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Particulate Matter 40 CFR 63 Subpart UUUUU LEE Demonstration

EUBOILER01 and EUBOILER02

CMS Enterprises TES Filer City Station 700 Mee Street Filer City, Michigan 49634 SRN: N1685

Test Date: May 7 through 9, 2018 Report Date: May 24, 2018

Test Performed by the Consumers Energy Company Regulatory Compliance Testing Section Air Emissions Testing Body Laboratory Services Section Work Order No. 4101981 Version No. 0

EXECUTIVE SUMMARY

Consumers Energy Regulatory Compliance Testing Section (RCTS) conducted filterable particulate matter (PM) testing of the single exhausts of coal-fired boilers EUBOILER01 and EUBOILER02 (Units 1 and 2) operating at the Tondu Energy Systems (TES) Filer City Station in Filer City, Michigan. The facility is a cogeneration power plant with a rated output of 60-megawatts net and 50,000 pounds of process steam per hour subject to 40 Code of Federal Regulations (CFR) Part 63, Subpart UUUUU – National Emission Standards for Hazardous Air Pollutants: Coal- and Oil-fired Electric Utility Steam Generating Units, also known as the Mercury and Air Toxics (MATS) rule. The 2nd quarter 2018 air emissions tests were performed to (1) satisfy 40 CFR 63.10006(c) quarterly testing requirements, (2) evaluate compliance with the applicable emission limit of 0.030 lb/mmBtu FPM, and (3) to evaluate if the sources qualify as Low Emitting EGUs (LEE) as specified 40 CFR 63.10005(h)(1)(i).

Three 120-minute PM test runs were performed at each boiler exhaust on May7 through 9, 2018 following the procedures described in the Test Protocol submitted by Consumers Energy to Michigan Department of Environmental Quality (MDEQ) on May 1, 2017 and subsequently approved by Mr. Jeremy Howe, MDEQ Environmental Quality Analyst, in his letter dated May 11, 2017. There were no deviations from the approved stack test protocol or the United States Environmental Protection Agency (USEPA) reference methods. The average results of the tests are presented below:

- Unit 1: 0.0010 lb/mmBtu
- Unit 2: 0.0010 lb/mmBtu

The results of the testing indicate EUBOILER01 and EUBOILER02 are in compliance with the applicable MATS PM lb/mmBtu emission limit, and because the emissions were less than 50 percent of the limit, meet the LEE qualification criterion for the 7th consecutive calendar guarter.

Detailed results are presented in Appendix Tables 1 and 2. Sample calculations and field data sheets are presented in Appendices A and B. Laboratory data is presented in Appendix C. Boiler operating data and supporting information are provided in Appendices D and E.

1.0 **INTRODUCTION**

This report summarizes the results of compliance air emissions testing conducted from the exhausts of EUBOILER01 (Unit 1) and EUBOILER02 (Unit 2) at the Tondu Energy Systems (TES) Filer City Station in Manistee, Michigan May 7 through May 9, 2018.

This document follows the Michigan Department of Environmental Quality (MDEQ) format described in the March 2018 Format for Submittal of Source Emission Test Plans and Reports. Reproducing only a portion of this report may omit critical substantiating documentation or cause information to be taken out of context. If any portion of this report is reproduced, please exercise due care in this regard.

1.1 IDENTIFICATION, LOCATION, AND DATES OF TESTS

Consumers Energy Regulatory Compliance Testing Section (RCTS) conducted filterable particulate matter (PM) testing at the TES Filer City Station in Manistee, Michigan May 7 through 9, 2018.

A test protocol was submitted to the Michigan Department of Environmental Quality (MDEQ) on May 1, 2017 and subsequently approved by Mr. Jeremy Howe, MDEQ Environmental Quality Analyst, in his letter dated May 11, 2017. The preceding reflects a standing approval for all quarterly MATS PM tests as long as no modifications from the original protocol are required.

1.2 PURPOSE OF TESTING

The 2^{nd} quarter 2018 air emissions tests were performed to (1) satisfy 40 CFR 63.10006(c) quarterly testing requirements, (2) evaluate compliance with the applicable emission limit, and (3) to evaluate if the sources qualify as Low Emitting EGUs (LEE) as specified 40 CFR 63.10005(h)(1)(i). The applicable emission limits are summarized in Table 1-1.

The PM LEE demonstration requires quarterly sampling over a period of three consecutive years. The results of each quarterly test must be less than or equal to 50 percent of the applicable standard listed in Table 2 of the MATS rule, equating to 0.015 lb/mmBtu for PM. MATS LEE testing for PM commenced in the 4th quarter of 2015. However, the 3rd quarter 2016 PM results for both units were between 50% and 100% of the associated MATS emission limit, so the initial attempt at LEE qualification was ended and a new series of LEE qualification tests was commenced in the 4th quarter of 2016. This test program evaluated LEE status for the 7th consecutive calendar quarter.

Table 1-1 MATS PM Emission Limits

Parameter	Emission Limit	Units	Applicable Requirement
РМ	0.030	lb/mmBtu	Table 2 to Subpart UUUUU of Part 63- Emission Limits for Existing EGU's
Ib/mmBtut nound	hor million Britich the	mol unit host input	

Ib/mmBtu: pound per million British thermal unit heat input

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1.3 BRIEF DESCRIPTION OF SOURCE

TES Filer City Station is a facility consisting of two solid-fuel fired boilers. EUBOILER01 and EUBOILER02 are spreader stoker boilers used to generate steam.

1.4 CONTACT INFORMATION

Table 1-2 presents the test program organization, major lines of communication, and names and contact information of responsible individuals.

