

Annual RICE MACT Performance Emissions Test Report

Upper Michigan Resources Corporation
F. D. Kuester Generating Station
MI-ROP-P0797-2020
EURICE1, EURICE2, EURICE3, EURICE4, EURICE5,
EURICE6, EURICE7
Negaunee, Michigan
October 24 through 26, 2023

Report Submittal Date December 4, 2023

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Project No. M234004H



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1.0 EXECUTIVE SUMMARY

Mostardi Platt conducted an annual RICE MACT performance formaldehyde emissions test program for Upper Michigan Energy Resources Corporation (UMERC) on October 24 through 26, 2023 at F.D. Kuester Generating Station on the Reciprocating Internal Combustion Engine (EURICE) 1, EURICE2, EURICE3, EURICE4, EURICE5, EURICE6, and EURICE7 Outlet Ducts in Negaunee, Michigan. The purpose of the test program was to meet the ongoing compliance demonstration requirements for emission rates in accordance with Renewable Operating Permit MI-ROP-P0797 and the RICE MACT 40 CFR Part 63 Subpart ZZZZ. This report summarizes the results of the test program and test methods used.

The test locations, test dates, and test parameters are summarized below.

	TEST INFORMATION							
Test Locations	Test Dates	Test Parameters						
EURICE1	October 25, 2023							
EURICE2	October 25, 2023							
EURICE3	October 25, 2023							
EURICE4	October 24, 2023	Formaldehyde (CH ₂ O), Moisture and Oxygen (O ₂)						
EURICE5	October 26, 2023	and Oxygen (O2)						
EURICE6	October 26, 2023							
EURICE7	October 26, 2023							

F. D. Kuester Generating Station electric generation facility includes seven (7) Wärtsilä W18V50SG natural gas-fired, four stroke, lean burn, spark ignition reciprocating internal combustion engines (RICE) coupled to 19,260 kW electric generators, a 1,000-kW natural gas-fired emergency generator, and one natural gas-fired natural gas conditioning heater. The RICE electric generating unit engines utilize pipeline quality natural gas and are equipped with selective catalytic reduction (SCR) for nitrogen oxides (NOx) control and oxidation catalyst systems for carbon monoxide (CO), volatile organic compound (VOC), and organic hazardous air pollutant (HAP) control. Each RICE electric generating unit exhausts into a common stack. Testing was done at the outlet duct to isolate the emissions from each unit.

Selected results of the test program are summarized below on a ppmvd @ 15% O₂ basis. A complete summary of emission test results follows the narrative portion of this report.

TEST RESULTS								
Test Location	Date	Test Parameter	Emission Limit	Emission Rate				
EURICE1	October 25, 2023			1.21 ppmvd @ 15% O ₂				
EURICE2	October 25, 2023			2.00 ppmvd @ 15% O ₂				
EURICE3	October 25, 2023			1.42 ppmvd @ 15% O ₂				
EURICE4	October 24, 2023	Formaldehyde	14 ppmvd @ 15% O ₂	1.28 ppmvd @ 15% O ₂				
EURICE5	October 26, 2023			1.59 ppmvd @ 15% O ₂				
EURICE6	October 26, 2023			1.28 ppmvd @ 15% O ₂				
EURICE7	October 26, 2023			1.41 ppmvd @ 15% O ₂				

Operating Data as provided by the plant is included in Appendix A.

The identifications of the individuals associated with the test program are summarized below.

TEST PERSONNEL INFORMATION						
Location	Address	Contact				
Test Coordinator	WEC Energy Group, Inc 231 W. Michigan Street Milwaukee, Wisconsin 53203	Mr. Justin Kowalski Senior Environmental Consultant 414-221-2265				
Test Facility	Upper Michigan Energy Resources Corporation F.D. Kuester Generating Station 80 Eagle Mills Road Negaunee, MI 49866	justin.kowalski@wecenergygroup.com				
Testing Company Representative	Mostardi Platt 888 Industrial Drive Elmhurst, Illinois 60126	Mr. Jeffrey Gross Project Supervisor (630) 993-2100 (phone) jgross@mp-mail.com				

The test crew consisted of J. Dockins, J. Jimenez, and J. Gross of Mostardi Platt.

