COMPLIANCE TEST REPORT GLGT COMPRESSOR STATION 8 CRYSTAL FALLS, MI COMBUSTION TURBINE NO. 802

December 2, 2021

() TC Energy

TC Energy's Great Lakes Gas Transmission Partnership Crystal Falls, MI 151 Oss Road Crystal Falls, MI Iron County Permit: No. MI-ROP-N3760-2021

Prepared by:



Environmental Quality Management, Inc. 1280 Arrowhead Court Suite 2 Crown Point, IN 46307 (219) 661-9900 www.eqm.com

PN: 050614.0099.047

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TC Energy GLGT Station 8-802 Project Number: 050614.0099.047

PREFACE

I, Karl Mast, do hereby certify that the source emissions testing conducted at TC Energy in Crystal Falls, MI was performed in accordance with the procedures set forth by the United States Environmental Protection Agency, and that the data and results submitted within this report are an exact representation of the testing.

Karl Mast Test Supervisor

I, Karl Mast, do hereby attest that all work on this project was performed under my direct supervision, and that this report accurately and authentically presents the source emissions testing conducted at Great Lakes Gas Transmission's Crystal Falls Compressor Station in Crystal Falls, MI.

Mast

Karl Mast Test Supervisor

SUMMARY

The compliance testing was performed on the Combustion Turbine No.802 system in accordance with the requirements of the Title 40, Code of Federal Regulations, Part 60, Subpart GG, (60.335(B)(2)) and at ambient temperature greater than 0 °F. The results of the testing are detailed in the following tables.

| | EU-UNIT 802 Summary Results | | | | | | | |
|---|-----------------------------|-----------|----------|--------|---------|-------|--|--|
| Parameter | High | Mid- High | Mid- Low | Low | Average | Limit | | |
| NO _x ppm @ 15% O ₂ | 118.036 | 100.546 | 83.867 | 70.820 | 93.317 | 175.2 | | |
| NO _x lb/hr | 55.357 | 41.092 | 29.360 | 21.237 | 36.762 | 89 | | |
| CO ppm @ 15% O2 | 20.313 | 20.576 | 25.293 | 35.116 | 25.325 | 31.9 | | |
| CO lb/hr | 5.798 | 5.119 | 5.390 | 6.405 | 5.678 | 14.8 | | |

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1. INTRODUCTION

This report presents the results of the source emissions testing conducted by Environmental Quality Management, Inc. (EQM) for TC Energy's Great Lakes Gas Transmission (GLGT) at Crystal Falls compressor station, near Crystal Falls, MI, which is located in Iron County.

The primary purpose of this testing program was to conduct emissions testing to determine compliance with operating permit No. MI-ROP-N3760-2021 for Combustion EU-UNIT 802 Turbine (No. 802) at GLGT's gas compressor facility.

EQM's responsibility was to conduct the compliance testing for the O2, CO, and NOx emissions rates and perform data reduction for conformance evaluation. Great Lakes Gas Transmission's responsibility was to maintain process operating parameters and to assist in providing process operating data per compliance test requirements. Where screen prints from the plant may not contain some information that is required, the data was manually recorded and hand written or typed on the screen prints from the instruments that produce the information.

The following report provides information pertaining to TC Energy's process operations, and Compliance testing. The Compliance testing conducted on the Combustion Turbine No. 802 was performed on December 2, 2021, from 8:40 A.M. to 1:32 P.M.

The following requirements were specific for the testing program:

- 1. Equipment calibrations were performed, and calibration data provided.
- 2. Three (3) twenty (20) minute O₂, CO, and NOx test runs performed at the Combustion Turbine No. 802 at four (4) load conditions, with the highest load at maximum achievable horsepower considering pipeline conditions and ambient temperature pursuant to EPA, Title 40, Code of Federal Regulations, Part 60 Subpart GG.
- 3. Process manufacturing operations maintained at 100%-50% of capacities and production and fuel consumption rates recorded during the emissions testing periods.
- 4. All testing and analyses performed in accordance with current EPA test methodologies and analytical procedures for O₂ CO, and NOx emissions determinations.
- 5. Stratification was found to be less than 5% in the turbine exhaust.

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The testing program was approved by and/or coordinated with Tyrah Lydia, TC Energy's GLGT. The emission testing was managed and performed by Karl Mast, Manager, Emission Measurement and Project Manager, EQM. The emission testing was not observed by MEGLE.