Contact Inform	nation	
Program Role	Contact	Address
Regulatory Agency Representative	Ms. Karen Kajiya-Mills Technical Programs Unit Manager 517-335-4874 <u>kajiya-millsk@michigan.gov</u>	Michigan Department of Environmental Quality Technical Programs Unit 525 W. Allegan, Constitution Hall, 2 nd Floor S Lansing, Michigan 48933
Regulatory Agency Inspector	Ms. Caryn Owens Environmental Engineer 231-876-4414 owensc1@michigan.gov	Michigan Department of Environmental Quality Cadillac District 120 W. Chapin Street Cadillac, Michigan 49601
Regulatory Agency Representative	Mr. Jeremy Howe Environmental Engineer 231-876-4416 <u>howej1@michigan.gov</u>	Michigan Department of Environmental Quality Cadillac District 120 W. Chapin Street Cadillac, Michigan 49601
Responsible Official	Mr. Henry Hoffman General Manager 231-723-6573, Ext 102 henry.hoffman@cmsenergy.com	CMS Generation Filer City Operating, LLC Filer City Station 700 Mee Street Filer City, Michigan 49634
Plant Representative	Mr. Austin Swiatlowski Plant Operator 231-723-6573, Ext 108 austin.swiatlowski@cmsenergy.com	CMS Generation Filer City Operating, LLC Filer City Station 700 Mee Street Filer City, Michigan 49634
Test Team Representative	Mr. Thomas R. Schmelter, QSTI Senior Engineering Technical Analyst 616-738-3334 thomas.schmelter@cmsenergy.com	Consumers Energy Company L&D Training Center 17010 Croswell Street West Olive, Michigan 49460
Test Team Representative	Mr. Brian E. Miska, QSTI Senior Engineering Technical Analyst 989-891-3415 <u>brian.miska@cmsenergy.com</u>	Consumers Energy Company D.E. Karn Power Plant 2742 N. Weadock Highway ESD Trailer #4 Essexville, Michigan 48732

Table 1-2 Contact Informat

2.0 SUMMARY OF RESULTS

2.1 OPERATING DATA

During the tests, the boilers were operated as close as possible to maximum normal operating load conditions. 40 CFR 63.10007(2) states the maximum normal operating load will be generally between 90 and 110 percent of design capacity but should be

representative of site specific normal operations. The average steam flow during the test was 307.0 klbs/hr for Unit 1 and 302.7 klbs/hr for Unit 2 (96% load for Unit 1 and 95% load for Unit 2, with a full load rating of 320 klbs/hr for each unit). Recorded operating data, including fuel blend firing rate and composite fuel factor data, is included in Appendix D.

2.2 APPLICABLE PERMIT INFORMATION

The TES Filer City Station is currently operating pursuant to the terms and conditions of State of Michigan Registration Number (SRN) N1685 air permit MI-ROP-N1685-2015b. The air permit incorporates state and federal regulations. The USEPA has assigned a Facility Registry Service (FRS) identification number of 110056958225. EUBOILER01 and EUBOILER02 are the emission unit sources listed within the permit and collectively comprise the FGBOILERS flexible group. Incorporated within the permit are the applicable requirements of 40 CFR 63, Subpart UUUUU – National Emission Standards for Hazardous Air Pollutants: Coal- and Oil-fired Electric Utility Steam Generating Units.

2.3 RESULTS

The results of the air emissions testing indicate the 3-run average PM emission rates are in compliance with the applicable limit and both EUBOILER01 and EUBOILER02 are emitting PM below the LEE qualification threshold. Refer to Table 2-1 for a summary of the PM test results. Refer to Section 5.0 for further discussion.

Source	Units	nits			Average		Emission Limit	
		1	2	3		MATS	MATS LE	
	lb/mmBtu	0.0015	0.0008	0.0008	0.0010	0.030	0.015	
Unit 1	lb/hr	0.59	0.32	0.34	0.42	N/A	N/A	
	lb/mmBtu	0.0008	0.0009	0.0013	0.0010	0.030	0.015	
Unit 2	lb/hr	0.34	0.37	0.52	0.41	N/A	N/A	

Table 2-1 Summary of PM Test Results

Detailed results are presented in Tables 1 and 2, following the report text. Sample calculations and field data sheets are presented in Appendices A and B. Laboratory data is presented in Appendix C. Boiler operating data and supporting information are provided in Appendices D and E.

3.0 SOURCE DESCRIPTION

TES Filer City Station is a cogeneration facility consisting of two solid-fuel fired boilers. The electricity output is sold pursuant to a long-term power purchase agreement with Consumers Energy Company. Process steam is sold to an adjacent industrial customer.

3.1 PROCESS

TES Filer City Station operates as a cogeneration electric power plant with a rated output of approximately 60-megawatts net (MW_n) and is also capable of generating 50,000 pounds of process steam per hour. The electricity and process steam are sold under contract to public and/or private companies. The facility commenced commercial operations beginning in 1990.

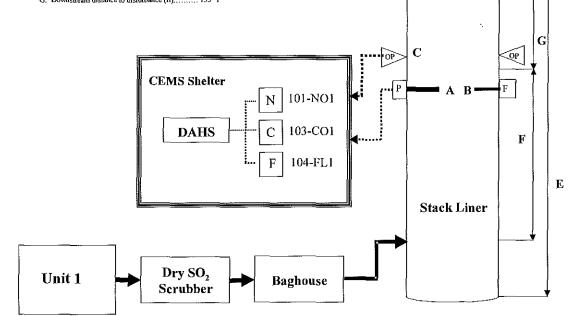
3.2 PROCESS FLOW

EUBOILER01 and EUBOILER02 are spreader stoker boilers used to generate steam. Each unit has a nominal heat input rating of approximately 384 mmBtu/hour and are currently allowed to combust coal, wood and wood waste, industrial construction/demolition wood waste, tire derived fuel, petroleum coke and natural gas. Note that pursuant to an Administrative Consent Order with EPA, all petroleum coke has been removed from the site and the facility does not anticipate using this fuel in the future. The fuel is fired in the furnace where the combustion heats water within boiler tubes producing steam. At full load, each unit is capable of producing approximately 320,000 pounds per hour of steam. This steam is used to turn a common steam turbine that is connected to an electricity producing generator. The electricity is routed through the transmission and distribution system to customers.

The exhaust gas from each boiler is vented to a spray dryer absorber (SDA) flue gas desulfurization system for sulfur dioxide and acid gas control and a baghouse to control particulate matter. The abated exhaust gases are discharged through separate circular flues housed within a single exhaust stack. The separate flues discharge approximately 250 feet above grade. Refer to Figure 3-1 for a process flow diagram of Unit 1 which is also representative of Unit 2.