2.0 TEST METHODOLOGY

Emission testing was conducted following the methods specified in 40CFR60, Appendix A and 40CFR63, Appendix A. Schematics of the test section diagrams and sampling trains used are included in Appendix B and C, respectively. Calculation nomenclature and example calculations are included in Appendix D. Reference method test data can be found in Appendix E.

The following methodology was used during the test program:

Method 3A Oxygen (O₂)

 $\mathrm{CO_2}$ and $\mathrm{O_2}$ concentrations were measured to determine stack gas molecular weight and emission rates in ppmvd corrected to 15% $\mathrm{O_2}$ in accordance with Method 3A. An Servomex analyzer was used to determine stack gas oxygen. All of the equipment used was calibrated in accordance with the specifications of the Method. Calibration data are presented in Appendix F and copies of gas cylinder certifications are included in Appendix G.

Method 320 Formaldehyde (HCHO) and Moisture (H2O) Determination

The Method 320 sampling and measurement system meets the requirements of US EPA Reference Method 320, "Vapor Phase Organic and Inorganic Emissions by Extractive FTIR," 40CFR63, Appendix A. This method applies to the measurement of combustion gas concentrations. With this method, gas samples are extracted from the sample locations through heated Teflon sample lines to the analyzer.

FTIR technology works on the principle that most gases absorb infrared light. This is true for all compounds with the exception of homonuclear diatomic molecules and noble gases such as: N2, O2, H2, He, Ne, and Ar. Vibrations, stretches, bends, and rotations within the bonds of a molecule determine the infrared absorption distinctiveness. The absorption creates a "fingerprint" which is unique to each given compound.

The quantity of infrared light absorbed is proportional to the gas concentration. Most compounds have absorbencies at different infrared frequencies, allowing the simultaneous analysis of multiple compounds at one time. The FTIR software compares each sample spectrum to a user-selected list of calibration references and performs a classical least squares analysis to determine concentration data on a wet volume basis and the spectral residuals for each analyte (the error associated with each measurement). FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer. The FTIR was equipped with a temperature-controlled, 5.11-meter multi-pass gas cell maintained at 191°C. Gas flows and sampling system pressures were monitored using a rotameter and pressure transducer.

All data was collected at 0.5 cm⁻¹ resolution. Each spectrum was derived from the coaddition of 62 scans, with a new data point generated approximately every one minute. Analyzer data for each run is present is Appendix E.

SAMPLING SYSTEM PARAMETERS							
MKS Serial #	Sampling Line	Probe Assembly	Particulate Filter Media	Operating Temperatures			
111171031	100' 3/8" dia., heated Teflon	Heated 8', 3/8" dia. SS	0.01µ heated borosilicate glass fiber	191°C			

QA/QC procedures followed US EPA Method 320. See below for QA/QC procedure details and list of calibration gas standards. All calibration gases were introduced to the analyzer and the sampling system using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable EPA methodology. See Appendix G for FTIR QA/QC Data and instrument linearity validations.

	F	TIR QA/QC PRO	CEDURES			
QA/QC Specification	Purpose	Calibration Purpose Gas Analyte		Frequency	Acceptance Criteria	Result
M320; Zero	Verify that the FTIR is free of contaminants & zero the FTIR	Nitrogen (zero)	Direct to FTIR	pre/post test	< MDL or Noise	Pass
M320:Calibration Transfer Standard (CTS) Direct	Verify FTIR linearity, confirm optical path length	Ethylene	Direct to FTIR	pretest	+/- 5% cert. value	Pass
M320: CTS Response	linearity recovery		Sampling System	Daily, pre/post test	+/- 5% of Direct Measurement	Pass
M320: Zero Response	-,		Sampling System	pretest	Bias correct data	Pass
M320: Analyte Spike	Verify system ability to deliver and quantify analyte of interest in the presence of effluent gases	Formaldehyde, SF6	Dynamic Addition to Sampling System, 1:10 effluent	Throughout testing – daily	+/- 30% theoretical recovery	Pass

Note: The determined concentrations from direct analyses were used in all system/spike recovery calculations.

The M320 Analyte Direct calibration did not meet the acceptance criteria prior to testing. This occurs due to cylinder stability over time which impacts the tag values as well as corrosion in the regulators which cause a loss of formaldehyde. Consequently, the determined concentration from the direct analysis was used in all system/spike recovery calculations. Performing all of the other health /QA checks of the FTIR showed the instrument working as well as reading the formaldehyde direct properly which validates the data and does not impact the compliance determination.