2. TEST RESULTS SUMMARY

The compliance testing was performed on the Combustion Turbine No. 802 system in accordance with the requirements of the Title 40, Code of Federal Regulations, Part 60, Subpart GG, (0.335(B)(2)) and at ambient temperature greater than 0 °F. A summary of the test results provided below:

| Table 1. EU-UNIT 802-Summary Results | | | | | | | |
|---|---------|-----------|----------|--------|---------|-------|--|
| Parameter | High | Mid- High | Mid- Low | Low | Average | Limit | |
| NO _x ppm @ 15% O ₂ | 118.036 | 100.546 | 83.867 | 70.820 | 93.317 | 175.2 | |
| NO _x lb/hr | 55.357 | 41.092 | 29.360 | 21.237 | 36.762 | 89 | |
| CO ppm @ 15% O2 | 20.313 | 20.576 | 25.293 | 35.116 | 25.325 | 31.9 | |
| CO lb/hr | 5.798 | 5.119 | 5.390 | 6.405 | 5.678 | 14.8 | |

Based on the information provided above, the Combustion Turbine No. 802 and met the acceptance criteria during the course of the testing. A complete list of performance parameters for each test run that was performed at the stack sampling locations can be found in Tables 2-11.

Additional testing information may be found in Appendix A.

| Run | 1 | 2 | 3 | |
|---------------------------------------|----------|----------|----------|----------|
| Date | 12/02/21 | 12/02/21 | 12/02/21 | |
| Time | 8:40 | 9:01 | 9:22 | |
| Engine Operating Conditions | High 802 | High 802 | High 802 | Averages |
| Unit Horsepower from Control Panel | 12,710.0 | 14,312.0 | 13,150.0 | 13,390.7 |
| % Load | 55.3 | 62.2 | 57.2 | 58.2 |
| Unit Speed (rpm) CT/GG/GP/Jet | 15,418.0 | 15,446.0 | 15,443.0 | 15,435.7 |
| % CT Speed | 93.7 | 93.9 | 93.9 | 93.8 |
| Gas Compressor Speed (rpm) PT/Booster | 5,830.0 | 5,866.0 | 5,873.0 | 5,856.3 |
| % PT Speed | 79.3 | 79.8 | 79.9 | 79.7 |
| Turbine Exhaust Temp T5 | 1,350.0 | 1,351.0 | 1,351.0 | 1,350.7 |
| Compressor Suction Pressure (PSIG) | 750.0 | 749.0 | 748.0 | 749.0 |
| Compressor Suction Temperature (°F) | 44.0 | 44.0 | 46.0 | 44.7 |
| Compressor Discharge Pressure (PSIG) | 831.0 | 831.0 | 831.0 | 831.0 |
| Compressor Discharge Temperature (°F) | 77.0 | 82.0 | 81.0 | 80.0 |
| Compressor Flow (MMSCF/D) | 1164.0 | 1165.0 | 1174.0 | 1,167.7 |
| Heat Rate (BTÚ(LHV)/HP-hr) | 8,996.9 | 8,048.7 | 8,810.9 | 8,618.8 |
| Ambient Conditions | | | | |
| Ambient Temperature (°F) | 42.50 | 43.20 | 42.20 | 42.63 |
| Barometric Pressure (psi) | 28.00 | 28.00 | 28.00 | 28.00 |
| Ambient Relative Humidity (%) | 81.00 | 81.00 | 81.00 | 81.00 |
| Absolute Humidity (grains/LB) | 17.00 | 17.46 | 16.80 | 17.09 |

Table 2. Operating Parameters and Ambient Conditions -High Load-Turbine No. 802

Table 3. Emissions Concentrations, Calculated Mass Emissions/Calculated & Fuel Flows -High Load-Turbine No. 802

