**Consumers Energy** 

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# PM<sub>10</sub>, VOCs, and HCHO ROP Test Report

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EUGT2B

AIR QUALITY DIVISION

Consumers Energy Company Zeeland Generating Station 425 Fairview Road Zeeland, Michigan 49464 SRN: N6521

February 1, 2019

## Test Dates: December 11-12, 2018

Test Performed by the Consumers Energy Company Regulatory Compliance Testing Section Air Emissions Testing Body Laboratory Services Section Work Order No. 6500411 Version No.: 0

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### **EXECUTIVE SUMMARY**

Consumers Energy Regulatory Compliance Testing Section (RCTS) personnel conducted filterable particulate matter (FPM), condensable particulate matter (CPM), volatile organic compounds (VOCs) and formaldehyde (HCHO) testing at the exhaust of gas turbine EUGT2B (Unit 2B) operating at the Zeeland Generating Station in Zeeland, Michigan. Unit 2B is a natural gas fired combined-cycle combustion turbine that generates electricity. The test program, performed December 11 and 12, 2018, was conducted to satisfy testing requirements in renewable operating permit (ROP) MI-ROP-B6521-2015a and reestablish lb/mmBtu emission factors to be used with heat input determinations to calculate mass emission rates as specified in Appendix 5 of the ROP.

Triplicate 120-minute FPM, CPM, and VOCs test runs and 60-minute HCHO test runs were conducted following the procedures in USEPA Reference Methods (RM) 1, 2, 4, 5, 18 and 19 in 40 CFR 60, Appendix A, RM 320 in 40 CFR 63, Appendix A and RM 202 in 40 CFR 51, Appendix M. One set of test runs was conducted with Unit 2B operating at 100% load, and another set of test runs was conducted at 70% load as required in the facility's air permit. There were no deviations from the approved stack test protocol or the USEPA Reference Methods therein. The Unit 2B PM less than 10 microns in diameter ( $PM_{10}$ ), VOCs and HCHO results are summarized in the following table.

Parameter	Units		Run	n de Stanfont <sub>de</sub> site Geografie de Capello Geografie de Capello	Average	Emission Limit	
		1	2	3		ROP	
Unit 2B - 70	% Load						
	lb/hr	3.77	2.92	3.35	3.35	14.7	
$PM_{10}$	ton/yr	16.5	12.8	14.7	14.7	64.4	
	lb/mmBtu	0.0023	0.0018	0.0021	0.0021	N/A*	
voo t	lb/hr	0.23	0.22	0.20	0.22	16.8	
VOCs <sup>†</sup>	ton/yr	1.0	1.0	0.9	1.0	73.6	
	lb/mmBtu	1.4E-04	1.3E-04	1.2E-04	1.3E-04	N/A*	
HCHO <sup>‡</sup>	ton/yr	1.0	1.0	0.9	1.0	2.35 <sup>‡</sup>	
	lb/mmBtu	1.4E-04	1.3E-04	1.2E-04	1.3E-04	N/A*	
Jnit 2B - 10	0% Load					· ·	
	lb/hr	3.32	4.34	7.08	4.91	14.7	
PM <sub>10</sub>	ton/yr	14.6	19.0	31.0	21.5	64.4	
	lb/mmBtu	0.0016	0.0022	0.0036	0.0025	N/A*	
	lb/hr	0.22	0.18	0.20	0.20	16.8	
VOCs <sup>†</sup>	ton/yr	1.0	0.8	0.9	0.9	73.6	
	lb/mmBtu	1.1E-04	9.4E-05	1.0E-04	1.0E-04	N/A*	
HCHO <sup>‡</sup>	ton/yr	1.0	0.8	0.9	0.9	2.35 <sup>‡</sup>	
	lb/mmBtu	1.1E-04	9.4E-05	1.0E-04	1.0E-04	N/A*	

#### Table E-1 Executive Summary of Test Results

\*: lb/mmBtu results are used in mass emission calculations with continuous heat input to evaluate compliance with the mass emission limits

<sup>†</sup>: VOCs mass emissions calculated as sum of mass emissions of VOCs detected

\* : HCHO limit is applicable to all turbine operations, the presented limit is the permit limit divided by four

Although not consistent with the prescribed compliance methodology in the ROP, the Unit 2B PM,  $PM_{10}$ , VOC and HCHO emission results indicate compliance with the mass emission limits

in the permit. The preceding tons per year values are extrapolated assuming continuous operation at the pounds per hour emission rates observed during the testing. The facility uses lb/mmBtu emission factors in conjunction with continuous heat input determinations to calculate mass emission rates, consistent with Appendix 5 of the ROP.

Detailed test results are presented in Appendix Tables 1 and 2. Sample calculations, field data sheets, and laboratory data are presented in Appendices A, B, and C. Operating data and supporting documentation are provided in Appendices D and E.

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### 1.0 **INTRODUCTION**

This report summarizes the results of compliance particulate matter (PM), PM less than 10 microns in diameter ( $PM_{10}$ ), volatile organic compounds (VOCs), and formaldehyde (HCHO) testing conducted December 11 and 12, 2018 on EUGT2B (Unit 2B) operating at the Consumers Energy Zeeland Generating Station in Zeeland, Michigan.

This document was prepared using the Michigan Department of Environmental Quality (MDEQ) *Format for Submittal of Source Emission Test Plans and Reports* published in March of 2018. Please exercise due care if portions of this report are reproduced, as critical substantiating documentation and/or other information may be omitted or taken out of context.

#### 1.1 IDENTIFICATION, LOCATION, AND DATES OF TESTS

Consumers Energy Regulatory Compliance Testing Section (RCTS) personnel conducted  $PM_{10}$  (as the sum of filterable and condensable PM), VOCs, and HCHO tests at the dedicated exhaust of natural gas-fired combustion turbine Unit 2B operating at the Zeeland Generating Station in Zeeland, Michigan on December 11 and 12, 2018.

A test protocol was submitted to the MDEQ on October 26, 2018 and subsequently approved by Mr. Jeremy Howe, Environmental Quality Analyst, in his letter dated November 21, 2018.

#### **1.2 PURPOSE OF TESTING**

The purpose of the test was to satisfy testing requirements in renewable operating permit (ROP) MI-ROP-B6521-2015a and reestablish lb/mmBtu emission factors to be used with heat input determinations to calculate mass emission rates as specified in Appendix 5 of the ROP. The applicable emission limits are presented in Table 1-1.

arameter	Emission Limit	Units	Applicable Requirement
UGT2A, EUG	Г2В		
PM	0.03	lb/mmBtu	MI-ROP-N6521-2015a, Section 1, FGCOMBINEDCYCLE
DM	14.7	lb/hr	Emission Limits
PM <sub>10</sub>	64.4	ton/yr	
NOC	16.8	lb/hr	
voc –	73.6	ton/yr	
нсно†	9.4	ton/yr	MI-ROP-N6521-2015a, Section 1, FGSIMPLECYCLE Emission Limits & FGCOMBINEDCYCLE <sup>†</sup> Emission Limits

#### Table 1-1 Emission Limi

<sup>†</sup>: HCHO limit is applicable to all combustion turbine operations

The ROP requires that testing be performed for one simple cycle and one combined cycle unit not tested at the last test event at 100% and 70% load. Units 1A and 2A were tested in 2013. This report summarizes the testing of Unit 2B, as Unit 1B testing occurred November 27 and 28, 2018 with results previously submitted in a separate report.

#### **1.3 BRIEF DESCRIPTION OF SOURCE**

The Zeeland Generating Station operates four General Electric (GE) model 7FA natural gas fired combustion turbines.

#### **1.4 CONTACT INFORMATION**

Table 1-2 presents the names, addresses, and telephone numbers for contacts involved in this test program.