CALIBRATION GAS STANDARDS							
Components	Concentration (ppm)	Vendor	Cylinder #	Standard Type			
Ethylene	99.97	Airgas	EB0153619	Certified Standard-Spec +/- 2			
Formaldehyde/ SF6	8.705/5.075	Airgas	EB0146284	Certified Standard +/- 2% (Acetaldehyde/Methanol) Certified Standard +/- 5% (SF ₆)			
Nitrogen	Zero Gas	Airgas	N/A	UHP Grade			

Analyte Spiking

Formaldehyde spiking was performed prior to testing to verify the ability of the sampling system to quantitatively deliver a sample containing formaldehyde from the base of the probe to the FTIR. Analyte spiking assures the ability of the FTIR sampling system to recover volatile organics in the presence of effluent gas.

As part of the spiking procedure, samples were measured to determine native formaldehyde concentration to be used in the spike recovery calculations. The analyte spiking gases contained a low concentration of sulfur hexafluoride (SF₆). The determined SF₆ concentration in the spiked sample was used to calculate the dilution factor of the spike and thus used to calculate the concentration of the spiked formaldehyde. The spike target dilution ratio was 1:10 or less.

The following equation illustrates the percent recovery calculation.

$$DF = \frac{SF6(spk)}{SF6(direct)}$$
 (Sec. 9.2.3 (3) USEPA Method 320)

$$CS = DF * Spike(dir) + Unspike(1 - DF)$$
 (Sec. 9.2.3 (4) USEPA Method 320)

DF = Dilution factor of the spike gas

SF_{6(dir)} = SF₆ concentration measured directly in undiluted spike gas

SF_{6(spk)} = Diluted SF₆ concentration measured in a spiked sample

Spikedir = Concentration of the analyte in the spike standard measure by the FTIR directly

CS = Expected concentration of the spiked samples

Unspike = Native concentration of analytes in unspiked samples

Post Collection Data Validation

As part of the data validation procedure, reference spectra are manually fit to that of the sample spectra and a concentration is determined. The reference spectra are scaled to match the peak amplitude of the sample, providing a scaling factor. The scaling factor multiplied by the reference spectra concentration is used to determine the concentration value for the sample spectra. Sample pressure and temperature corrections are then applied to compute the final sample concentration. The manually calculated results are then compared with the software-generated results. The data is then validated if the two concentrations are within ± 20% agreement. In some cases, the percent difference between the two analyses is relatively large, but the absolute concentration difference is minimal. If this is not determined to be the case, then the spectra are reviewed for possible spectral interferences or any other possible causes leading to incorrectly quantified data. See Appendix G FTIR QAQC for manual subtractions.

Detection Limit

The detection limit of each analyte was calculated following Annex A2 of ASTM D6348-12 procedure using spectra that contained similar amounts of moisture and carbon dioxide.

Analyte	Detection Limit (ppmv wet)	Detection Limit (%v)
Formaldehyde	0.4	
Moisture		0.1

The spectral residuals for each compound is calculated using the classical least squares analysis. When the residual error exceeds the measured concentration, the compound is considered a non-detect, allowing the residual to verify the detection limit. The spectral residual also permits the analyst to determine if there are possible interferences in the sample matrix.

QA/QC data are found in Appendix G. Copies of gas cylinder certifications are found in Appendix H. All concentration data were recorded on a wet, volume basis. The sample and data collection followed the procedures outlined in Method 320.

3.0 TEST RESULT SUMMARIES

Upper Michigan Energy Resources Corporation F. D. Kuester Generating Facility EURICE 1 Outlet Duct Formaldehyde Summary

Test No.	Date	Start Time	End Time	O ₂ % (dry)	Moisture, %	CH2O ppmvw	CH2O ppmvd	CH2O ppmvd @ 15% O2
1	10/25/23	16:46	17:53	11.5	10.08	1.81	2.01	1.26
2	10/25/23	18:09	19:08	11.5	10.05	1.70	1.89	1.19
3	10/25/23	19:24	20:23	11.5	10.06	1.67	1.86	1.17
Average			11.5	10.06	1.73	1.92	1.21	

