Output

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	Mercury (Hg)		5.7 E-06 Lbs/MMBTU	of Heat Input or 6.4 E-06 Lbs/MMBTU	
1				of Steam Output	
2			2.2 E-02 Lbs/MMBTU	of Heat Input or 2.5 E-02 Lbs/MMBTU	ł
1	Hydrochloric Acid (H	<b>Ci)</b>		of Steam Output	ŀ
11				or occurr output	L

#### IV. SOURCE DESCRIPTION

There are two (2) boilers at the Sebewaing facility. Both boilers are Wicks "A" frame coal fired stokers. These boilers are as follows:

- Boiler #2 (EUICKESEASTBOIL) Built in 1940. Designed heat input of approximately 87 MMBTU/Hr
- Boiler #3 (EUICKESWESTBOIL) Built in 1939. Designed heat input of approximately 87 MMBTU/Hr

These boilers are used for generating process steam. The exhaust gases from these boilers have a common exhaust duct that leads to a wet scrubber followed by a Wet ESP before being emitted to atmosphere. Source operating data during the sampling can be found in Appendix H.

#### V. SAMPLING AND ANALYTICAL PROTOCOL

The sampling location was on the 60 inch I.D. stack with 2 sample ports in a location that exceeded the 8 duct diameters downstream and 2 duct diameters upstream from the nearest disturbances requirement of U.S. EPA Method 1. Twelve (12) sampling points were used for this source.

**V.1 Particulate & Mercury (Hg)** - The Particulate & Hg emission sampling was conducted by employing U.S. EPA Method 29 (combined with U.S. EPA Method 5). This is an out of stack filtration method, where the sampling probe and filter are heated at 250 °F (plus or minus 25 °F). Three (3) samples were collected. The samples were one hundred fifty (150) minutes in duration and each had a minimum sample volume of three (3) dry standard cubic meters (DSCM). The samples were collected isokinetically on quartz filters, in a nitric acid/hydrogen peroxide solution and in a acidic potassium permanganate solution.

The nozzle/probe rinses and filters (front half) were analyzed for particulate by gravimetric analysis in accordance with Method 5. The front half, the nitric acid/hydrogen peroxide solutions and the acidic potassium permanganate solutions were analyzed for mercury by cold vapor atomic absorption spectrophotometry (CVAAS). All the quality assurance and quality control procedures listed in the methods were incorporated in the sampling and analysis. A diagram of the Particulate & Hg sampling train is shown in Figure 1.

**V.2 Carbon Monoxide -** The CO sampling was conducted in accordance with U.S. EPA Reference Method 10. A Thermo Environmental Model 48C gas analyzer was used to monitor the Wet ESP exhaust. A heated teflon sample line was used to transport the exhaust gases to a gas conditioner to remove moisture and reduce the temperature. From the gas conditioner stack gases were passed to the analyzer. The analyzer produces instantaneous readouts of the CO concentrations (PPM).

The analyzer was calibrated by direct injection prior to the testing. A span gas of 169.2 PPM was used to establish the initial instrument calibration. Calibration gases of 49.66 PPM and 92.97 PPM were used to determine the calibration error of the analyzer. The sampling system (from the back of the stack probe to the analyzer) was injected using the 92.97 PPM gas to determine the system bias. After each sample, a system zero and system injection of 92.97 PPM were performed to establish system drift and system bias during the test period. All calibration gases were EPA Protocol 1 Certified. Three (3) samples were collected from the Wet ESP exhaust. Each sample was sixty (60) minutes in duration.

The analyzer was calibrated to the output of the data acquisition system (DAS) used to collect the data from the boiler. The analyzer averages were corrected for calibration error and drift using formula EQ.7E-5 from 40 CFR Part 60, Appendix A, Method 7E. A diagram of the sampling train is shown in Figure 2.

**V.3** Oxygen & Carbon Dioxide (2/8/17) - The O<sub>2</sub> & CO<sub>2</sub> sampling was conducted in accordance with U.S. EPA Reference Method 3A. Servomex Model 1400M portable stack gas analyzers were used to monitor the Wet ESP exhaust. A heated teflon sample line was used to transport the exhaust gases to a gas conditioner to remove moisture and reduce the temperature. From the gas conditioner stack gases were passed to the analyzers. The analyzers produce instantaneous readouts of the O<sub>2</sub> & CO<sub>2</sub> concentrations (%).

The analyzers were calibrated by direct injection prior to the testing. Span gases of 20.96%  $O_2$  and 20.1%  $CO_2$  were used to establish the initial instrument calibrations. Calibration gases of 5.96%  $O_2/12.1\%$   $CO_2$  and 12.1%  $O_2/5.97\%$   $CO_2$  were used to determine the calibration error of the analyzers. The sampling

system (from the back of the stack probe to the analyzers) was injected using the  $12.1\% O_2/5.97\% CO_2$  gas to determine the system bias. After each sample, a system zero and system injection of  $12.1\% O_2/5.97\% CO_2$  were performed to establish system drift and system bias during the test period. All calibration gases were EPA Protocol 1 Certified.

The analyzers were calibrated to the output of the data acquisition system (DAS) used to collect the data from the boiler. The analyzer averages were corrected for calibration error and drift using formula EQ.7E-5 from 40 CFR Part 60, Appendix A, Method 7E. A diagram of the sampling train is shown in Figure 2.

**V.4** Oxygen & Carbon Dioxide (2/7&9/17) - The O<sub>2</sub> & CO<sub>2</sub> sampling during the sampling on these days was performed by employing U.S. EPA Method 3. Bag samples were collected from the back of the isokinetic sampling trains and analyzed by Orsat analysis. All the quality assurance and quality control requirements specified in the method were incorporated in the sampling and analysis.

**V.5** Hydrochloric Acid – The HCl emission sampling was conducted in accordance with U.S. EPA Method 26A. The sampling was performed isokinetically in accordance with the method. The HCl was collected in the first two impingers of the sampling train, which contained 100 mls of 0.1 normal sulfuric acid each. The probe rinse and the impinger catch from the impingers were combined and analyzed for HCl using Ion-chromatography as described in the method..

Three (3) samples were collected from the Wet ESP exhaust. Each sample was sixty (60) minutes in duration and had a minimum sample volume of one (1) dry standard cubic meter (DSCM). All the quality assurance and quality control requirements specified in the method were incorporated in the sampling and analysis. A diagram of the sampling train is shown in Figure 3.

V.6 Exhaust Gas Parameters – The exhaust gas parameters (air flow rate, temperature, moisture and density) were determined in conjunction with the other sampling by employing U.S. EPA Methods 1 through
4. Air flow rates, temperatures and moistures were determined using the isokinetic sampling trains. All the quality assurance and quality control procedures listed in the methods were incorporated in the sampling and analysis.

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