#### Table 1-2 Contact Information

Program Role	Contact	Address
EPA Regional Contact	Compliance Tracker, AE-18J 312-353-2000	Air Enforcement and Compliance Assurance U.S. Environmental Protection Agency–Region 5 77 W. Jackson Boulevard Chicago, Illinois 60604
Regulatory Agency Representative	Ms. Karen Kajiya-Mills Technical Programs Unit Manager 517-335-4874 Kajiya-Millsk@michigan.gov	Michigan Department of Environmental Quality Technical Programs Unit 525 W. Allegan, Constitution Hall, 2nd Floor S Lansing, Michigan 48933
Regulatory Agency Representative	Mr. Jeremy Howe Environmental Quality Analyst 231-878-6687 HoweJ1@michigan.gov	Michigan Department of Environmental Quality Air Quality Division 120 W. Chapin Street Cadillac, Michigan 49601
Test Facility	Mr. J. Homer Manning Environmental Health & Safety 616-237-4004 Homer.ManningIII@cmsenergy.com	Consumers Energy Company Zeeland Generating Station 425 Fairview Road Zeeland, Michigan 49464
Test Team Representative	Mr. Dillon King, QSTI Sr. Engineering Technical Analyst 989-891-5585 Dillon.King@cmsenergy.com	Consumers Energy Company D.E. Karn Power Plant 2742 North Weadock Highway, ESD Trailer #4 Essexville, Michigan 48732
Test Team Representative	Mr. Thomas Schmelter, QSTI Sr. Engineering Technical Analyst 616-738-3234 Thomas.Schmelter@cmsenergy.com	Consumers Energy Company L&D Training Center 17010 Croswell Street West Olive, Michigan 49460

## 2.0 SUMMARY OF RESULTS

#### 2.1 OPERATING DATA

The combined cycle combustion turbine fired natural gas during the test event. As noted in the test protocol, the achievable load for a combustion turbine varies with ambient conditions. Based upon weather conditions at the time of testing, the 100% load condition was run at the maximum achievable load condition and corresponded to approximately 170 gross megawatts (MWg). The reduced load testing was run at approximately 123 MWg, or 72% of the load achieved at the 100% load condition. Note that the preceding loads reflect electrical production for the combustion turbine only and do not account for the share of electrical production from the common steam turbine and electrical generator. When accounting for the additional electricity from the steam turbine and electrical generator, the 100% load condition test equated to approximately 258 MW, while the reduced load condition equated to approximately 196 MW.

Refer to Attachment D for detailed operating data, which was recorded in Eastern Standard Time (EST).

#### 2.2 APPLICABLE PERMIT INFORMATION

The Zeeland generating station is identified by State Registration Number (SRN) N6521 and operates in accordance with renewable operating permit (ROP) MI-ROP-N6521-2015a. The permit incorporates federal regulations and reports under Federal Registry Service (FRS) Id: 110012534551. EUGT1A and EUGT1B are included in the flexible group FGSIMPLECYCLE. EUGT2A and EUGT2B are included in the FG COMBINEDCYCLE flexible group.

#### 2.3 RESULTS

The Unit 2B PM less than 10 microns in diameter ( $PM_{10}$ ), VOCs and HCHO results are summarized in Table 2-1 below.

	of Test Resu		Run			Emissio	
arameter	Units	1 1	2 2	8	Average	Limit ROP	
nit 2B - 70	% Load						
	lb/hr	3.77	2.92	3.35	3.35	14.7	
PM <sub>10</sub>	ton/yr	16.5	12.8	14.7	14.7	64.4	
	lb/mmBtu	0.0023	0.0018	0.0021	0.0021	N/A <sup>*</sup>	
vee t	lb/hr	0.23	0.22	0.20	0.22	16.8	
VOCs <sup>†</sup>	ton/yr	1.0	1.0	0.9	1.0	73.6	
	lb/mmBtu	1.4E-04 1.3E-04 1.2E-04 1		1.3E-04	N/A*		
HCHO <sup>‡</sup>	ton/yr	1.0	1.0	0.9	1.0	2.35 <sup>‡</sup>	
	lb/mmBtu	1.4E-04 1.3E-04 1.2E-04 <b>1.3E-0</b> 4		N/A*			
nit 2B - 10(	0% Load					dun	
	lb/hr	3.32	4.34	7.08	4.91	14.7	
PM <sub>10</sub>	ton/yr	14.6	19.0	31.0	21.5	64.4	
	lb/mmBtu	0.0016	0.0022	0.0036	0.0025	N/A*	
voc t	lb/hr	0.22	0.18	0.20	0.20	16.8	
VOCs <sup>†</sup>	ton/yr	1.0	0.8	0.9	0.9	73.6	
	lb/mmBtu	1.1E-04	9.4E-05	1.0E-04	1.0E-04	N/A <sup>*</sup>	
HCHO <sup>‡</sup>	ton/yr	1.0	0.8	0.9	0.9	2.35 <sup>*</sup>	
	lb/mmBtu	1.1E-04	9.4E-05	1.0E-04	1.0E-04	N/A <sup>*</sup>	

#### Table 2-1 Summary of Test Results

\*: lb/mmBtu results are used in mass emission calculations with continuous heat input to evaluate compliance with the mass emission limits

<sup>†</sup>: VOCs mass emissions calculated as sum of mass emissions of VOCs detected

\* : HCHO limit is applicable to all turbine operations, the presented limit is the permit limit divided by four

Although not consistent with the prescribed compliance methodology in the ROP, the Unit 2B PM,  $PM_{10}$ , VOC and HCHO emission results indicate compliance with the mass emission limits in the permit.  $PM_{10}$  was determined as the sum of filterable and condensable PM. The preceding tons per year values are extrapolated assuming continuous operation at the pounds per hour emission rates observed during the testing. The facility uses lb/mmBtu emission factors in conjunction with continuous heat input determinations to calculate mass emission rates, consistent with Appendix 5 of the ROP.

Detailed test results are presented in Appendix Tables 1 and 2. Sample calculations, field data sheets, and laboratory data are presented in Appendices A, B, and C. Operating data and supporting documentation are provided in Appendices D and E.

#### 3.0 SOURCE DESCRIPTION

EUGT2B is a combined-cycle natural gas fired combustion turbine directly coupled to an electricity producing generator. Steam generated in the associated Heat Recovery Steam Generator (HRSG) is then fed to a common steam extraction turbine and electrical generator shared with EUGT2A.

#### 3.1 PROCESS

The Zeeland Generating Station operates four General Electric (GE) model 7FA natural gas fired combustion turbines. Units 1A and 1B are simple cycle units rated at 2,205 mmBtu/hr heat input, with an Upper Bound Range of Operation (UBRO) at 190 megawatts (MW) and a Lower Bound Range of Operation (LBRO) at 17 MW. Units 2A and 2B are combined-cycle units rated at 2,323 mmBtu/hr heat input, with an UBRO at approximately 303 MW and an LBRO at 17 MW.

#### 3.2 PROCESS FLOW

Air pollution control is achieved on all four combustion turbines through the use of Dry Low NOx Burners. The combined cycle units are also equipped with selective catalytic reduction (SCR) systems for controlling NOx.

#### 3.3 MATERIALS PROCESSED

Natural gas is combusted in the turbine producing heat that is used for electricity generation.

#### 3.4 RATED CAPACITY

Units 1A and 1B are rated at 2,205 mmBtu/hr heat input, with an UBRO at 190 MW and a LBRO at 17 MW. Units 2A and 2B are rated at 2,323 mmBtu/hr heat input, with an UBRO at 303 (Unit 2A) and 305 (Unit 2B) MW and an LBRO at 17 MW.

Testing was performed on one combined-cycle unit (Unit 2B, as 2A was tested during the most recent test event in 2013) at 100% and 70% load as required in MI-ROP-N6521-2015a.

#### 3.5 PROCESS INSTRUMENTATION

Operators, environmental technicians, and data acquisition systems continuously monitored the process during testing. One-minute data for the following parameters were collected during each FPM, CPM, VOCs, and HCHO test run:

- total heat input (mmBtu/hr)
- gross electricity output (MWg) [for the combustion turbine only]
- turbine and duct burner gas flow (hundred scfh)
- ammonia injection rate (lb/hr)
- oxygen (%)
- nitrogen oxides (ppmv at 15% O<sub>2</sub>, lb/mmBtu)
- carbon monoxide (ppmv, lb/mmBtu)

Due to the various instrumentation systems, the sampling times were correlated to Instrumentation times. Refer to Appendix D for operating data.

### 4.0 SAMPLING AND ANALYTICAL PROCEDURES

RCTS personnel tested for FPM, CPM, VOCs and HCHO using the USEPA test methods presented in Table 4-1. The sampling and analytical procedures associated with each parameter are described in the following sections.