| Run | 1 | 2 | 3 | |
|---|---|-----------|---------------------|-----------|
| Date | 12/02/21 | 12/02/21 | 12/02/21 | |
| Time | 8:40 | 9:01 | 9:22 | |
| Emissions Concentrations & Calculated Mass Emissions | High 802 | High 802 | High 802 | Averages |
| NO _x ppm (BIAS Corrected) | 113.210 | 114.220 | 114.060 | 113.830 |
| NO _X g/BHP-HR | 1.944 | 1.752 | 1.942 | 1.880 |
| NO _X LB/HR 89 | 54.484 | 55.278 | 56.310 | 55.357 |
| NO _X (ppm @ 15% O ₂) 175.2 | 116.977 | 117.814 | 119.318 | 118.036 |
| NO _X (ppm @ 15% O ₂ , ISO) | 82.610 | 83.129 | 84.296 | 83.345 |
| NOx LB/MMBTU | 0.431 | 0.434 | 0,439 | 0.435 |
| NO _X Tons/Year | 238.640 | 242.117 | 246.636 | 242.464 |
| NO _X LB/SCF Fuel | 4.513E-04 | 4.546E-04 | 4.604E-04 | 4.554E-04 |
| NO _X LB/MMSCF Fuel | 4.513E+02 | 4.546E+02 | 4.604E+02 | 455.425 |
| CO ppm (BIAS Corrected) | 19.940 | 19.410 | 19.420 | 19.590 |
| CO g/BHP-HR | 0.208 | 0.181 | 0.201 | 0.197 |
| CO LB/HR 14.8 | 5.841 | 5.718 | 5.836 | 5.798 |
| CO LB/MMBTU ** | 0.046 | 0.045 | 0.046 | 0.046 |
| CO (ppm @ 15% O ₂) 31.9 | 20,604 | 20.021 | 20.315 | 20.313 |
| CO (ppm @ 15% O ₂ , ISO) | 14.550 | 14.127 | 14.352 | 14.343 |
| CO Tons/Year | 25.586 | 25.045 | 25.561 | 25.397 |
| CO LB/SCF Fuel | 4.839E-05 | 4.702E-05 | 4.771E-05 | 4.771E-05 |
| CO LB/MMSCF Fuel | 48.390 | 47.021 | 47.713 | 47.708 |
| % O ₂ (BIAS Corrected) | 15.190 | 15.180 | 15.260 | 15.210 |
| Calculated Flows | | | | |
| Fuel Flow- (SCFM) | 2016.00 | 2030.83 | 2042.67 | 2029.83 |
| Fuel Flow- (SCFH) | 120,960 | 121,850 | 122,560 | 121,790 |
| Exhaust Flow (LB/HR) | 267,381.0 | 268,852.8 | 274,127.1 | 270,120 |
| Exhaust Flow Method 19 (scfm) | 67,043 | 67,419 | 68,773 | 67,745 |
| BSAC, #/BHP-hr | 23.17 | 20.69 | 22.97 | 22 |
| Fuel Flow Measurements | | | | |
| Fuel Flow From Screen(MSCFH) | 120.96 | 121.85 | 122.56 | 121.79 |
| ** BASED ON FUEL SPECIFIC DRY F-FACTOR CALCULATION | Run 1 | Run 2 | Run 3 | |
| * BASED ON CARBON BALANCE (STOICH. + O2) - A/F IS TOTAL MASS RATIO | ² алын алын тороо алын 2 ⁴ т | | · · · · · · · · · · | |

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Table 4. Operating Parameters and Ambient Conditions – Mid-High Load-Turbine No. 802 10 11 12 12/02/21 12/02/21 12/02/21

| Run | 10 | 11 | 12 | |
|--|--------------|--------------|--------------|----------|
| Date | 12/02/21 | 12/02/21 | 12/02/21 | |
| Time | 12:30 | 12:51 | 13:12 | |
| Engine Operating Conditions | Mid High 802 | Mid High 802 | Mid High 802 | Averages |
| Unit Horsepower from Control Panel | 8,457.0 | 8,928.0 | 9,546.0 | 8,977.0 |
| % Load | . 36.8 | 38.8 | 41.5 | 39.0 |
| Unit Speed (rpm) CT/GG/GP/Jet | 15,130.0 | 15,127.0 | 15,111.0 | 15,122.7 |
| % CT Speed | 92.0 | 92.0 | 91.9 | 91.9 |
| Gas Compressor Speed (rpm) PT/Booster | 5,476.0 | 5,477.0 | 5,475.0 | 5,476.0 |
| % PT Speed | 74.5 | 74.5 | 74.5 | 74.5 |
| Turbine Exhaust Temp T5 | 1,277.0 | 1,270.0 | 1,268.0 | 1,271.7 |
| Compressor Suction Pressure (PSIG) | 780 | 777 | 776.0 | 777.7 |
| Compressor Suction Temperature (°F) | 45 | 43 | 45.0 | 44.3 |
| Compressor Discharge Pressure (PSIG) | 805 | 806 | 806.0 | 805.7 |
| Compressor Discharge Temperature (^o F) | 68 | 68 | 69.0 | 68.3 |
| Compressor Flow (MMSCF/D) | 1159 | 1155 | 1147.0 | 1,153.7 |
| Heat Rate (BTU(LHV)/HP-hr) | 11,905.1 | 11,226.2 | 10,486.5 | 11,205.9 |
| Ambient Conditions | | | | |
| Ambient Temperature (°F) | 42.0 | 40.5 | 40.30 | 40.93 |
| Barometric Pressure (psi) | 28.10 | 28.20 | 28.20 | 28.17 |
| Ambient Relative Humidity (%) | 85.0 | 85.0 | 85.00 | 85.00 |
| Absolute Humidity (grains/LB) | 17.44 | 16.39 | 16.27 | 16.70 |