Figure 3-1. Unit 1 Data Flow Diagram

- B: Location of flow monitor probe (ft) 95' 2"



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D

3.3 MATERIALS PROCESSED

At the time of testing, Units 1 and 2 were capable of firing mixtures of coal (bituminous and subbituminous), wood and wood waste, construction/demolition (C/D) material, tire-derived-fuel (TDF), petroleum coke and natural gas. As noted previously, the facility does not anticipate firing petroleum coke in the future. During the tests, coal, TDF, and wood were fired. Refer to Appendix D for facility operating data recorded during the test program.

In March of 2016, two low NO_x natural gas-fired burners were installed each boiler. Natural gas is utilized as a clean startup fuel, as well as at other times for flame stabilization and other purposes. Natural gas was not fired during the PM testing.

3.4 RATED CAPACITY

EUBOILER01 and EUBOILER02 each have a nominally rated heat input capacity of 384 mmBtu/hr and a steam generation capacity of 320,000 lbs/hr; they can generate a combined net electrical output of approximately 60 MW_n and 50,000 pounds of process steam per hour. The boilers normally operate in a continuous manner near their rated capacity in order to meet the contractual electrical and steam requirements of TES Filer City Station customers.

3.5 PROCESS INSTRUMENTATION

The process was continuously monitored by boiler operators, environmental technicians, and data acquisition systems during testing. The following operating parameters were recorded during the test program and are included in Appendix D:

- Carbon dioxide concentration (%)
- Fuel blend (coal, natural gas, TDF, and wood) firing rates (lb/hr) (scfm for natural gas)
- Steam load flow (1,000s lb/hr) and pressure (psia) [In lieu of electrical load, which is only determined on a combined basis.]
- Opacity (%)
- Total heat input (mmBtu/hr)
- Mixed fuel factor, F_c (scf/mmBtu)
- SO₂ reduction (%)

Due to the various instrumentation monitoring systems, the facility instrumentation time stamps were correlated to reference method test times in local Eastern Standard Time (EST).

4.0 SAMPLING AND ANALYTICAL PROCEDURES

Consumers Energy RCTS tested for PM emissions using the USEPA test methods presented in Table 4-1. The sampling and analytical procedures associated with each parameter are described in the following sections.

Table 4-1 Test Methods

Parameter	Method	USEPA
		Title
Sampling location and Traverse Points	1	Sample and Velocity Traverses for Stationary Sources
Stack Gas Velocity and Temperature	2	Determination of Stack Gas Velocity and Volumetric Flow Rate (Type S Pitot Tube)
Molecular weight (O ₂ and CO ₂)	3A	Determination of Oxygen and Carbon Dioxide Concentrations in Emissions from Stationary Sources (Instrumental Analyzer Procedure)
Moisture	4	Determination of Moisture Content in Stack Gases
Filterable particulate matter	5	Determination of Particulate Matter Emissions from Stationary Sources
Emission rate	19	Determination of Sulfur Dioxide Removal Efficiency and Particulate Matter, Sulfur Dioxide, and Nitrogen Oxide Emission Rates

4.1 DESCRIPTION OF SAMPLING TRAIN AND FIELD PROCEDURES

The test matrix presented in Table 4-2 summarizes the sampling and analytical methods performed for the specified parameters during this test program.

Test M	latrix						
Date	Run	Sample Type	Start Time (EST)	Stop Time (EST)	Test Duration (min)	EPA Test Method	Comment
May 7, 2018	1	Unit 1 PM	13:00	15:08	120	MATS5	12 traverse points; isokinetic sampling; 120 minute test; minimum sample volume of 2 dscm
May 7, 2018	2	Unit 1 PM	15:30	17:37	120	MATS5	12 traverse points; isokinetic sampling; 120 minute test; minimum sample volume of 2 dscm
May 8, 2018	3	Unit 1 PM	9;10	11:20	120	MATS5	12 traverse points; isokinetic sampling; 120 minute test; minimum sample volume of 2 dscm
May 8, 2018	1	Unit 2 PM	11:55	14:05	120	MATS5	12 traverse points; isokinetic sampling; 120 minute test; minimum sample volume of 2 dscm
May 8, 2018	2	Unit 2 PM	14:30	16:45	120	MATS5	12 traverse points; isokinetic sampling; 120 minute test; minimum sample volume of 2 dscm
May 9, 2018	3	Unit 2 PM	9:05	11:10	120	MATS5	12 traverse points; isokinetic sampling; 120 minute test; minimum sample volume of 2 dscm

Table 4-2 Test Matrix

4.1.1 SAMPLE LOCATION AND TRAVERSE POINTS (USEPA METHOD 1)

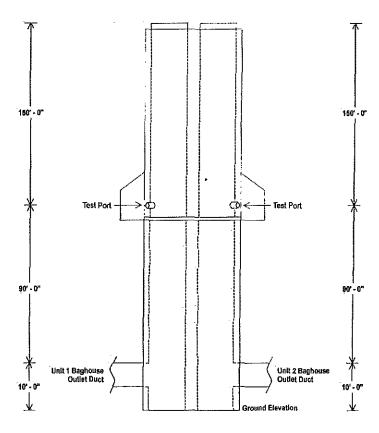
The selection of the measurement site was evaluated using the procedure in USEPA Method 1, *Sample and Velocity Traverses for Stationary Sources*. Each exhaust gas flue is 76 inches in diameter with two 6-inch internal diameter sample ports that extend 20 inches from the flue interior wall. The sample ports are situated:

- Approximately 90 feet or 14 duct diameters downstream of a duct bend disturbance where the combustion gases exit the baghouse and enter the exhaust stack, and
- Approximately 150 feet or 24 duct diameters upstream of the exhaust to atmosphere.

Because the sampling locations are at least eight stack or duct diameters downstream and two diameters upstream from any flow disturbance such as a bend, expansion, or contraction in the stack, or from a visible flame and meet the requirements of USEPA Method 1, flue gas measurements were collected from a total of 12 traverse points. The area of the exhaust duct was calculated and the cross-section divided into a number of equal areas based on distances to air flow disturbances. Flue gas was sampled for 10 minutes at six traverse points from the two sample ports for a total test duration of 120 minutes.