Table 4-1 **Test Methods** 

Parameter	Method	USEPA Title			
Sampling location	1	Sample and Velocity Traverses for Stationary Sources			
Traverse points	2	Determination of Stack Gas Velocity and Volumetric Flow Rate (Type S Pitot Tube)			
Moisture	4	Determination of Moisture Content in Stack Gases			
Filterable Particulate Matter <sup>*</sup>	5	Determination of Particulate Matter Emissions from Stationary Sources			
Formaldehyde 18		Measurement of Gaseous Organic Compound Emissions by Gas Chromatography (FTIR)			
Emission Rate	19	Determination of Sulfur Dioxide Removal Efficiency and Particulate Matter, Sulfur Dioxide, and Nitrogen Oxide Emission Rates			
Condensable Particulate Matter <sup>*</sup>	202	Dry Impinger Method for Determining Condensable Particulate Emissions From Stationary Sources			
Molecular Weight $(CO_2 \text{ and } O_2^{\dagger})$	220	Vapor Phase Organic and Inorganic Emissions by Extractive FTIR			
Volatile Organic Compounds	320				

<sup>†</sup>: O<sub>2</sub> values will be determined from certified CEMS measurements <sup>\*</sup>: Methods 5 and 202 will be conducted in conjunction to measure PM<sub>10</sub>

#### 4.1 DESCRIPTION OF SAMPLING TRAIN AND FIELD PROCEDURES

The test matrix presented as Table 4-2 summarizes the sampling and analytical methods performed as specified in this test program.

#### Table 4-2 **Test Matrix**

Date (2018)	Run	Sample Type	Load (%)	Start Time (EDT)	Stop Time (EDT)	Test Duration (min)	Comment
	1	PM <sub>10</sub> and VOCs	70	9:05	11:19	120	Isokinetic sampling from 24 traverse points collected 3.137 dscm sample volume
Dec. 11	1	нсно	70	9:41	10:41	60	Single point, 1,199.7 milliliter sample volume
	2	PM <sub>10</sub> and VOCs	70	11:50	14:00	120	Isokinetic sampling from 24 traverse points collected 3.165 dscm sample volume

Regulatory Compliance Testing Section

GE&S/Environmental & Laboratory Services Department

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#### Table 4-2 Test Matrix

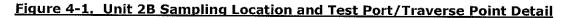
lest Matrix									
Date (2018)	Run	Sample Type	Load (%)	Start Time (EDT)	Stop Time (EDT)	Test Duration (min)	Comment		
	2	нсно	70	12:24	13:24	60	Single point, 1,199.7 milliliter sample volume		
Dec. 11	3	PM <sub>10</sub> and VOCs	70	14:20	16:30	120	Isokinetic sampling from 24 traverse points collected 3.234 dscm sample volume		
	3	нсно	70	15:10	16:10	60	Single point, 1,199.7 milliliter sample volume		
	1	PM <sub>10</sub> and VOCs	100	8:30	10:39	120	Isokinetic sampling from 24 traverse points collected 3.487 dscm sample volume		
	1	нсно	100	8:45	9:45	60	Single point, 1,199.7 milliliter sample volume		
Dec. 12	2	PM <sub>10</sub> and VOCs	100	11:00	13:09	120	Isokinetic sampling from 24 traverse points collected 3.305 dscm sample volume		
	2	нсно	100	13:46	14:46	60	Single point, 1,199.7 milliliter sample volume		
	3	PM <sub>10</sub> and VOCs	100	13:25	15:33	120	Isokinetic sampling from 24 traverse points collected 3.347 dscm sample volume		
	3	нсно	100	14:50	15:50	60	Single point, 1,199.7 milliliter sample volume		

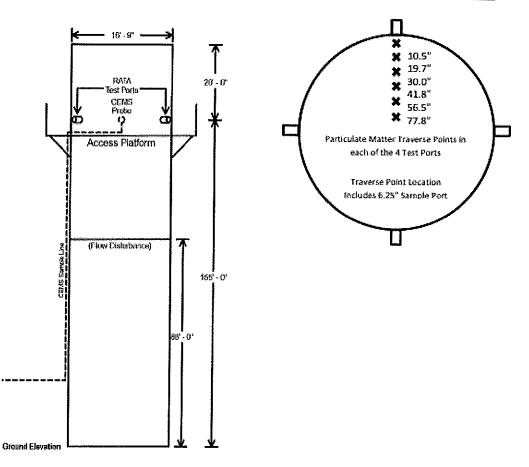
## 4.1.1 SAMPLE LOCATION AND TRAVERSE POINTS (USEPA METHOD 1)

The number and location of traverse points for measuring exhaust gas velocity and volumetric airflow was determined in accordance with USEPA Method 1, *Sample and Velocity Traverses for Stationary Sources.* Four test ports are located in the horizontal plane of the approximately 16.75 feet diameter stack. Refer to Figure 4-1 for a drawing showing the traverse points and upstream and downstream disturbances. The sampling ports are situated:

- Approximately 67 feet or 4 duct diameters downstream of a flow disturbance, and
- Approximately 20 feet or 1.2 duct diameters upstream of the stack exit.

The sample ports are 6-inches in diameter and extend 6.25 inches beyond the stack wall. The area of the exhaust duct was calculated and the cross-sectional area divided into a number of equal areas based on distances to air flow disturbances. Flue gas was sampled for five minutes at each of the six traverse points from the four sample ports for a total of 24 sample points and 120 minutes.

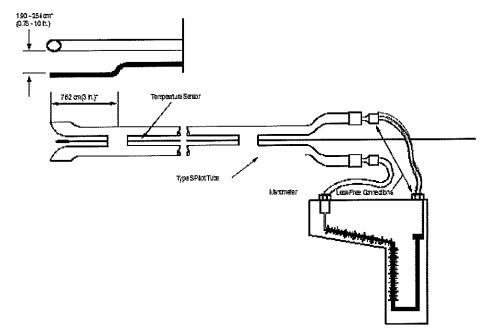




#### 4.1.2 VELOCITY AND TEMPERATURE (USEPA METHOD 2)

The exhaust gas velocity and temperature were measured using USEPA Method 2, *Determination of Stack Gas Temperature and Velocity (Type S Pitot Tube)*. The pressure differential ( $\Delta P$ ) across the positive impact and negative static openings of the Pitot tube inserted in the exhaust duct at each traverse point were measured using an "S Type" (Stauscheibe or reverse type) Pitot tube connected to an appropriately sized oil filled inclined manometer. Exhaust gas temperatures were measured using a nickel-chromium/nickel-alumel "Type K" thermocouple and a temperature indicator. Refer to Figure 4-2 for the Method 2 Pitot tube, thermocouple, and inclined oil-filled manometer configuration.

Figure 4-2. Method 2 Sample Apparatus



Method 1, § 11.4.2 states "if the average (null angle) is greater than 20°, the overall flow condition in the stack is unacceptable, and alternative methodology...must be used." The average null yaw angle measured at the Unit 1B exhaust on December 10, 2018 was 5.1°, thus meeting the less than 20° requirement. Since no ductwork and/or stack configuration changes are expected to occur in the future, the null angle information is considered reliable and additional cyclonic flow verification will not be performed. The cyclonic flow testing data is presented in Appendix B.

#### 4.1.3 MOLECULAR WEIGHT (CERTIFIED CEMS AND USEPA METHOD 320)

The exhaust gas composition and molecular weight was calculated using  $O_2$  measurements from the certified CEMS during the testing and  $CO_2$  measurements obtained from the FTIR following the sampling and analytical procedures of USEPA Method 320, *Vapor Phase Organic and Inorganic Emissions by Extractive FTIR*. The flue gas oxygen and carbon dioxide concentrations are required to calculate molecular weight, flue gas velocity, and emissions in lb/mmBtu, lb/hr, and ton/yr. Refer to Section 4.1.8 for sampling and analytical procedures of USEPA Method 320.

#### 4.1.4 MOISTURE CONTENT (USEPA METHOD 4)

The exhaust gas moisture content was measured using USEPA Method 4, *Determination of Moisture in Stack Gases* in conjunction with the Method 5 and 202 sample apparatus. Flue gas was drawn through a series of impingers immersed in an ice bath to condense and remove water from the sample. The amount of water condensed and collected in the impingers was measured gravimetrically and used to calculate the exhaust gas moisture content.

#### 4.1.5 FILTERABLE PARTICULATE MATTER (USEPA METHOD 5)

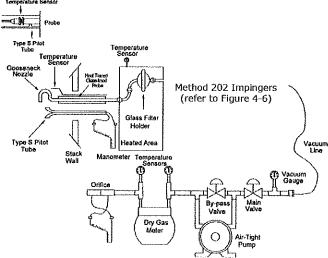
Filterable particulate matter samples were collected isokinetically in conjunction with RM 202 following USEPA Method 5, *Determination of Particulate Matter Emissions from Stationary Sources* procedures.