Table 5. Emissions Concentrations, Calculated Mass Emissions/Calculated & Fuel Flows –Mid-High Load-Turbine No. 802

| Run | 10 | 11 | 12 | |
|--|--------------|---------------------------------------|--------------|-----------|
| Date | 12/02/21 | 12/02/21 | 12/02/21 | |
| Time | 12:30 | 12:51 | 13:12 | |
| Emissions Concentrations & Calculated Mass Emissions | Mid High 802 | Mid High 802 | Mid High 802 | Averages |
| NO _x ppm (BIAS Corrected) | 90.263 | 90.270 | 90.090 | 90.208 |
| NO _X g/BHP-HR | 2.210 | 2.088 | 1.947 | 2.082 |
| NO _X LB/HR 89 | 41.206 | 41.101 | 40.969 | 41.092 |
| NO _X (ppm @ 15% O ₂) 175.2 | 100.481 | 100.679 | 100.478 | 100.546 |
| NO _X (ppm @ 15% O ₂ , ISO) | 70.832 | 70.839 | 70.998 | 70.890 |
| NOx LB/MMBTU | 0.370 | 0.371 | 0.370 | 0.370 |
| NO _X Tons/Year | 180.483 | 180.023 | 179.444 | 179.984 |
| NO _X LB/SCF Fuel | 3.877E-04 | 3.885E-04 | 3.877E-04 | 3.879E-04 |
| NO _X LB/MMSCF Fuel | 3.877E+02 | 3.885E+02 | 3.877E+02 | 387.943 |
| CO ppm (BIAS Corrected) | 18.530 | 18.420 | 18.430 | 18.460 |
| CO g/BHP-HR | 0.276 | 0.259 | 0.242 | 0.259 |
| CO LB/HR 14.8 | 5.149 | 5.105 | 5.102 | 5.119 |
| CO LB/MMBTU ** | 0.046 | 0.046 | 0.046 | 0.046 |
| CO (ppm @ 15% O ₂) 31.9 | 20.628 | 20.544 | 20.555 | 20.576 |
| CO (ppm @ 15% O ₂ , ISO) | 14.581 | 14.521 | 14.533 | 14.545 |
| CO Tons/Year | 22.553 | 22.361 | 22.345 | 22.420 |
| CO LB/SCF Fuel | 4.845E-05 | 4.825E-05 | 4.828E-05 | 4.832E-05 |
| CO LB/MMSCF Fuel | 48.447 | 48.250 | 48.276 | 48.324 |
| % O2 (BIAS Corrected) | 15.600 | 15.610 | 15.610 | 15.607 |
| Calculated Flows | | | | |
| Fuel Flow - (SCFM) | 1775.00 | 1767.00 | 1764.83 | 1768.94 |
| Fuel Flow- (SCFH) | 106,500 | 106,020 | 105,890 | 106,137 |
| Exhaust Flow (LB/HR) | 253,156.4 | 252,587.8 | 252,292.4 | 252,679 |
| Exhaust Flow Method 19 (scfm) | 63,595 | 63,428 | 63,350 | 63,458 |
| BSAC, #/BHP-hr | 33.00 | 31.18 | 29.13 | 31 |
| Fuel Flow Measurements | | | | |
| Fuel Flow From Screen(MSCFH) | 106.50 | 106.02 | 105.89 | 106.14 |
| ** BASED ON FUEL SPECIFIC DRY F-FACTOR CALCULATION | Run 10 | Run 11 | Run 12 | |
| * BASED ON CARBON BALANCE (STOICH. + O2) - A/FIS TOTAL MASS RATIO | | · · · · · · · · · · · · · · · · · · · | | |

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| Run | 7 | 8 | 9 | |
|---------------------------------------|-------------|-------------|-------------|----------|
| Date | 12/02/21 | 12/02/21 | 12/02/21 | |
| Time | 11:23 | 11:44 | 12:05 | |
| Engine Operating Conditions | Mid Low 802 | Mid Low 802 | Mid Low 802 | Averages |
| Unit Horsepower from Control Panel | 7,771.0 | 7,372.0 | 7,116.0 | 7,419.7 |
| % Load | 33.8 | 32.1 | 30.9 | 32.3 |
| Unit Speed (1pm) CT/GG/GP/Jet | 14,804.0 | 14,829.0 | 14,828.0 | 14,820.3 |
| % CT Speed | 90.0 | 90.1 | 90.1 | 90.1 |
| Gas Compressor Speed (rpm) PT/Booster | 5,086.0 | 5,087.0 | 5,088.0 | 5,087.0 |
| % PT Speed | 69.2 | 69.2 | 69.2 | 69.2 |
| Furbine Exhaust Temp T5 | 1,200.0 | 1,198.0 | 1,198.0 | 1,198.7 |
| Compressor Suction Pressure (PSIG) | 780.0 | 780.0 | 781 | 780.3 |
| Compressor Suction Temperature (°F) | 45.0 | 45.0 | 45 | 45.0 |
| Compressor Discharge Pressure (PSIG) | 804.0 | 804.0 | 804 | 804.0 |
| Compressor Discharge Temperature (°F) | 66.0 | 67.0 | 66 | 66,3 |
| Compressor Flow (MMSCF/D) | 1078.0 | 1066.0 | 1074 | 1,072.7 |
| Heat Rate (BTU(LHV)/HP-lu) | 11,035.1 | 11,667.0 | 12,096.0 | 11,599.4 |
| Ambient Conditions | | | | |
| Ambient Temperature (°F) | 42.10 | 43,60 | 42.9 | . 42.87 |
| Barometric Pressure (psi) | 28.10 | 28.10 | 28.10 | 28.10 |
| Ambient Relative Humidity (%) | 84,00 | 84.00 | 83.0 | 83.67 |
| Absolute Humidity (grains/LB) | 17.30 | 18,33 | 17.63 | 17.75 |