Upper Michigan Energy Resources Corporation F. D. Kuester Generating Facility EURICE 2 Outlet Duct Formaldehyde Summary

Test No.	Date	Start Time	End Time	O ₂ % (dry)	Moisture, %	CH2O ppmvw	CH2O ppmvd	CH2O ppmvd @ 15% O2
1	10/25/23	12:21	13:29	11.9	9.76	2.72	3.01	1.96
2	10/25/23	13:44	14:43	11.9	9.76	2.82	3.13	2.04
3	10/25/23	14:59	15:58	11.9	9.77	2.75	3.05	1.99
Average			11.9	9.76	2.76	3.06	2.00	

Upper Michigan Energy Resources Corporation F. D. Kuester Generating Facility EURICE 3 Outlet Duct Formaldehyde Summary

Test No.	Date	Start Time	End Time	O ₂ % (dry)	Moisture, %	CH2O ppmvw	CH2O ppmvd	CH2O ppmvd @ 15% O2
1	10/25/23	7:28	8:38	11.5	10.19	2.05	2.29	1.43
2	10/25/23	8:54	9:53	11.5	10.15	2.06	2.29	1.43
3	10/25/23	10:10	11:09	11.5	10.14	1.98	2.21	1.38
	Average			11.5	10.16	2.03	2.26	1.42

Upper Michigan Energy Resources Corporation F. D. Kuester Generating Facility EURICE 4 Outlet Duct Formaldehyde Summary

Test No.	Date	Start Time	End Time	O ₂ % (wet)	Moisture, %	O ₂ % (dry)	CH2O ppmvw	CH2O ppmvd	CH2O ppmvd @ 15% O2
1	10/24/23	10:25	11:24	10.1	10.40	11.30	2.47	2.75	1.69
2	10/24/23	13:05	14:04	10.2	10.49	11.35	1.53	1.71	1.06
3	10/24/23	17:06	18:05	10.1	10.74	11.33	1.56	1.75	1.08
	Aver	age		10.1	10.54	11.33	1.85	2.07	1.28

Upper Michigan Energy Resources Corporation F. D. Kuester Generating Facility EURICE 5 Outlet Duct Formaldehyde Summary

Test No.	Date	Start Time	End Time	O₂ % (dry)	Moisture, %	CH2O ppmvw	CH2O ppmvd	CH2O ppmvd @ 15% O2
1	10/26/23	7:40	8:49	11.6	9.95	2.23	2.47	1.57
2	10/26/23	9:02	10:01	11.6	9.96	2.28	2.53	1.61
3	10/26/23	10:17	11:16	11.6	10.03	2.24	2.49	1.58
	Aver	age		11.6	9.98	2.25	2.50	1.59

Upper Michigan Energy Resources Corporation F. D. Kuester Generating Facility EURICE 6 Outlet Duct Formaldehyde Summary

Test No.	Date	Start Time	End Time	O ₂ % (dry)	Moisture, %	CH2O ppmvw	CH2O ppmvd	CH2O ppmvd @ 15% O2
1	10/26/23	11:58	13:06	11.6	10.09	2.08	2.31	1.47
2	10/26/23	13:21	14:20	11.6	10.26	1.75	1.95	1.23
3	10/26/23	14:35	15:34	11.5	10.33	1.62	1.81	1.14
	Aver	age		11.6	10.23	1.82	2.02	1.28

Upper Michigan Energy Resources Corporation F. D. Kuester Generating Facility EURICE 7 Outlet Duct Formaldehyde Summary

Test No.	Date	Start Time	End Time	O₂ % (dry)	Moisture, %	CH2O ppmvw	CH2O ppmvd	CH2O ppmvd @ 15% O2
1	10/26/23	16:13	17:19	11.6	10.28	2.05	2.28	1.45
2	10/26/23	17:33	18:32	11.6	10.28	1.96	2.18	1.39
3	10/26/23	18:46	19:45	11.6	10.27	1.96	2.18	1.39
	Aver	age		11.6	10.28	1.99	2.22	1.41

4.0 CERTIFICATION

Mostardi Platt is pleased to have been of service to Upper Michigan Energy Resources Corporation. If you have any questions regarding this test report, please do not hesitate to contact us at 630-993-2100.