The flue gas is collected using a specifically sized nozzle, probe, quartz-fiber filter, and a series of impingers configured as shown in Method 5/202 Table 4-3. The FPM is collected on the filter and water vapor and/or CPM is collected in the impingers. Figure 4-3 depicts the USEPA Method 5 sample apparatus.

Before testing, a preliminary velocity traverse was performed and/or representative flow data from previous measurements was reviewed to calculate an ideal nozzle size that allowed isokinetic sampling to be performed. A pre-cleaned nozzle that had an inner diameter approximating the calculated value was measured with calipers across three cross-sectional chords, rinsed and brushed with acetone and connected to the sample probe.

The impact and static pressure openings of the Pitot tube were leak-checked at or above a velocity head of 3.0 inches of water for a minimum of 15 seconds. The PM sample train was leak-checked by capping the nozzle opening and applying a vacuum of approximately 15 inches of mercury. The dry-gas meter was monitored for approximately 1 minute to verify a sample apparatus leak rate of less than 0.02 cubic feet per minute (cfm). The sample probe was inserted into the sampling port to begin sampling.

Ice was placed around the impingers and the probe, and filter temperatures were allowed to stabilize to a temperature of  $248\pm25^{\circ}$ F before sampling, as applicable. After the desired operating conditions were coordinated with the facility, testing was initiated. Stack and sample apparatus parameters (e.g., flue velocity, temperature) were monitored to ensure isokinetic sample rates were within  $100\pm10\%$  for the duration of the test.



#### Figure 4-3. USEPA Method 5 Sampling Train

At the conclusion of a test run and the post-test leak check, the sample train was disassembled and the impingers and FPM filter housing were transported to the recovery area.

The filter was recovered from the filter housing, placed in a Petri dish, sealed with Teflon tape, and labeled as "FPM Container 1." The nozzle, probe liner, and the front half of the filter housing was triple rinsed with acetone and collected in pre-cleaned sample containers, sealed with Teflon tape, and labeled as "FPM Container 2." The flue gas moisture condensed in the impingers was weighed on an electronic scale to determine flue gas moisture content, after which the impingers were recovered following Method 202 CPM requirements (see Section 4.1.6). Refer to Figure 4-4 for the USEPA Method 5 sample recovery scheme.

The sample containers, including blanks, were transported to the RCTS laboratory for analysis. The sample analysis followed USEPA Method 5 procedures as summarized in the sample recovery scheme presented in Figure 4-5.

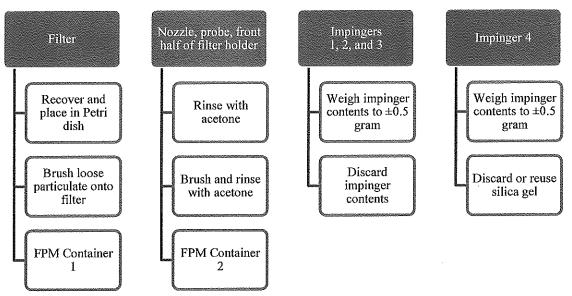
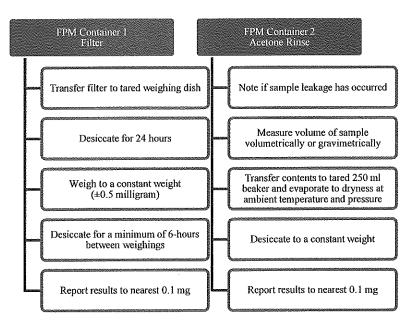


Figure 4-4. USEPA Method 5 Sample Recovery Scheme

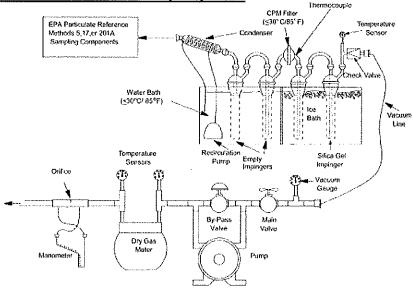
Figure 4-5. USEPA Method 5 Analytical Scheme



#### 4.1.6 CONDENSABLE PARTICULATE MATTER (USEPA METHOD 202)

Condensable particulate matter was collected isokinetically in conjunction with USEPA Method 5 using 40 CFR Part 51, EPA Method 202, *Dry Impinger Method for Determining Condensable Particulate Emissions from Stationary Sources.* The Method 202 sample apparatus uses clean, baked glassware comprised of a glass coil type condenser, a dropout impinger, a modified Greenburg-Smith (GS) impinger with an open tube tip, a CPM filter holder containing a Teflon filter, one impinger containing approximately 100 milliliters of

Regulatory Compliance Testing Section GE&S/Environmental & Laboratory Services Department Page 10 of 16 QSTI: D.A. King water and one impinger containing silica gel. During each CPM run, temperature controlled water recirculated in the coil condenser jacket maintained the CPM filter temperature below 85°F. Refer to Figure 4-6 for a drawing of the Method 202 sample apparatus and Table 4-3 which describes the Method 5/202 impinger configuration.



#### Figure 4-6. USEPA Method 202 Sampling Train

Impinger Order (Upstream to Downstream)	Impinger Type	Impinger Contents	Amount (gram)
1	Dropout	Empty	0
2	Modified	Empty	0
	CPI	M Filter	
3	Modified	Water	100
4	Modified	Silica gel desiccant	~200-300

Upon test completion, each impinger was weighed to determine flue gas moisture content. The condenser, dropout and back-up impingers, and the CPM filter housing were then reassembled and purged with Ultra-high purity nitrogen at a rate of approximately 14 liters per minute for a minimum of one hour to remove dissolved sulfur dioxide ( $SO_2$ ) gases from the impinger water. During the purge, water continued to recirculate in the condenser jacket to maintain the CPM filter exit temperature and the impingers were observed to ensure the contents did not evaporate.

After the nitrogen purge, the condensate collected in the dropout and back-up impingers were transferred to a clean sample bottle labeled as CPM Container #1, Aqueous Liquid Impinger. The back half of the Method 5 filter bell, condenser, impingers and connecting glassware were then rinsed twice with deionized, ultra-filtered water into the same container. The water rinses were followed by an acetone rinse and duplicate hexane rinses

into a separate sample bottle identified as CPM Container #2 (organic rinses). The CPM filter was removed prior to the water and organic rinses and placed in a clean Petri dish identified as CPM Container #3. Liquid levels on the sample bottles were marked and the samples were sealed and transported to Maxxam Analytics laboratory in Mississauga, Ontario for analysis.

#### 4.1.7 FORMALDEHYDE (USEPA METHOD 18)

Formaldehyde concentrations were determined using USEPA Method 18, Measurement of Gaseous Organic Compound Emissions by Gas Chromatography via adsorbent tube sampling and analysis. The target organic compound (formaldehyde) was separated by gas chromatography and quantified by the FTIR onsite. Sampling, analytical and calibration procedures followed USEPA Method 18 specifications for adsorbent tube sampling.

A recovery study was performed utilizing two identical trains. One of the sampling trains was designated the spiked train and the other the unspiked train. Formaldehyde was spiked (at 40% to 60% of the expected catch) onto the adsorbent tube in the spiked train prior to sampling. The two trains were sampled simultaneously and the fraction of the spiked compound recovered (R) was calculated in accordance with USEPA Method 18. A complete recovery study will consist of three runs. For the adsorbent tube sampling and analytical procedure to be acceptable, R (in this case the average of three runs) must be  $\geq$ 0.70 and  $\leq$ 1.30. The calculated R value was 1.067 for the 100% load condition and 0.980 for the 70% load condition. Refer to the laboratory report in Appendix C for detailed data and calibrations.

#### 4.1.8 VOCs AND CARBON DIOXIDE (USEPA METHOD 320)

VOCs and CO2 were measured using the sampling and analytical procedures of USEPA Method 320, Vapor Phase Organic and Inorganic Emissions by Extractive FTIR. Exhaust gas was extracted through a heated stainless steel probe and heated Teflon® sample line prior to being introduced to the FTIR. The stainless steel probe and Teflon® sample line were maintained at approximately 375°F.

Prior to testing a calibration transfer standard (CTS) was used to ensure suitable agreement between the sample and reference spectra. Following the CTS, a spike gas and tracer gas was introduced to the sample line at a constant flowrate of  $\leq 10\%$  of the total sample flow. The system passed the QA spike when the average spike concentration was within 0.7 to 1.3 times the expected concentration.

Data was validated and corrected per specifications outlined in USEPA Method 301. A total of 120 minutes of reference spectra data was collected for each run. Following each run, another CTS spectrum was recorded and compared to the pre-test CTS. The pre-test and post-test CTS are required to be within  $\pm 5\%$  of the mean value for the run to be valid.