 Table 6. Operating Parameters and Ambient Conditions – Mid-Low Load-Turbine No. 802

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Table 7. Emissions Concentrations, Calculated Mass Emissions/Calculated & Fuel Flows – Mid-Low Load-Turbine No. 802

| Run | 7 | 8 | 9 | |
|---|--------------|-------------|----------------|-----------|
| Date | 12/02/21 | 12/02/21 | 12/02/21 | |
| Time | 11:23 | 11:44 | 12:05 | |
| Emissions Concentrations & Calculated Mass Emissions | Mid Losy 802 | Mid Low 802 | Mid Low 802 | Averages |
| NO _x ppm (BIAS Corrected) | 70.980 | 71.460 | 71.620 | 71.353 |
| NO _x g/BHP-HR | 1.687 | 1.810 | 1.896 | 1.798 |
| NO _X LB/HR 89 | 28.908 | 29,423 | 29.748 | 29.360 |
| NO _X (ppm @ 15% O ₂) 175.2 | 82.763 | 83.987 | 84.851 | 83.867 |
| NO _X (ppm @ 15% O ₂ , ISO) | 58.391 | 59.493 | 59.718 | 59.201 |
| NOx LB/MMBTU | 0.305 | 0.309 | 0.312 | 0.309 |
| NO _X Tons/Year | 126.618 | 128.872 | 130.298 | 128.596 |
| NO _x LB/SCF Fuel | 3.193E-04 | 3.241E-04 | 3.274E-04 | 3.236E-04 |
| NO _x LB/MMSCF Fuel | 3.193E+02 | 3.241E+02 | 3.274E+02 | 323.588 |
| CO ppm (BIAS Corrected) | 21.640 | 21.460 | 21,460 | 21.520 |
| CO g/BHP-HR | 0.313 | 0.331 | 0.346 | 0.330 |
| CO LB/HR 14.8 | 5,365 | 5.379 | 5.426 | 5.390 |
| CO LB/MMBTU ** | 0.057 | 0.057 | 0.057 | 0.057 |
| CO (ppm @ 15% O ₂) 31.9 | 25.232 | 25.222 | 25.424 | 25.293 |
| CO (ppm @ 15% O ₂ , ISO) | 17.824 | 17.785 | 17.932 | 17.847 |
| CO Tons/Year | 23.498 | 23.558 | 23.765 | 23.607 |
| CO LB/SCF Fuel | 5.926E-05 | 5.924E-05 | 5.971E-05 | 5.940E-05 |
| CO LB/MMSCF Fuel | 59.261 | 59.237 | 59.712 | 59.403 |
| % O2 (BIAS Corrected) | 15.840 | 15.880 | 15.920 | 15.880 |
| Calculated Flows | | | | |
| Fuel Flow - (SCFM) | 1511.83 | 1516.33 | 1517.50 | 1515.22 |
| Fuel Flow - (SCFH) | 90,710 | 90,980 | 91,050 | 90,913 |
| Exhaust Flow (LB/HR) | 225,291.8 | 227,574.3 | 229,457.3 | 227,441 |
| Exhaust Flow Method 19 (scfm) | 56,735 | 57,358 | 57,863 | 57,319 |
| BSAC, #/BHP-lu | 32.03 | 34.13 | 35.67 | 34 |
| Fuel Flow Measurements | | | STAR LETE STAR | |
| Fuel Flow From Screen(MSCFH) | 90.71 | 90.98 | 91.05 | 90.91 |
| ** BASED ON FUEL SPECIFIC DRY F-FACTOR CALCULATION | Run 7 | Run 8 | Run 9 | |
| * BASED ON CARBON BALANCE (STOICH, + O2) - A/F IS TOTAL MASS RATIO | | | · · · · | · |