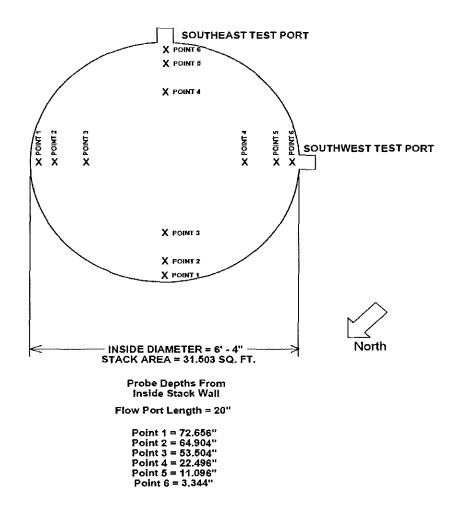
A dimensioned sketch of the sample location showing the sampling ports in relation to breeching and to upstream and downstream disturbances or obstructions in gas flow is presented as Figure 4-1. The Unit 1 duct cross section and sampling point detail is presented as Figure 4-2; Unit 2 is identical to Unit 1 with the exception the two test ports are located at the northeast and northwest compass positions.

Figure 4-1. Unit 1 and 2 Sample Locations



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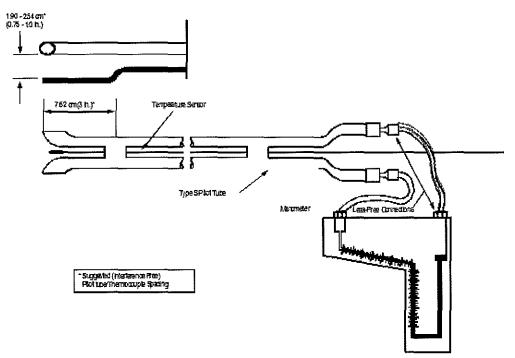




4.1.2 VELOCITY AND TEMPERATURE (USEPA METHOD 2)

The exhaust gas velocity and temperature were measured using USEPA Method 2, Determination of Stack Gas Temperature and Velocity (Type S Pitot Tube). The pressure differential (Δ P) across the positive and negative openings of the Pitot tube inserted in the exhaust duct at each traverse point were measured using an "S Type" (Stauscheibe or reverse type) Pitot tube connected to an appropriately sized oil filled inclined manometer. Exhaust gas temperatures were measured using a chromel/alumel "Type K" thermocouple and a temperature indicator. Refer to Figure 4-3 for a drawing of the Method 2 sample apparatus showing the Pitot tube and thermocouple configuration.

Figure 4-3. Method 2 Sample Apparatus



Flue gas velocity and velocity vector measurements (cyclonic flow evaluation) were measured following the procedures in USEPA Method 2 at the sampling locations. Cyclonic flow is defined as a flow condition with an average null angle greater than 20 degrees. The direction of flow can be determined by aligning the Pitot tube to obtain zero (null) velocity head reading—the direction would be parallel to the Pitot tube face openings or perpendicular to the null position. By measuring the angle of the Pitot tube face openings in relation to the stack walls when a null angle is obtained, the direction of flow is measured. If the absolute average of the flow direction angles is greater than 20 degrees, the flue gas is considered to be cyclonic at that sampling location and an alternative location should be found.

Appendix B of this report includes cyclonic flow test data as verification of the absence of cyclonic flow at each test location. Method 1, § 11.4.2 indicates *if the average* (null angle) *is greater than 20°, the overall flow condition in the stack is unacceptable, and alternative methodology...must be used*. The average null yaw angle measured in August 2012 was 3.25° for Unit 1 and 8.25° for Unit 2, thus meeting the less than 20° requirement. Because there have been no significant ductwork and/or stack configuration changes, this null angle information is considered to be valid and additional cyclonic flow verification was not performed prior to the PM test.

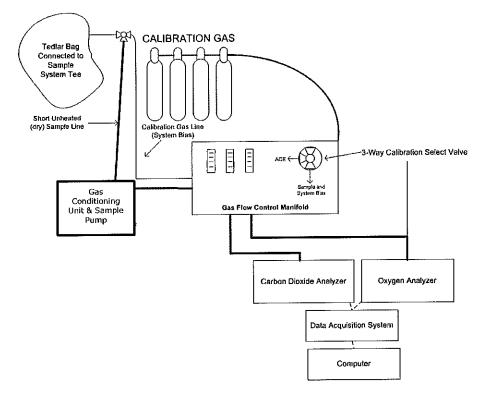
4.1.3 MOLECULAR WEIGHT (USEPA METHOD 3A)

The exhaust gas composition and molecular weight was measured using the sampling and analytical procedures of USEPA Method 3A, Determination of Oxygen and Carbon Dioxide Concentrations in Emissions from Stationary Sources (Instrumental Analyzer Procedure). The flue gas oxygen and carbon dioxide concentrations were used to calculate molecular weight, flue gas velocity, and emissions in Ib/mmBtu, and Ib/1,000 lbs corrected to 50% excess air.

An integrated flue gas sample was collected during each PM run from each of 12 traverse points into a stainless steel lined probe and inert sample line into a flexible sample bag.

Molecular weight analysis was performed by connecting the flexible bag to a gas sample conditioner which conveyed the sample to paramagnetic and infrared gas analyzers that measure oxygen and carbon dioxide concentrations. Figure 4-4 depicts the Method 3A sampling system.

Figure 4-4. Method 3A Sampling System



Prior to sampling flue gas, the analyzers were calibrated by performing a calibration error test where zero-, mid-, and high-level calibration gases are introduced to the back of the analyzers. The calibration error check was performed to evaluate if the analyzers response was within $\pm 2.0\%$ of the calibration gas span. A system-bias and drift test was performed where the zero- and mid- or high- calibration gases are introduced at the inlet to the gas conditioner to measure the ability of the system to respond to within ± 5.0 percent of span.