An on-site minimum detectable concentration (MDC) analysis was performed for the target analytes using procedures outlined in ASTM D 6348 A2.3. The MDC was calculated as three times the standard deviation of the concentrations from ten representative background spectra taken during the MDC analysis.

The VOCs tested for with the FTIR were acetylene, propane, propylene, butane, acetaldehyde, ethylene and methanol. Total VOC mass and lb/mmBtu emission rates were calculated as the sum of the mass and lb/mmBtu emission rates of any VOCs present above the detection limit plus the mass and lb/mmBtu emission rate of formaldehyde (from M18). No VOCs were detected above the minimum detection limit (0.5 ppmv) and each such VOC was assigned a value of zero consistent with guidance from the MDEQ-AQD. It should be

noted that there was a minor sampling system contaminant/interferent that required bias corrections to be applied to butane concentration data.

#### 4.1.9 EMISSION RATES (USEPA METHOD 19)

USEPA Method 19, *Determination of Sulfur Dioxide Removal Efficiency and Particulate Matter, Sulfur Dioxide, and Nitrogen Oxide Emission Rates*, was used to calculate PM<sub>10</sub>, VOC and formaldehyde emission rates in units of lb/mmBtu. Measured oxygen concentrations from the certified CEMS and F factors (ratios of combustion gas volumes to heat inputs) were used to calculate emission rates using equation 19-1 from the method; refer to Appendix A for sample calculations.

## 5.0 TEST RESULTS AND DISCUSSION

The test results obtained as required by MDEQ ROP MI-ROP-N6521-2015a on December 11 and 12, 2018 indicate the average of the three runs performed on Unit 2B for  $PM_{10}$ , VOCs and HCHO measured less than the emission limits in Table 1-1 at both load conditions (again, stack testing is not the compliance method; the lb/mmBtu emission factors will be used in conjunction with heat input determinations to calculate mass emissions based upon the proper averaging periods). Therefore, Unit 2B is in compliance with the mass emission limits in the ROP. Refer to Section 2.3 for a summary of the test results.

#### **5.1 TABULATION OF RESULTS**

Table 2-1 in Section 2 of this report summarizes the results and Appendix Tables 1 and 2 contain detailed tabulation of results, process operating conditions, and exhaust gas conditions.

#### **5.2 SIGNIFICANCE OF RESULTS**

The Unit 2B  $PM_{10}$ , VOCs and HCHO results indicate ongoing compliance with the mass emission limits present in MDEQ ROP MI-ROP-N6521-2015a.

#### 5.3 VARIATIONS FROM SAMPLING OR OPERATING CONDITIONS

There were no significant sampling or variations encountered during the test program. It should be noted that the  $2^{nd}$  and  $3^{rd}$  Method 18 test runs for HCHO at 100% load did not occur concurrently with the PM/VOCs test runs. Additional process data sheets are included in Appendix D to accompany these runs.

#### 5.4 PROCESS OR CONTROL EQUIPMENT UPSET CONDITIONS

The turbine and associated control equipment were operating under routine conditions and no upsets were encountered during testing.

#### 5.5 AIR POLLUTION CONTROL DEVICE MAINTENANCE

No significant pollution control device maintenance occurred during the three months prior to the test. Optimization of the air pollution control equipment is a continuous process to ensure compliance with regulatory emission limits.

#### 5.6 RE-TEST DISCUSSION

Based on the results of this test program, a re-test is not required.

#### 5.7 RESULTS OF AUDIT SAMPLES

Audit samples are not required for the reference methods utilized during this test program and are not available from USEPA Stationary Source Audit Sample Program providers. A list of QA/QC Procedures is listed below in Table 5-1.

Table 5-1 QA/QC Procedures

QA/QC Procedu QA/QC	Purpose	Procedure	Frequency	Acceptance
Activity		Measure distance	or carpennes/	Criteria
M1: Sampling Location	Evaluates if the sampling location is suitable for sampling	from ports to downstream and upstream flow disturbances	Pre-test	≥2 diameters downstream; ≥0.5 diameter upstream.
M1: Duct diameter/ dimensions	Verifies area of stack is accurately measured	Review as-built drawings and field measurement	Pre-test	Field measurement agreement with as- built drawings
M1: Cyclonic flow evaluation	Evaluate the sampling location for cyclonic flow	Measure null angles	Pre-test	≤20°
M2: Pitot tube calibration and standardization	Verifies construction and alignment of Pitot tube	Inspect Pitot tube, assign coefficient value	Pre-test and after each field use	Method 2 alignment and dimension requirements
M2: Pitot tube leak check	Verify leak free sampling systems	Apply minimum pressure of 3.0 inches of H <sub>2</sub> O to Pitot tube	Pre-test and Post-test	$\pm 0.01$ in H <sub>2</sub> O for 15 seconds at minimum 3.0 in H <sub>2</sub> O velocity head
M4: Field balance calibration	Verify moisture measurement accuracy	Use Class 6 weight to check balance accuracy	Daily before use	The field balance must measure the weight within ±0.5 gram of the certified mass
M4: Impinger temperature	Ensures collection of condensed water	Maintain last Impinger temperature ≤68°F	Throughout test	Last impinger temperature must be ≤68°F
M5: nozzle diameter measurements	Verify nozzle diameter used to calculate sample rate	Measure inner diameter across three cross- sectional chords	Pre-test	3 measurements agree within ±0.004 inch
M5: Apparatus Temperature	Prevents condensation within sample apparatus	Set probe & filter heat controllers to 248±25°F	Verify prior to and during each run	Apparatus temperature must be 248±25°F
M5: sample rate	Ensure representative sample collection	Calculate isokinetic sample rate	During and post-test	100±10% isokinetic rate
M5: Sample volume	Ensure minimum required sample volumes collected	Record pre- and post-test dry gas meter volume reading	Post test	PM: ≥100 dscf

#### Table 5-1 QA/QC Procedures

QA/QC Procedu	res			
QA/QC Activity	Purpose	Procedure	Frequency	Acceptance Criteria
M5/202: Post-test leak check	Evaluate if system leaks biased the sample	Cap sample train; monitor DGM	Post-test	≤0.020 cfm
M5/202: post- test meter audit	Evaluates sample volume accuracy	DGM pre- and post- test; compare calibration factors (Y and Yqa)	Pre-test Post-test	±5%
M5: Apparatus Temperature	Ensures purge of acid gases in glass probe liner and Teflon filter	Set probe & filter heat controllers to ≥248°F	Verify prior to and during each run	Apparatus temperature must be ≥223°F and ≤273°F
M202: impinger temperature	Ensure collection of condensate	Maintain CPM filter temperature below 85°F	Throughout test	CPM filter temperature must be ≥65°F and ≤85°F
M18: Analyzer calibration	Develop calibration curve, evaluates operation of analyzers	Calibration gases introduces directly into analyzers	Pre-test Post-test	pre- and post- test average response factors ±5% of mean value
M18: Recovery study	Verify the acceptability of the sampling technique for the target compound(s)	Average recovery from three spiked adsorption tubes; correct all field measurements based on the average recovery	Field sample runs not validated without successful field recovery test	Average recovery between 0.7 and 1.3
M320: Sampling system leak check	Verify leak free sampling system	Cap sampling system, monitor flowrate	Pre-test	≤200 mL/min
M320: Analytical system leak check	Verify leak free analytical system	Cap analytical system, monitor pressure	Pre-test	≤4.0% of the FTIR system volume
M320: QA Spike	Evaluates operation of analyzer	Calibration gases introduced into sampling system at ≤10.0% of sampling rate	Pre-test Post-test	average spiked concentration 0.7 to 1.3 times the expected concentration

#### **5.8 CALIBRATION SHEETS**

Calibration sheets, including dry gas meter, gas protocol sheets, and analyzer quality control and assurance checks are presented in Appendix E.

#### **5.9 SAMPLE CALCULATIONS**

Sample calculations and formulas used to compute emissions data are presented in Appendix A.

#### 5.10 FIELD DATA SHEETS

Field data sheets are presented in Appendix B.

#### 5.11 LABORATORY QUALITY ASSURANCE / QUALITY CONTROL PROCEDURES

The method specific quality assurance and quality control procedures in each method employed during this test program were followed, without deviation. Refer to Appendix C for the laboratory data sheets.

#### 5.11.1 QA/QC BLANKS

Reagent and media blanks were analyzed for the parameters of interest. The results of the blanks analysis are presented in the Table 5-2. Laboratory QA/QC and blank results data are contained in Appendix C.