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| Run | 4 | 5 | 6 | |
|---------------------------------------|----------|----------|----------|----------|
| Date | 12/02/21 | 12/02/21 | 12/02/21 | |
| Time | 10:15 | 10:36 | 10:57 | |
| Engine Operating Conditions | Low 802 | Low 802 | Low802 | Averages |
| Unit Horsepower from Control Panel | 5,846.0 | 5,822.0 | 6,136.0 | 5,934.7 |
| % Load | 25.4 | 25.3 | 26.7 | 25.8 |
| Unit Speed (rpm) CT/GG/GP/Jet | 14,470.0 | 14,473.0 | 14,462.0 | 14,468.3 |
| % CT Speed | 88.0 | 88.0 | 87.9 | 88.0 |
| Gas Compressor Speed (rpm) PT/Booster | 4,700.0 | 4,700.0 | 4,699.0 | 4,699.7 |
| % PT Speed | 63.9 | 63.9 | 63.9 | 63.9 |
| Turbine Exhaust Temp T5 | 1,130.0 | 1,125.0 | 1,128.0 | 1,127.7 |
| Compressor Suction Pressure (PSIG) | 769.0 | 771.0 | 778.0 | 772.7 |
| Compressor Suction Temperature (°F) | 44.0 | 46.0 | 44.0 | 44.7 |
| Compressor Discharge Pressure (PSIG) | 811.0 | 810.0 | 804.0 | 808.3 |
| Compressor Discharge Temperature (°F) | 53 | 54.0 | 64.0 | 57.0 |
| Compressor Flow (MMSCF/D) | 953.0 | 953.0 | 972.0 | 959.3 |
| Heat Rate (BTU(LHV)/HP-hr) | 12,725.0 | 12,572.9 | 11,935.7 | 12,411.2 |
| Ambient Conditions | | | | |
| Ambient Temperature (°F) | 42.10 | 42.40 | 42.50 | 42.33 |
| Barometric Pressure (psi) | 28.10 | 28.10 | 28.10 | 28.10 |
| Ambient Relative Humidity (%) | 84.00 | 81.00 | 81.00 | 82.00 |
| Absolute Humidity (grains/LB) | 17.30 | 16.87 | 16.94 | 17.04 |

 Table 8. Operating Parameters and Ambient Conditions- Low Load-Turbine No. 802

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Table 9. Emissions Concentrations, Calculated Mass Emissions/Calculated & Fuel Flows -Low Load-Turbine No. 802

| Run | 4 | 5 | 6 | ŕ |
|---|-----------|-----------|-----------|-----------|
| Date | 12/02/21 | 12/02/21 | 12/02/21 | |
| Time | 10:15 | 10:36 | 10:57 | |
| Emissions Concentrations & Calculated Mass Emissions | Low 802 | Low 802 | Law 802 | Averages |
| NO _x ppm (BIAS Corrected) | 61.800 | 56.330 | 56.480 | 58.203 |
| NO _{x g} /BHP-HR | 1.725 | 1.612 | 1.537 | 1.625 |
| NO _X LB/HR 89 | 22.230 | 20.687 | 20.796 | 21.237 |
| NO _X (ppm @ 15% O ₂) 175.2 | 73.364 | 69.384 | 69.714 | 70.820 |
| NO _X (ppm @ 15% O ₂ , ISO) | 51.823 | 48.910 | 49.137 | 49.957 |
| NOx LB/MMBTU | 0.270 | 0.255 | 0.257 | 0.261 |
| NO _X Tons/Year | 97.365 | 90.608 | 91.086 | 93.020 |
| NO _X LB/SCF Fuel | 2.831E-04 | 2.677E-04 | 2.690E-04 | 2.732E-04 |
| NO _X LB/MMSCF Fuel | 2.831E+02 | 2.677E+02 | 2.690E+02 | 273.250 |
| CO ppm (BIAS Corrected) | 26.100 | 30.160 | 30.150 | 28.803 |
| CO g/BHP-HR | 0.443 | 0.525 | 0.500 | 0.489 |
| COLB/HR 14.8 | 5.715 | 6.742 | 6.757 | 6.405 |
| CO LB/MMBTU ** | 0.069 | 0.083 | 0.083 | 0.079 |
| CO (ppm @ 15% O ₂) 31.9 | 30.984 | 37.149 | 37.214 | 35.116 |
| CO (ppm @ 15% O ₂ , ISO) | 21.887 | 26.187 | 26.230 | 24.768 |
| CO Tons/Year | 25.030 | 29.530 | 29.598 | 28.053 |
| CO LB/SCF Fuel | 7.277E-05 | 8.725E-05 | 8.740E-05 | 8.247E-05 |
| CO LB/MMSCF Fuel | 72.769 | 87.249 | 87.402 | 82.473 |
| % O2 (BIAS Corrected) | 15.930 | 16.110 | 16.120 | 16.053 |
| Calculated Flows | | | | |
| Fuel Flow - (SCFM) | 1311.50 | 1290.50 | 1291.17 | 1297.72 |
| Fuel Flow - (SCFH) | 78,690 | 77,430 | 77,470 | 77,863 |
| Exhaust Flow (LB/HR) | 198,829.4 | 202,410.0 | 202,914.8 | 201,385 |
| Exhaust Flow Method 19 (scfm) | 50,109 | 51,159 | 51,293 | 50,854 |
| BSAC, #/BHP-hr | 37.60 | 38.53 | 36.65 | 38 |
| Fuel Flow Measurements | | | | |
| Fuel Flow From Screen(MSCFH) | 78.69 | 77.43 | 77.47 | 77.86 |
| ** BASED ON FUEL SPECIFIC DRY F-FACTOR CALCULATION | Run 4 | Run 5 | Run 6 | |
| * BASED ON CARBON BALANCE (STOICH. + O2) - A/F IS TOTAL MASS RATIO | | | | |