As project manager, I hereby certify that this test report represents a true and accurate summary of emissions test results and the methodologies employed to obtain those results, and the test program was performed in accordance with the methods specified in this test report.

MOSTARDI PLATT

Jeffrey M. Gross

Program Manager

Quality Assurance

Scott W Banach

APPENDICES

Appendix A - Plant Operating Data

F.D. Kuester Generating Station Performance Emissions Testing 40 CFR Part 60 Subpart JJJJ & 63 Subpart ZZZZ (MACT) October 24 through 26, 2023

EURICE1				
10/25/2023 Start Time	1646	1809	1924	
End Time	1646 1809 1924 1753 1908 2023 Run 1 Run 2 Run 3 18,900 18,890 18,879 6,786 6,782 6,780			
	Run 1	Run 2	Run 3	Average
Engine (kW)	18,900	18,890	18,879	18,890
Engine natural gas use (pound/hour)	6,786	6,782	6,780	6,783
SCR/Oxidation catalyst inlet temperature) (deg F)	720	719	719	719
Pressure drop across the oxidation catalyst (PSI)	0.15	0.15	0.15	0.15
Urea injection rate to the SCR (gallons/hour)	6.5	6.4	6.6	6.5

EURICE2 10/25/2023				
Start Time	1221	1344	1459	
End Time	1329	1443	1558	
	Run 1	Run 2	Run 3	Average
Engine (kW)	18,872	18,875	18,867	18,871
Engine natural gas use (pound/hour)	6,735	6,743	6,748	6,742
SCR/Oxidation catalyst inlet temperature) (deg F)	690	689	689	689
Pressure drop across the oxidation catalyst (PSI)	0.14	0.14	0.14	0.14
Urea injection rate to the SCR (gallons/hour)	3.4	3.3	3.4	4.7

EURICE3				
10/25/2023				
Start Time	728	854	1010	
End Time	838	953	1109	
	Run 1	Run 2	Run 3	Average
Engine (kW)	18,872	18,778	18,880	18,843
Engine natural gas use (pound/hour)	6,762	6,758	6,753	6,758
SCR/Oxidation catalyst inlet temperature) (deg F)	716	717	718	717
Pressure drop across the oxidation catalyst (PSI)	0.22	0.20	0.21	0.21
Urea injection rate to the SCR (gallons/hour)	5.8	5.8	6.0	5.9

EURICE4				
10/24/2023				
Start Time	1025	1305	1706	
End Time	1124	1404	1805	
	Run 1	Run 2	Run 3	Average
Engine (kW)	18,875	18,862	18,877	18,871
Engine natural gas use (pound/hour)	6,647	6,689	6,675	6,670
SCR/Oxidation catalyst inlet temperature) (deg F)	727	724	725	725
Pressure drop across the oxidation catalyst (PSI)	0.18	0.18	0.18	0.18
Urea injection rate to the SCR (gallons/hour)	7.7	6.6	6.2	6.9

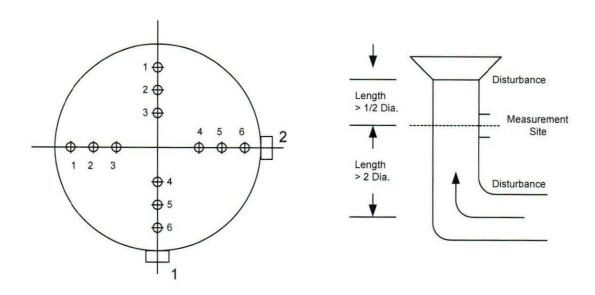
EURICE5				
10/26/2023				
Start Time	740	902	1017	
End Time	849	1001	1116	
	Run 1	Run 2	Run 3	Average
Engine (kW)	18,908	18,913	18,923	18,915
Engine natural gas use (pound/hour)	6,757	6,757	6,752	6,755
SCR/Oxidation catalyst inlet temperature) (deg F)	702	702	703	702
Pressure drop across the oxidation catalyst (PSI)	0.14	0.14	0.14	0.14
Urea injection rate to the SCR (gallons/hour)	4.2	4.1	4.1	4.1