#### Table 5-2 OA/OC Blanks

Sample Identification	Result	Comment		
Method 5 Acetone Blank	1.4 mg	Sample volume was 200 milliliters Acetone blank corrections were applied		
Method 5 Filter Blank	0.0 mg	Reporting limit is 0.1 milligrams		
Method 202 DI H <sub>2</sub> O Blank	<0.5 mg	Sample weight was 200 grams Result is for inorganic condensable		
Method 202 Acetone Blank	<1.0 mg	Sample weight was 160 grams Result is for organic condensable		
Method 202 Hexane Blank	<1.0 mg	Sample weight was 150 grams Result is for organic condensable		
Method 202 Field Train Recovery Blank	1.9 mg inorganic 1.1 mg organic	Maximum blank correction of 2.0 mg applied to results		

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Facility and Source Information	Units	Run 1	Run 2	Run 3	Average
Customer:	01113			erating Stalion	ritorago
Source:				70% Load	
Nork Order:				0411	
Date:		12/11/2018	12/11/2018	12/11/2018	
_0ad:	MWg	122.8	122.6	122,8	122.7
Stack Diameter	inches	201.0	201.0	201.0	
Cross-sectional Area of Stack, A	ft <sup>2</sup>	220,35	220.35	220.35	
Source Pollutant Test Data	Units	Run 1	Run 2	Run 3	Average
Barometric Pressure, P <sub>bar</sub>	inches of Hg	29.25	29.25	29.40	29,30
Dry Gas Meter Calibration Factor, Y	dimensionless	0.999	0.999	0,999	0,999
Pitot Tube Coefficient, Cp	dimensionless	0.84	0.84	0.84	0,84
Stack Static Pressure, Pg	inches of H <sub>2</sub> O	-1.00	-0.70	-1.00	-0.90
Nozzie Diameter, D <sub>n</sub>	inches	0.240	0.240	0.240	0.240
Run Start Time	hr:mm	9:05	11:50	14:20	
Run Stop Time	hr:mm	11:19	14:00	16:30	
Duration of Sample, θ	minutes	120	120	120	120
Dry Gas Meter Leak Rate, Lp	cfm	0,000	0.000	0.000	0.000
Dry Gas Meter Start Volume	ft <sup>3</sup>	408.04	521.62	642,25	523.97
Try Gas Meter Final Volume	ft <sup>3</sup>	521.00	636.88	760,01	639.30
werage Pressure Difference across the Orifice Meter, AH	inches of H <sub>2</sub> O	2.87	3.09	3.06	3.01
Verage Dry Gas Meter Temperature, Tm	۴	69.5	75.8	78.4	74.6
verage Square Root Velocity Head, νΔp	vinches H <sub>2</sub> O	1.0761	1.1115	1.1037	1.0971
Stack Gas Temperature, T <sub>s(abavg)</sub>	19-	217.5	217.7	219.5	218.2
Source Moisture Data		Run 1	Run 2	Run 3	Average
olume of Water Vapor Condensed in Silica Gel, V <sub>wsq(std)</sub>	scf	1.2	1.6	1.7	1.5
otal Volume of Water Vapor Condensed, Vwsd	scf	8.659	9.187	8,968	8.938
olume of Gas Sample as Measured by the Dry Gas Meter, Vm	dcf	112.959	115.256	117.760	115.325
olume of Gas Sample Measured by the Dry Gas Meter corrected to STP, Viristo	dscf	110.759	111.743	114.188	112.230
olume of Gas Sample Measured by the Dry Gas Meter corrected to STP, Vm(std)	dscm	3.137	3.165	3.234	3.178
Noisture Content of Stack Gas, Bus	% H <sub>2</sub> O	7.25	7.60	7.28	7.38
Gas Analysis Data		Run 1	Run 2	Run 3	Average
Carbon Dioxide, %CO2	%, dry	4.2	4.2	4.2	4.2
Dxygen, %O <sub>2</sub>	%, dry	13.4	13.4	13,5	13.4
litrogen, %N	%, dry	82.4	82,4	82.3	82.4
Dry Molecular Weight, Md	lb/lb-mole	29.21	29.21	29,21	29.21
Vet Molecular Weight, Ms	lib/lb-male	28,40	28.36	28,40	28.38
uel F-Factor, F <sub>d</sub> ;	dscf/mmBtu	8,710	8,710	8,710	8,710
Gas Volumetric Flow Rate Data		Run 1	Run 2	Run 3	Average
werage Stack Gas Velocity, vs	fl/s	69,9	72,2	71.6	71.2
Stack Gas Volumetric Flow Rate, Q	acím	923,878	954,716	946,575	941,723
Rack Gas Venander of Holl Hate, Q	scfm	702,118	725,879	720,937	716.312
Mack Gas Dry Standard Volumetric Flow Rate, Qsd	dscfm	651,207	670,734	668,440	663,460
ercent of Isokinetic Sampling, I	%	99.5	97,4	99.9	98.9
Gas Concentrations and Emission Rates	110	Run 1	Run 2	Run 3	Average
Ass of Filterable PM Collected, mp	mg	0.76	1.68	1.04	1.16
illerable PM Concentration, c.	gr/dscf	0.00011	0,00023	0.00014	0.00016
		0.59	1.33	0.80	0.91
iliterable PM Mass Emission Rate, E	lb/nr lb/mmBtu	0.0004	1,33	0.80	0.0006
iliterable PM, Ib/mmBlu, E					
ilterable PM, tpy [Assumes 8,760 Hrs/Yr Operation]	tpy	2,6	5.8	3.5	4.0
Aass of Organic CPM, ma		1.0	1.4	1.9	1.4
Ass of Inorganic Condensable PM, mi	mg	5.1	2.6	3.4	3.7
idaa or morganio oomaanaaola nin, mj	mg		2.0	0.4	5.1
lass of Total CPM in Field Train Recovery Blank Correction, mp		2.0	2,0	2.0	2.0
	mg	4.1	2,0	3.3	3.1
Aass of Total Condensable PM, meen	តាព្វ	-			
condensable PM Concentration	gr/dscf	0.00057	0.00028	0.00045	0.00043
condensable PM Mass Emission Rate	lb/hr	3.18	1,58	2.55	2.44
condensable PM Mass Emission Rate	lb/mmBtu	0.0020	0,0010	0.0016	0.0015
ondensable PM Mass Emission Rate [Assumes 8,760 Hrs/Yr Operation]	tpy	13.9	6,9	11.2	10.7
	· · ·				
fass of Filterable and Condensable PM (PM <sub>10</sub> )	mg	4.9	3.7	4.3	4.3
M <sub>10</sub> Concentration	gr/dscf	0.00068	0.00051	0.00058	0.00059
PM <sub>10</sub> Mass Emission Rate	lb/hr	3.77	2.92	3.35	3.35
					0 0004
2M <sub>10</sub> Mass Emission Rate 2M <sub>10</sub> Mass Emission Rate (Assumes 8,760 Hrs/Yr Op.)	lb/mm8tu	0.0023	0.0018 12.8	0,0021	0.0021

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## Table 2 - Unit 2B 70% Load VOC Emission Test Results