3. PROCESS DESCRIPTION

TC Energy's GLGT Crystal Falls Compressor Station is located in Crystal Falls, Michigan and operates a General Electric Model LM1600 stationary gas turbine, labeled EU-Unit 802, and burns only pipeline quality natural gas. The unit peak load HP rating is 23,000 at ISO conditions. The plant is located at 151 Oss Road, Crystal Falls, MI

The General Electric LM1600 gas turbine is a simple cycle, natural gas fired, split-shaft turbine. In a simple cycle turbine, filtered atmosphere air is first compressed by the axial flow compressor. The hot compressed air is then fired with natural gas in the combustor. The hot exhaust gases expand through two turbine stages. The gas producer (G.P.) turbine drives the axial flow air while the power turbine (P.T.) drives the centrifugal pipeline compressor. The pipeline gas compressor moves natural gas through the pipeline by compressing it from an initial "suction" state to a more compressed "discharge" state.

| Table 10. Turbine No. 802 Production Data | | | |
|---|-----------|----------|---------|
| Parameter | HP | СТ | PT |
| High | 13,390.7 | 15,435.7 | 5,856.3 |
| Mid-High | 8,977.0 | 15,122.7 | 5,476.0 |
| Mdi-Low | 7,419.7 | 14,820.3 | 5,087.0 |
| Low | • 5,934.7 | 14,468.3 | 4,699.7 |
| Rated | 23,000 | 16,450 | 7,350 |

The following tables provide a summary of the production rates for the Turbine No. 802 during the test:

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Figure 1. Flow Schematic



Additional Information pertaining to the Fuel Flows may be found in Appendix B.

4. TEST PROCEDURES

EQM and EQM's affiliates and subcontractors use current U.S. EPA accepted testing methodologies in their Air Quality Programs as listed in the U.S. Code of Federal Regulations, Title 40, Part 60, Appendix A. For this testing program, the following specific methodologies were utilized:

- U.S. EPA Method 3A Determination of Oxygen and Carbon Dioxide Concentrations in Emissions From Stationary Sources (Instrumental Analyzer Procedure)
- U.S. EPA Method 7E Determination of Nitrogen Oxides Emissions From Stationary Sources (Instrumental Analyzer Procedure)
- U.S. EPA Method 10 Determination of Carbon Monoxide Emissions From Stationary Sources (Instrumental Analyzer Procedure)
- U.S. EPA Method 19– Determination of Volumetric Flow Rate From Stationary Sources

USEPA Methods 3A, 7E, 10 and 19 were performed at the Exhaust Stack sampling location by continuously extracting a gas sample from the stack through a single point stainless steel sample probe. The extracted sample was pulled through a series of filters to remove any particulate matter. Directly after the probe, the sample was conditioned by a series of refrigeration dryers to remove moisture from the gas stream. After the refrigeration dryers, the sample was transported through a Teflon® line to the analyzers. The flow of the stack gas sample was regulated at a constant rate to minimize drift.

At the start of the day, each monitor was checked for calibration error by introducing zero, midrange and high-range EPA Protocol 1 gases to the measurement system at a point upstream of the analyzers. In this report, the calibration error test is referred to as instrument calibration. The gas was injected into the sampling valve located at the outlet of the sampling probe. The bias test was conducted before and after each consecutive test run by introducing zero and upscale calibration gases for each monitor. The upscale calibration gases used for each monitor were the high calibration gases.