At the conclusion of one or more flexible bag analyses, an additional system bias check was performed to evaluate the drift from the pre- and post-test system bias checks. The system-bias checks evaluated if the analyzers drift is within the allowable criterion of $\pm 3.0\%$ of span from pre- to post-test system bias checks. The measured oxygen and carbon dioxide concentrations were corrected for analyzer drift. Refer to Appendix E for analyzer calibration supporting documentation.

4.1.4 MOISTURE CONTENT (USEPA METHOD 4)

The exhaust gas moisture content was determined using USEPA Method 4, *Determination of Moisture in Stack Gases* in conjunction with the Method 5 sample apparatus. The sampled gas was conveyed through a series of impingers immersed in an ice bath to condense water in the flue gas. The amount of water condensed and collected in the impingers was measured gravimetrically and used to calculate the exhaust gas moisture content.

4.1.5 PARTICULATE MATTER (USEPA METHOD 5)

Filterable particulate matter samples were collected isokinetically following the procedures of USEPA Method 5, Determination of Particulate Matter Emissions from Stationary Sources with the necessary modifications specified in the MATS Rule for low emitting EGU (LEE) status determinations. Specifically, the probe and filter temperatures were maintained at 320° F, $\pm 25^{\circ}$ F, throughout the duration of each test run and a minimum of 2 dry standard cubic meters (dscm) or 70.629 dry standard cubic feet (dscf) of sample volume was collected.

As flue gas is withdrawn isokinetically from the stack, filterable PM is collected on a heated quartz-fiber filter. Moisture or water vapor in the gas condenses in a series of impingers following the heated filter. Figure 4-5 depicts the Method 5 sample apparatus and Table 4-3 provides the Method 5 impinger configuration detail.

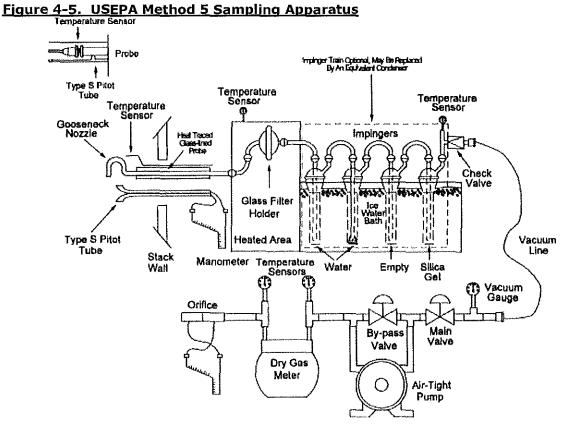
Impinger Order (Upstream to Downstream	Impinger Type	Impinger Contents	Amount (gram)
1	Modified	Water	100
2	Greenburg-Smith	Water	100
3	Modified	Empty	0
4	Modified	Silica gel desiccant	~200-300

Table 4-3 Method 5 Impinger Configuration

Prior to testing, representative velocity head and temperature data was reviewed to calculate an ideal nozzle diameter allowing isokinetic sampling to be performed. The diameter of the selected nozzle was measured with a caliper across three cross-sectional chords; this data was used to calculate the cross-sectional area. Prior to testing, the nozzle was rinsed and brushed with deionized water and acetone, and connected to the sample probe.

The impact and static pressure openings of the S-Type Pitot tube were leak-checked at or above a velocity head of 3.0 inches of water for a minimum of 15 seconds. The PM sample apparatus was leak-checked by capping the nozzle tip and applying a vacuum of approximately 15 inches of mercury while the dry-gas meter was monitored for approximately 1 minute to verify the sample train leakage rate was less than 0.02 cubic foot per minute (cfm). The sample probe was then inserted into the sampling port to begin sampling.

After placing ice around the impingers, the probe and filter temperatures were allowed to stabilize to a temperature of $320\pm25^{\circ}$ F. Once the desired operating conditions were coordinated with the facility, testing was initiated. Stack and sampling apparatus parameters (e.g., flue velocity head, temperature) were then monitored throughout each run to maintain an isokinetic rate of 100 ± 10 %. Refer to Appendix B for field data sheets.



At the conclusion of a test run and post-test leak check, the sampling apparatus was disassembled and the impingers and filter housing were transported to the recovery area.

The filter was recovered from the filter housing and placed in a Petri dish, sealed with Teflon tape, and labeled as "FPM Container 1." The nozzle, probe liner, and the front half of the filter housing were triple rinsed with acetone to collect particulate matter. The acetone rinses were collected in pre-cleaned sample containers, sealed with Teflon tape, and labeled as "FPM Container 2." The weight of liquid collected in each impinger, including the silica gel impinger, was measured using an electronic scale; these weights were used to calculate the moisture content of the sampled flue gas. The contents of the impingers were discarded. Refer to Figure 4-6 for the USEPA Method 5 sample recovery scheme.

The sample containers, including a filter and acetone blank were transported to the laboratory for analysis. The sample analysis followed USEPA Method 5 procedures as summarized in the analytical scheme presented in Figure 4-7. Refer to Appendix C for laboratory data sheets.

Figure 4-6. USEPA Method 5 Sample Recovery Scheme

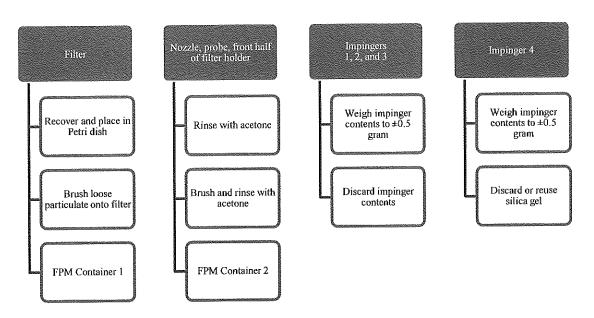
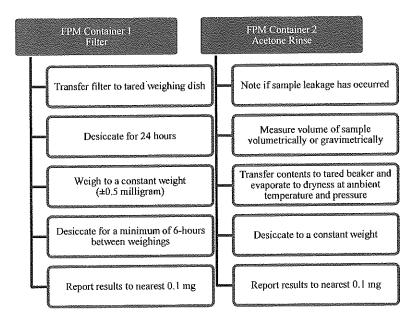