Table 2 - Unit 2B 70% Lo Facility and Source Information	Units	Run 1	Run 2	Run 3	Average
Customer:	Units			erating Station	Average
Source:				-	
Work Order:		Unit 2B - 70% Load 6500411			
Dale;		12/11/2018	12/11/2018	12/11/2018	
Load:	MWg	122.8	122.6	122.8	122,7
Stack Diameter	inches	201.0	201.0	201.0	
Cross-sectional Area of Stack, A	ft <sup>2</sup>	220.35	220.35	220.35	
Source Pollutant Test Data	Units	Run 1	Run 2	Run 3	Average
Barometric Pressure, P <sub>bar</sub>	inches of Hg	29.25	29.25	29.40	29.30
Dry Gas Meter Calibration Factor, Y	dimensionless	0,999	0.999	0.999	0.999
Pitot Tube Coefficient, Cp	dimensionless	0.84	0.84	0.84	0.84
Stack Static Pressure, Pg	inches of H <sub>2</sub> O	-1.00	-0.70	-1.00	-0.90
Nozzle Diameter, D <sub>n</sub>	inches	0.240	0.240	0.240	0.240
Run Start Time	hrmm	9:05	11:50	14:20	
Run Stop Time	hrm	11:19	14:00	16:30	
Duration of Sample, 0	minutes	120	120	120	120
Dry Gas Meter Leak Rate, Lp	cfm	0.000	0,000	0,000	0.000
Dry Gas Meter Start Volume	ft <sup>3</sup>	408.04	521.62	642.25	523.97
Dry Gas Meter Final Volume	ft <sup>3</sup>	521.00	636.88	760.01	639.30
Average Pressure Difference across the Orifice Meter, ΔH	inches of H <sub>2</sub> O	2.87	3.09	3.06	3.01
Average Dry Gas Meter Temperature, Tm	*F	69.5	75,8	78.4	74.6
Average Square Root Velocity Head, vop	Vinches H <sub>2</sub> O	1.0761	1,1115	1,1037	1.0971
Stack Gas Temperature, Tstabavo)		217.5	217.7	219.5	218.2
Source Moisture Data	1	Run 1	Run 2	Run 3	Average
Volume of Water Vapor Condensed in Silica Gel, V <sub>wsg(std)</sub>	lscf	1.2	1.6	1.7	1.5
Total Volume of Water Vapor Condensed, V <sub>w(std)</sub>	scf	8.659	9.187	8.968	8.938
Volume of Gas Sample as Measured by the Dry Gas Meter, Vm	dcf	112.959	115.256	117.760	115.325
volume of Gas Sample Measured by the Dry Gas Meter corrected to STP, $V_{m(std)}$	dscf	110.759	111.743	114,188	112.230
Volume of Gas Sample Measured by the Dry Gas Meter corrected to STP, $V_{m(star)}$	dscm	3.137	3.165	3,234	3,178
Moisture Content of Stack Gas, B <sub>ve</sub>	% H <sub>2</sub> O	7.25	7.60	7.28	7.38
Gas Analysis Data	1 -	Run 1	Run 2	Run 3	Average
Carbon Dioxide, %CO <sub>2</sub>	%, dry	4.2	4.2	4.2	4.2
Dxygen, %O <sub>2</sub>	%, dry	13.4	13.4	13.5	13.4
Nitrogen, %N Dry Molecular Weight, M <sub>d</sub>	%, dry lib/lb-mole	82.4	82,4 29.21	82,3 29.21	82.4
Wet Molecular Weight, M <sub>e</sub>	lb/lb-mole	28.40	28.36	28.40	28.38
Fuel F-Factor, Frd:	dscf/mmBtu	8,710	8,710	8,710	8,710
	daoninintia			,	
Gas Volumetric Flow Rate Data	lavo	Run 1	Run 2 72.2	Run 3 71.6	Average 71.2
	ft/s	69.9			
Stack Gas Volumetric Flow Rate, Q Stack Gas Standard Volumetric Flow Rate, Qs	acfm	923,878	954,716	946,575	941,723
· •	scfm	702,118	725,879	720,937	716,312
Stack Gas Dry Standard Volumetric Flow Rate, Qed	dscfm	651,207	670,734	668,440	663,460
Percent of Isokinetic Sampling, I	%	99.5	97.4	99.9	98,9
Gas Concentrations and Emission Rates	T	Run 1	Run 2	Run 3	Average
Formaldehyde Concentration	ppmvd	0.076	0.071	0.065	0.071
Formaldehyde Molecular Weight	g/mole	30.031	30.031	30.031	30.031
Formaldehyde lb/scf Coversion Factor	lb/scf	7,799E-08	7.799E-08	7.799E-08	7.799E-0
Formaldehyde Mass Emission Rate	lb/hr	0.23	0.22	0.20	0.22
Formaldehyde Mass Emission Rate	lb/mmBtu	0.0001	0.0001	0.0001	0.0001
Formaldehyde Mass Emission Rate [Assumes 8,760 Hrs/Yr Operation]	tpy	1.0	1.0	0.9	1.0
Acetylene Concentration	ppmvd	ND	ND	ND	0
Propane Concentration	ppmvd	ND	ND	ND	0
Butane Concentration	ppmvd	ND	ND	ND	0
Propylene Concentration	ppmvd	ND	ND	ND	0
Acetaldehyde Concentration	ppmvd	ND	ND	ND	0
Ethylene Concentration	ppmvd	ND	ND	ND	0
Aethanol Concentration	ppmvd	ND	ND	ND	0
Total VOC Mass Emission Rate	lb/hr	0.23	0.22	0.20	0.22
Total VOC Mass Emission Rate	lb/mmBtu	0.0001	0.0001	0.0001	0.0001

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Table 3 - Unit 2B 100%	Load PM Er	nission Te	est Resu	lts	
Facility and Source Information	Units	Run 1	Run 2	Run 3	Average
Customer:		Zeeland Generating Station			
Source:			Unit 2B -	100% Load	
Work Order:			650	0411	
Date:		12/12/2018	12/12/2018	12/12/2018	
Load:	MWg	171.2	169.1	168.0	169.4
Stack Diameter	inches	201.0	201.0	201.0	
Cross-sectional Area of Stack, A	ft²	220.35	220.35	220.35	
Source Pollutant Test Data	Units	Run 1	Run 2	Run 3	Average
Barometric Pressure, P <sub>bar</sub>	inches of Hg	29.10	29.10	29,05	29.08
Dry Gas Meter Calibration Factor, Y	dimensionless	0.999	0,999	0.999	0,999
Pitot Tube Coefficient, Cp	dimensionless	0.84	0.84	0.84	0.84
Stack Static Pressure, Pg	inches of H <sub>2</sub> O	-1.00	-1.00	-1.00	-1.00
Nozzle Diameter, D <sub>n</sub>	inches	0.219	0.219	0.219	0.219
Run Start Time	hr:mm	8:30	11:00	13:25	
Run Stop Time	hr:mm	10:39	13:09	15:33	
Duration of Sample, 6	minutes	120	120	120	120
Dry Gas Meter Leak Rate, Lp	cfm	0.000	0.000	0.000	0.000
Dry Gas Meter Start Volume	ff <sup>3</sup>	761.26	889.10	12.13	554.16
Dry Gas Meter Final Volume	ft <sup>3</sup>	888.16	1011.25	135.94	678.45
Average Pressure Difference across the Orifice Meter, AH	inches of H <sub>2</sub> O *F	3.48	3.30	3.36	3.38
Average Dry Gas Meter Temperature, Tm		73.2	81.3	80.8	78.4
Average Square Root Velocity Head, v∆p	vinches H <sub>2</sub> O	1.4353	1.3837 227.9	1.3957	1.4049 228.3
Stack Gas Temperature, T <sub>s(ebavg)</sub>	1			<u>.</u>	l
Source Moisture Data	1	Run 1	Run 2	Run 3	Average
Volume of Water Vapor Condensed, Vuo(sto)	scf	8.2	7.8	7.5	7.8
Volume of Water Vapor Condensed in Silica Gel, V <sub>wsg(std)</sub>	scf	1.4	1.4	1.7	1.5
Tolal Volume of Water Vapor Condensed, V <sub>v(sto)</sub>	scf	9.630	9.175	9.185	9.330
Volume of Gas Sample as Measured by the Dry Gas Meter, Vm	dcf	126.905	122.150	123.810 118.189	124,288
Volume of Gas Sample Measured by the Dry Gas Meter corrected to STP, V <sub>m(std)</sub>	dscf	123,128	116.688		119.335
Volume of Gas Sample Measured by the Dry Gas Meter corrected to STP, V <sub>rn(sti)</sub> Moisture Content of Stack Gas, B <sub>vis</sub>	dscm % H <sub>2</sub> O	3.487	3,305 7,29	3.347	3,380
	701120				I
Gas Analysis Data	lor des	Run 1	Run 2	Run 3	Average
Carbon Dioxide, %CO <sub>2</sub>	%, dry	4.0	4.1	4.1	4.1
Oxygen, %O <sub>2</sub>	%, dry	13.5	13.8		
Nitrogen, %N	%, dry	82.5	82.1 29.21	82.1 29.21	82,2 29,20
Dry Motecular Weight, M <sub>d</sub> Wet Motecular Weight, M <sub>e</sub>	Ib/lb-mole	29.18	29.21	29.21	29.20
Fuel F-Factor, F <sub>d</sub> :	lb/lb-mole dscf/mmBtu	8,710	8,710	8,710	8,710
	Cochettining		Run 2	Run 3	
Gas Volumetric Flow Rate Data	10/n	Run 1 94,3	90.8	91.6	Average 92.2
Average Stack Gas Velocity, vs	fl/s				· · · · · ·
Stack Gas Volumetric Flow Rate, Q	acim	1,246,600	1,200,302	1,211,458 900,623	1,219,453 907,016
Stack Gas Standard Volumetric Flow Rate, Qs	scfm	926,663	893,761		
Stack Gas Dry Standard Volumetric Flow Rate, Q <sub>st</sub>	dscfm	859,442	828,606	835,680	841,243
Percent of Isokinetic Sampling, I	%	100.6	98.9	99.3	99.6
Gas Concentrations and Emission Rates	1.	Run 1	Run 2	Run 3	Average 3.01
Mass of Fillerable PM Collected, mn	mg	1.91	2.33	4.79	
Filterable PM Concentration, cs	gr/dscf	0.00024	0.00031	0.00062	0.00039
Filterable PM Mass Emission Rate, E	lb/hr	1.76	2.18	4.47	2.80
Filterable PM, Ib/mmBlu, E	lb/mmBtu	0,0008	0.0011	0.0023	0.0014
Fillerable PM, tpy [Assumes 8,760 Hrs/Yr Operation]	tpy	7.7	9.6	19.6	12.3
Mass of Oraquio CBM m		~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	14	2.2	16
Mass of Organic CPM, m <sub>o</sub>	mg	<1.0	1.6 2.7	2.2	1.6 2.7
Mass of Inorganic Condensable PM, m	mg	2.1	2.1	2.0	4.1
Mana of Total COM in Field Train Paceuras Disale Correction, m			2.0	2.0	2,0
Mass of Total CPM in Field Train Recovery Blank Correction, m <sub>8</sub>	mg	2.0	2.0	2.0	2.0
Mass of Total Condensable PM, m <sub>com</sub>	mg				0.00029
Condensable PM Concentration	gr/dscf	0.00021	0.00030	0.00036	
Condensable PM Mass Emission Rate	lb/hr	1.57	2.16	2.61	2.11
Condensable PM Mass Emission Rate	lb/mmBlu	0.0007	0.0011	0.0013	0,0011
Condensable PM Mass Emission Rate [Assumes 8,760 Hrs/Yr Operation]	tpy	6,9	9.4	11.4	9.2
	l	3,6	10	78	5,3
Mana of Fillerable and Goodenable DH (DM )		1 3.5	4.6	7.6	0.0
Mass of Filterable and Condensable PM (PM <sub>10</sub> )	mg		0.00004	0.00000	0.00000
PM <sub>10</sub> Concentration	gr/dscf	0.00045	0.00061	0.00099	0.00068
PM <sub>10</sub> Concentration PM <sub>10</sub> Mass Emission Rate	gr/dscf Ib/hr	0.00045 3,32	4.34	7.08	4.91
Mass of Filterable and Condensable PM (PM <sub>10</sub> ) PM <sub>10</sub> Concentration PM <sub>10</sub> Mass Emission Rate PM <sub>10</sub> Mass Emission Rate PM <sub>10</sub> Mass Emission Rate (Assumes 8,760 Hrs/Yr Op.)	gr/dscf	0.00045			