Measurement System Performance Specifications were as follows:

- Analyzer Calibration Error Less than +/- 2% of the span of the zero, mid-range and high-range calibration gases.
- Sampling System Bias Less than +/-5% of the span for the zero, mid-range and high-range calibration gases.
- Zero Drift Less than +/-3% of the span over the period of each test run.
- Calibration Drift Less than +/-3% of the span over the period of each set of runs.

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Calculations that were used in this testing event for the Unit No. 802 are as follows:

Calibration Correction

$$C_{GAS} = \left(C_R - C_O\right) \frac{C_{MA}}{C_M - C_O}$$

Where:

| CGAS: | Corrected flue gas concentration (ppmvd) |
|------------------|--|
| C _R : | Flue gas concentration (ppmvd) |
| Co: | Average of initial and final zero checks (ppmvd) |
| См: | Average of initial and final span checks (ppmvd) |
| Cma: | Actual concentration of span gas (ppmvd) |

EPA F-Factor

$$F_{d} = \frac{\left[(3.64 \cdot H_{WI\%} \cdot 100) + (1.53 \cdot C_{WI\%} \cdot 100) \right]}{\frac{GCV}{\rho_{FuelGas}}} \cdot 10^{6} + \frac{\left[(0.14 \cdot N_{2WI\%} \cdot 100) - (0.46 \cdot O_{2WI\%} \cdot 100) \right]}{\frac{GCV}{\rho_{FuelGas}}} \cdot 10^{6}$$

Where:

| F_d : | Fuel specific F-factor, dscf/MMBtu |
|-----------------|-------------------------------------|
| Hwt%: | Hydrogen weight percent |
| Cwt%: | Carbon weight percent |
| N2 <i>wt%</i> : | Nitrogen weight percent |
| $O_{2Wt\%}$: | Oxygen weight percent |
| GCV: | Heating value of the fuel, BTU/dscf |
| ρFuel Gas∶ | Density of the fuel gas, lb/scf |

NO_x Corrected to 15% O₂

$$Em = NO_X \left(\frac{5.9}{20.9 - \%O_2}\right)$$

Where:

| Em: | Pollutant concentration corrected to 15% O ₂ , ppm |
|-------------------|---|
| NO _x : | Pollutant concentration, ppm |
| %O2: | Oxygen concentration in percent, measured on a dry basis |

Mass Emissions Calculations

The F-factor Method and guidance from Part 75 was used to calculate the mass emissions rates.

$$Em = Cd \times Fd \times \frac{20.9}{(20.9 - \%O_2)} \times Qh \times \frac{GCV}{10^6}$$

Where:

| E _m : | Pollutant emission rate, lb/hr |
|------------------|---|
| Cd: | Pollutant concentration, lb/scf |
| Fd: | Fuel specific F-factor, dscf/MMBtu |
| %O2: | Oxygen concentration, dry basis |
| Qh: | Fuel rate from calibrated AGA specified |
| | Meter, scfh. |
| GCV: | Heating value of the fuel, Btu/scf |

| To Convert f | rom: To | Multiply by: |
|---------------------|---------|--------------|
| ppm CO | lb/scf | 7.268 x 10-8 |
| ppm NO _x | lb/scf | 1.194 x 10-7 |

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5. QUALITY ASSURANCE PROCEDURES

Each reference method presented in the U.S. Code of Federal Regulations details the instrument calibration requirements, sample recovery and analysis, data reduction and verification, types of equipment required, and the appropriate sampling and analytical procedures to ensure maximum performance and accuracy. EQM and EQM's affiliates and subcontractors adhere to the guidelines for quality control set forth by the United States Environmental Protection Agency. These procedures are outlined in the following documents:

- Code of Federal Regulations, Title 40, Part 51
- Code of Federal Regulations, Title 40, Part 60
- Quality Assurance Handbook, Volume 1, EPA 600/9-76-005
- Quality Assurance Handbook, Volume 2, EPA 600/4-77-027a
- Quality Assurance Handbook, Volume 3, EPA 600/4-77-027b

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6. CONCLUSIONS

An Emissions Test was conducted on the Turbine No. 802 at TC Energy's GLGT Pipeline Company's Crystal Falls Compressor Station located in Crystal Falls, MI. The testing was conducted on December2, 2021.

During the course of the testing, the Turbine No. 802 conformed to the requirements of Code of Federal Regulations, Title 40, Part 60, Appendix A.

The usefulness and/or significance of the emissions values presented in this document as they relate to the compliance status of the Turbine No. 802 emissions shall be determined by others.

For additional information pertaining to the testing program see Appendix E of this report.

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A. FIELD TEST DATA