Figure 4-7. USEPA Method 5 Analytical Scheme



4.1.6 EMISSION RATES (USEPA METHOD 19)

USEPA Method 19, *Determination of Sulfur Dioxide Removal Efficiency and Particulate Matter, Sulfur Dioxide, and Nitrogen Oxide Emission Rates,* was used to calculate PM emission rates in units of Ib/mmBtu. Measured carbon dioxide concentrations and F factors (ratios of combustion gas volumes to heat inputs) were used to calculate emission rates using equation 19-6 from the method. Figure 4-8 presents the equation used to calculate lb/mmBtu emission rate:

Figure 4-8. USEPA Method 19 Equation 19-6

$$E = C_d F_c \frac{100}{\% CO_{2d}}$$

Where:

E = Pollutant emission rate (lb/mmBtu)

 C_d = Pollutant concentration, dry basis (lb/dscf)

F_c = Volumes of combustion components per unit of heat content

1,800 scf CO₂/mmBtu for bituminous coal from 40 CFR 75, Appendix F, Table 1 (prorated based on actual fuel usage)

 $%CO_{2d} =$ Concentration of carbon dioxide on a dry basis (%, dry)

Refer to Appendix A for example calculations and Appendix D for operating data that includes the calculated F_c factor based on the fuels combusted during each test run.

5.0 TEST RESULTS AND DISCUSSION

The test program results summarized in Section 2.3 indicate Units 1 and 2 are in compliance with the MATS Rule emission limits. Because the results are less than 50% of the applicable emission standard, both EUBOILER01 and EUBOILER02 met the MATS LEE qualification threshold for the seventh consecutive calendar quarter. Refer to Tables 1 and 2 for detailed results.

5.1 TABULATION OF RESULTS

The results of the testing are tabulated in Tables 1 and 2 for EUBOILER01 and EUBOILER02, respectively. The tabulated information includes dry gas meter data, moisture data, stack gas analysis data, velocity and volumetric flow data and concentration and emission rate data. Additional tabulated supporting data is presented in Appendices B-E.

5.2 SIGNIFICANCE OF RESULTS

The results of this test program indicate EUBOILER01 and EUBOILER02 are in compliance with the applicable MATS PM emission limit of 3.0E-02 lb/mmBtu. Further, the PM emission rates for both units continue to fall below the MATS LEE qualification threshold of 1.5E-02 lb/mmBtu (i.e., 50% of the MATS PM emission limit).

5.3 VARIATIONS FROM SAMPLING OR OPERATING CONDITIONS

No sampling procedure variations from the USEPA test methods or approved Test Protocol were performed.

Testing was paused for approximately 10 minutes during the second run on Boiler #2. This was due to the loss of the coal feeder which resulted in a boiler steam flow swing.

Soot blowing was conducted on Unit 1 during the run 1 PM Test and conducted on Unit 2 during the run 1 PM Test.

5.4 PROCESS OR CONTROL EQUIPMENT UPSET CONDITIONS

Other than the previously described event during Unit 2, Run 2, no process or control equipment upset conditions occurred during the testing.

5.5 AIR POLLUTION CONTROL DEVICE MAINTENANCE

No significant pollution control device maintenance occurred during the three months prior to the test. Optimization of the air pollution control devices is a continuous process to ensure compliance with regulatory emission limits.

5.6 RE-TEST DISCUSSION

Based on the results of this test program, a re-test is not required.

5.7 RESULTS OF AUDIT SAMPLES

Audit samples are not required for the reference methods utilized during this test program and are not available from USEPA Stationary Source Audit Sample Program providers. A list of QA/QC Procedures is listed below in Table 5-1.

QA/QC Proced	ures			
QA/QC Activity	Purpose	Procedure	Frequency	Acceptance Criteria
M1: Sampling Location	Evaluate if the sampling location is suitable for sampling	Measure distance from ports to downstream and upstream flow disturbances	Pre-test	≥2 diameters downstream; ≥0.5 diameter upstream.
M1: Duct diameter/ dimensions	Verify area of stack is accurately measured	Review as-built drawings and field measurement	Pre-test	Field measurement agreement with as-built drawings
M1: Cyclonic flow evaluation	Evaluate the sampling location for cyclonic flow	Measure null angles	Pre-test (if needed)	≤20°
M2: Pitot tube inspection	Verify Pitot and thermocouple assembly is free of aerodynamic interferences	Inspection	Pre-test and post-test	Refer to Section 6.1 and 10.0 of USEPA Method 2
M2: Pitot tube leak check	Verify leak free sampling system	Apply minimum pressure of 3.0 inches of H2O to Pitot tube	Pre-test and Post-test	±0.01 in H2O for 15 seconds at minimum 3.0 in H2O velocity head
M3A: Calibration gas standards	Ensure accurate calibration standards	Traceability protocol of calibration gases	Pre-test	Calibration gas uncertainty ≤2.0%
M3A: Calibration Error	Evaluates operation of analyzers	Calibration gases introduced directly into analyzers	Pre-test	±2.0% of the calibration span
M3A: System Bias and Analyzer Drift	Evaluates ability of sampling system to deliver stack gas to analyzers	Calibration gases introduced at the sample conditioning system, and into	Pre-test and Post-test	±5.0% of the analyzer calibration span for bias and ±3.0% of analyzer calibration span for drift

Table 5-1

Regulatory Compliance Testing Section GE&S/Environmental & Laboratory Services Department

Table 5-1 QA/QC Procedures

QA/QC Activity	Purpose	Procedure	Frequency	Acceptance Criteria
M5: nozzle diameter measurements	Verify nozzle diameter used to calculate sample rate	analyzers Measure inner diameter across three cross- sectional chords	Pre-test	Three measurements agree within ±0.004 inch
M5: sample rate	Ensure representative sample collection	Calculate isokinetic sample rate	During and post-test	100±10% isokinetic sample rate
M5: sample volume	Ensure sufficient sample volume is collected	Record pre- and post-test dry gas meter volume reading	Post test	≥ 2 dscm or 70.6 dscf (requirements for MATS PM LEE testing; twice the sampling volume in Table 2 to Subpart UUUUU)
M5: post-test leak check	Evaluate if the sample was affected by system leak	Cap sample train; monitor dry gas meter	Post-test	≤0.020 cfm
M5: post-test meter audits	Evaluates accurate measurement equipment for sample volume	Calibrate DGM pre- and post-test; compare calibration factors (Y)	Pre-test Post-test	±5 %

5.8 CALIBRATION SHEETS

Calibration and inspection sheets for dry gas meter, Pitot tube, and other equipment are presented in Appendix E.