#### Table 4 - Unit 2B 100% Load VOC Emission Test Results Facility and Source Information Units Run 1 Run 2 Run 3 Average Zeeland Generating Station Customer; Unit 2B - 100% Load Source: Work Order: 6500411 Date: 12/12/2018 12/12/2018 12/12/2018 M₩g 171.2 169.1 168.0 169.4 Load: 201.0 201.0 201.0 Stack Diameter inches Cross-sectional Area of Stack, A 220.35 220.35 220.35 Source Pollutant Test Data Units Run 1 Run 2 Run 3 Average Barometric Pressure, Pbar inches of Hg 29.10 29.10 29.05 29.08 0,999 0.999 0.999 Dry Gas Meter Calibration Factor, Y dimensionless 0.999 Pitot Tube Coefficient, Cp 0.84 0.84 0.84 0.84 dimensionless Stack Static Pressure, P. inches of H<sub>2</sub>O -1.00 -1.00 -1.00 -1.00Nozzle Diameter, D, 0.219 0.219 0.219 0.219 inches Run Start Time 8:30 11:00 13:25 br:mm Run Stop Time 10:39 13:09 15:33 hr:mm Duration of Sample, θ Dry Gas Meter Leak Rate, L<sub>p</sub> 120 120 120 120 minutes cfm 0.000 0.000 0.000 0.000 ft<sup>3</sup> 761.26 889.10 554.16 Dry Gas Meter Start Volume 12.13 Dry Gas Meter Final Volume ft 888.16 1011.25 135.94 678.45 Average Pressure Difference across the Orifice Meter, ΔH inches of H<sub>2</sub>O 3.48 3,30 3.36 3.38 Average Dry Gas Meter Temperature, Tm 80.8 78.4 73.2 81.3 Average Square Root Velocity Head, v∆p vinches H<sub>2</sub>O 1.4353 1.3837 1.3957 1.4049 Stack Gas Temperature, I<sub>s(abavg)</sub> 227.9 227.8 228.3 229.1 Run 1 Run 2 Run 3 Average Source Moisture Data Volume of Water Vapor Condensed, V<sub>wc(std)</sub> 8.2 7.8 7.5 7.8 scf Volume of Water Vapor Condensed in Silica Gel, Vwg(std) scf 1.4 1.4 1.7 1.5 Total Volume of Water Vapor Condensed, V<sub>w(std)</sub> scf 9.630 9,175 9,185 9 330 Volume of Gas Sample as Measured by the Dry Gas Meter, Vm dcf 126.905 122.150 123.810 124.288 Volume of Gas Sample Measured by the Dry Gas Meter corrected to STP, V<sub>m(std)</sub> dscf 123.128 116.688 118.189 119.335 Volume of Gas Sample Measured by the Dry Gas Meter corrected to STP, Vm(std) 3.487 3,305 3,347 3,380 ldscm Moisture Content of Stack Gas, B % H<sub>2</sub>O 7.25 7.29 7.21 7.25 Gas Analysis Data Run 1 Run 2 Run 3 Average Carbon Dioxide, %CO2 %, dry 4,0 4.1 4.1 4.1 Oxygen, %O<sub>2</sub> 13.8 13.7 %, dry 13.5 13.8 82.1 82.2 Nitrogen, %N %, dry 82.5 82.1 Dry Molecular Weight, MJ lb/ib-mole 29.18 29.21 29.21 29.20 Wet Molecular Weight, M₅ lb/的-mole 28.37 28.39 28.40 28.39 Fuel F-Factor, Fa: dscf/mmBtu 8,710 8,710 8,710 8.710 Run 2 Run 3 Gas Volumetric Flow Rate Data Run 1 Average Average Stack Gas Velocity, v<sub>s</sub> ft/s 94.3 90.8 91.6 92.2 Stack Gas Volumetric Flow Rate, Q acfm 1,246,600 1,200,302 1,211,458 1,219,453 Stack Gas Standard Volumetric Flow Rate, Qs scfm 926,663 893,761 900,623 907,016 Stack Gas Dry Standard Volumetric Flow Rate, Qsd 828,606 835,680 841.243 dscfm 859 442 Percent of Isokinetic Sampling, I % 100.6 98.9 99.3 99.6 Gas Concentrations and Emission Rates Run 3 Run 1 Run 2 Average 0.055 0.047 0.051 0.051 Formaldehyde Concentration ppmvd Formaldehyde Molecular Weighl g/mole 30.031 30.031 30.031 30.031 7.799E-08 7.799E-08 7.799E-08 7.799E-08 Formaldehyde lb/scf Coversion Factor lb/scf Formaldehyde Mass Emission Rate lb/hr 0.22 0.18 0,20 0,20 0.0004 0.0001 0.0001 Formaldehyde Mass Emission Rate lb/mmBtu 0.0001 Formaldehyde Mass Emission Rate [Assumes 8,760 Hrs/Yr Operation] 1.0 0,8 0.9 0,9 tpy ND ND NÐ 0 Acetylene Concentration ppmvd Propane Concentration ppmvd ND ND NÐ 0 ND ND ND 0 Butane Concentration ppmvď NÐ ND ND 0 Propylene Concentration ppmvd ND ND NÐ 0 Acetaldehyde Concentration ppmvd ND ND ND 0 Ethylene Concentration ppmvd ND ND ND 0 Methanol Concentration ppmvd Total VOC Mass Emission Rate 0.18 0.20 0.20 0.22 lb/hr Total VOC Mass Emission Rate lb/mmBtu 0.0001 0.0001 0.0001 0.0001 Total VOC Mass Emission Rate [Assumes 8,760 Hrs/Yr Operation] 0.9 1.0 0.8 0.9 tpy