5.9 SAMPLE CALCULATIONS

Sample calculations and formulas used to compute emissions data are presented in Appendix A.

5.10 FIELD DATA SHEETS

Field data sheets are presented in Appendix B.

5.11 LABORATORY QUALITY ASSURANCE / QUALITY CONTROL PROCEDURES

Laboratory quality assurance and quality control procedures were performed in accordance with USEPA Method 5. Specific QA/QC procedures include evaluation of reagent and filter blanks, laboratory conditions, and the application of blank corrections. Refer to Appendix C for the laboratory data sheets.

5.11.1 QA/QC BLANKS

Reagent and media blanks were analyzed for the parameters of interest. The results of the blanks are presented in the Table 5-2.

Table 5-2 QA/QC Blanks

Sample Identification	Result	Comment
Method 5 Acetone Field Blank	2.9 mg	Sample volume was 200 milliliters. Acetone blank corrections of \sim 0.30 mg were applied.
Method 5 Laboratory Filter Blank	0.0 mg	Reporting limit is 0.1 milligrams.

Table

		Soloca
Consumers	Energy	B

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Facility and Source Information	Units	Run 1	Run 2	Run 3	Average
Customer:	Onits	<u></u>		Filer City	Average
Source:				nit 1	
Work Order:				1981	
Date:	<u> </u>	5/7/2018	5/7/2018	5/8/2018	I
Unit Steam Load:	klbs/hr	308	306	307	307
Stack Diameter	inches	76,0	76.0	76.0	<u> </u>
Cross-sectional Area of Stack, A	ft ²	31.50	31.50	31.50	[
Source Pollutant Test Data	Units	Run 1	Run 2	Run 3	Average
Barometric Pressure, P _{bar}	inches of Hg	29.53	29,51	29.40	29.48
Dry Gas Meter Calibration Factor, Y	dimensionless	0.999	0.999	0.999	0.999
Pitot Tube Coefficient, Cp	dimensionless	0,84	0.84	0.84	0.84
Stack Static Pressure, Pg	inches of H ₂ O	-0.50	-0.50	-0.50	-0.50
Nozzle Diameter, D _n	inches	0,212	0.212	0.212	0.212
Run Start Time	hr:mm	13:00	15:30	9:10	
Run Stop Time	hr:mm	15:08	17:37	11:20	İ
Duration of Sample, 9	minutes	120	120	120	120
Dry Gas Meter Leak Rate, L _p	cfm	0.000	0.000	0.000	0.000
Dry Gas Meter Start Volume	ft ³	97.34	193,48	293.55	194.79
Dry Gas Meter Final Volume	- <u> n</u> ³	192.80	292.69	388.65	291.38
Average Pressure Difference across the Orifice Meter, AH	inches of H ₂ O	2,05	2.19	2.05	2.10
Average Dry Gas Meter Temperature, Tm	1°F	80.8	94.5	78.4	84.6
Average Square Root Velocity Head, vop	vinches H ₂ O	1.1822	1.1950	1,1755	1.1842
Stack Gas Temperature, T _{s(abavg)}	*F	177.3	175.6	175.5	176.1
Source Moisture Data		Run 1	Run 2	Run 3	Average
Volume of Water Vapor Condensed in Silica Gei, Vysa(std)	scf	2.0	1.3	1.2	1.5
Total Volume of Water Vapor Condensed, Vw(std)	scf	14,501	15.189	14.279	14,657
Volume of Gas Sample as Measured by the Dry Gas Meter, Vm	dcf	95.451	99.211	95.100	96.587
/olume of Gas Sample Measured by the Dry Gas Meter corrected to STP, Vm(std)	dscf	92,311	93.553	91.980	92.615
/olume of Gas Sample Measured by the Dry Gas Meter corrected to STP, Vm(std)	dscm	2.614	2.649	2.605	2.62
Molsture Content of Stack Gas, Bws	% H ₂ O	13.58	13.97	13.44	13.66
Gas Analysis Data		Run 1	Run 2	Run 3	Average
Carbon Dioxide, %CO2	%, dry	12.0	12.8	12.7	12.5
Oxygen, %O ₂	%, dry	7.1	6,8	7.2	7.0
Nitrogen, %N	%, dry	80.9	80,4	80.2	80.5
Dry Molecular Weight, Ma	lb/lb-mole	30.20	30,32	30.32	30.28
Wet Molecular Weight, Ms	ib/lb-mole	28.55	28.60	28.66	28.60
Percent Excess Air, %EA	%	49.37	46.75	51.05	49.06
Fuel F-Factor, F _o :	dimensionless	1.154	1,105	1.084	1.114
Fuel F-Factor, Fc:	scf/mmBtu	1,800.6	1,800,6	1,800.1	1.800.4
Gas Volumetric Flow Rate Data		Run 1	Run 2	Run 3	Average
Average Stack Gas Velocity, vs	ft/s	73.9	74.5	73.4	73.9
Stack Gas Volumetric Flow Rate, Q	acím	139,611	140,854	138,658	139,707
Stack Gas Volumetric Flow Rate, Q	scfm	114,026	115,265	113,059	114,116
Stack Gas Dry Standard Volumetric Flow Rate, Qet	dscfm	98,546	99,164	97,866	98,525
Percent of Isokinetic Sampling, I	%	100.4	101.1	100.7	100.7
Gas Concentrations and Emission Rates		Run 1	Run 2	Run 3	Average
Mass of Filterable PM Collected, me	mg	4.21	2.30	2.42	2.98
ilterable PM Concentration, cs	gr/dscf	0.00070	0.00038	0.00041	0,00050
illerable PM Concentration at Stack Conditions, cs@stack.conditions	mg/wacm	1.136	0.612	0.657	0.802
Filterable PM Concentration, C ₅ [Actual Conditions, Wet Basis]	lb/1,000 lbs	0.001	0.0012	0.001	0.001
Filterable PM Concentration, C ₅₅₀ [Actual Conditions, Wet Basis]	lb/1,000 lbs @ 50% EA	0.001	0.001	0.001	0.001
Filterable PM Mass Emission Rate, E	lb/hr	0.59	0.32	0.34	0.001
	lb/mmBtu	0,0015	0.0008		0,0010
Filterable PM, Ib/mmBtu, E	(International Content of Content	0,0010	0.0000	0.0008	0,0010



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Facility and Source Information	Units	Run 1	Run 2	Run 3	Average
Customer:		<u>_</u>		iler City	
Source:				nit 2	
Nork Order:			1	1981	
Date:		5/8/2018	5/8/2018	5/9/2018	
Unit Steam Load:	kibs/hr	299	305	305	303
Stack Diameter	inches ft ²	76.0	76.0	76.0	<u> </u>
Cross-sectional Area of Stack, A		31.50	31.50		l
Source Pollutant Test Data	Units	Run 1	Run 2	Run 3	Average
Barometric Pressure, P _{bar}	inches of Hg	29.40	29.40	29.20	29.33
Dry Gas Meter Calibration Factor, Y	dimensionless	0.999	0.999	0.999	0.999
Pilot Tube Coefficient, Cp	dimensionless	0.84	0.84	0.84	0.84
Stack Static Pressure, Pg	inches of H ₂ O	-0.50	-0.50	-0.50	-0.50
Nozzle Diameter, D _n	(inches	0.212	0.212	0.212	0.212
Run Start Time	hr:mm	11:55	14:30	9:05	
Run Stop Time	hr:mm	14:05	16:45	11:10	l
Duration of Sample, 0	minutes	120	120	120	120
Dry Gas Meier Leak Rale, L _p		0.000	0.000	0.000	0.000
Dry Gas Meter Start Volume	ft ³	389.15	488.78	587.29	488.40
Dry Gas Meter Final Volume	ft ³	488.04	586.72	683.08	585.95
Average Pressure Difference across the Orifice Meter, AH	Inches of H ₂ O	2.16	2.14	2.11	2.14
Average Dry Gas Meter Temperature, Tm	۴ <u> </u>	97.6	100.2	76,6	91.5
Average Square Root Velocity Head, v∆p	vinches H ₂ O	1.1786	1.1791	1,1896	1.1824
Stack Gas Temperature, T _{s(abavg)}	*F	172.3	174.2	170.7	172.4
Source Moisture Data		Run 1	Run 2	Run 3	Average
Volume of Water Vapor Condensed in Silica Gel, V _{wsg(std)}	scf	1.3	1.3	1.3	1.3
Total Volume of Water Vapor Condensed, Vw(std)	scf	14.164	14.829	14.100	14,364
Volume of Gas Sample as Measured by the Dry Gas Meter, V _m	dcf	98.895	97.934	95.795	97.541
/olume of Gas Sample Measured by the Dry Gas Meter corrected to STP, $V_{m(std)}$	dscf	92.388	91.064	92.346	91.933
volume of Gas Sample Measured by the Dry Gas Meter corrected to STP, $V_{m(std)}$	dscm	2.616	2.579	2.615	2.60
Moisture Content of Stack Gas, B _{ws}	% H ₂ O	13.29	14.00	13.25	13.51
Gas Analysis Data		Run 1	Run 2	Run 3	Average
Carbon Dioxide, %CO2	%, dry	12.5	13.1	12.4	12.6
Oxygen, %O ₂	%, dry	7.3	6,6	7.0	7.0
Nitrogen, %N	%, dry	80.2	80.4	80.6	80.4
Dry Motecular Weight, M _d	lb/ib-moie	30.29	30,35	30.26	30.30
Net Motecular Weight, M.	lb/tb-mole	28.66	28.62	28.64	28.64
Percent Excess Air, %EA	%	52.19	44,82	49.46	48.82
Fuel F-Factor, Fo:	dimensionless	1.090	1.097	1.121	1.103
Fuel F-Factor, F _c :	scf/mmBtu	1,800.7	1,800.7	1,800.0	1,800.5
Gas Volumetric Flow Rate Data		Run 1	Run 2	Run 3	Average
Average Stack Gas Velocity, vs	ft/s	73.4	73.6	74.2	73.7
Stack Gas Volumetric Flow Rate, Q	acím	138,679	139,027	140,326	139,344
Stack Gas Standard Volumetric Flow Rate, Qs	scfm	113,642	113,598	114,511	113,917
Stack Gas Dry Standard Volumetric Flow Rate, Q _{sd}	dscfm	98,536	97,691	99,342	98,523
Percent of Isokinetic Sampling, I	%	100.5	<u>99.9</u>	99.6	100.0
Gas Concentrations and Emission Rates		Run 1	Run 2	Run 3	Average
Mass of Fillerable PM Collected, mn	mg	2.43	2,59	3.67	2.90
Filterable PM Concentration, c _s	gr/dscf	0.00041	0.00044	0.00061	0.00049
ilterable PM Concentration at Stack Conditions, Cs@stack conditions	mg/wacm	0.661	0,706	0.994	0.787
ilterable PM Concentration, Cs [Actual Conditions, Wet Basis]	lb/1,000 lbs	0.001	0.001	0.001	0.001
ilterable PM Concentration, C ₅₅₀ [Actual Conditions, Wet Basis]	lb/1,000 lbs @ 50% EA	0,001	0.001	0.001	0.001
Filterable PM Mass Emission Rate, E	lb/hr	0,34	0.37	0.52	0.41
Filterable PM, Ib/mmBtu, E	lb/mmBtu	0,0008	0.0009	0.0013	0.0010
Filterable PM, tpy [Assumes 8,760 Hrs/Yr Operation]	lpy	1.50	1.61	2.28	1.80