EURICE6				
10/26/2023				
Start Time	1158	1321	1435	
End Time	1306	1420	1435 1534 Run 3 18,950 6,670 714 0.14	
	Run 1	Run 2	Run 3	Average
Engine (kW)	18,934	18,952	18,950	18,945
Engine natural gas use (pound/hour)	6,812	6,708	6,670	6,730
SCR/Oxidation catalyst inlet temperature) (deg F)	707	712	714	711
Pressure drop across the oxidation catalyst (PSI)	0.14	0.14	0.14	0.14
Urea injection rate to the SCR (gallons/hour)	4.2	4.7	4.8	4.6

EURICE7				
10/26/2023				
Start Time	1613	1733	1846	
End Time	1719	1832	1945	
	Run 1	Run 2	Run 3	Average
Engine (kW)	18,910	18,907	18,897	18,905
Engine natural gas use (pound/hour)	6,551	6,548	6,536	6,545
SCR/Oxidation catalyst inlet temperature) (deg F)	709	710	710	710
Pressure drop across the oxidation catalyst (PSI)	0.21	0.21	0.21	0.21
Urea injection rate to the SCR (gallons/hour)	4.2	4.3	4.3	4.3

Appendix B - Test Section Diagram

STRATIFICATION TRAVERSE FOR ROUND DUCTS



Job: Upper Michigan Energy Resources Corporation

F.D. Kuester Generating Station

Date: October 24-26, 2023

Test Locations: EURICE1, EURICE2, EURICE3, EURICE4, EURICE5, EURICE6, and

EURICE7 Outlet Ducts (identical)

Duct Diameter: 5.29 Feet

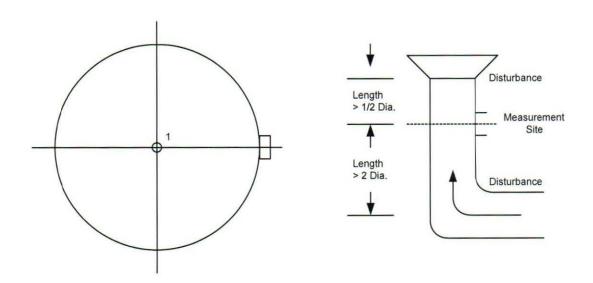
Duct Area: 21.98 Square Feet

No. Points Across Diameter: 6

No. of Ports: 2

Port Length: 8.0 Inches

GASEOUS TRAVERSE FOR ROUND DUCTS



Job: Upper Michigan Energy Resources Corporation

F.D. Kuester Generating Station

Date: October 24-26, 2023

Test Location: EURICE1, EURICE2, EURICE3, EURICE4, EURICE5, EURICE6, and

EURICE7 Outlet Ducts (identical)

Duct Diameter: 5.29 Feet

Duct Area: 21.98 Square Feet

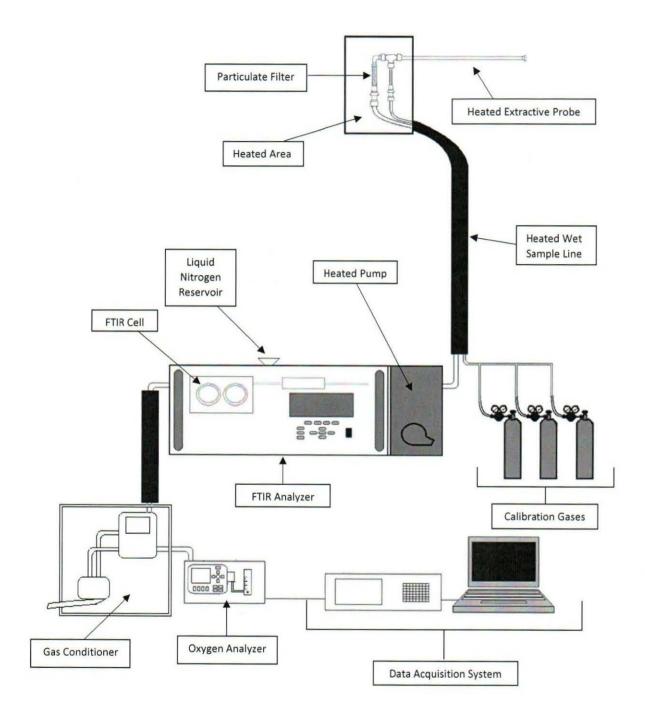
No. Points Across Diameter: 1

No. of Ports: 1

Port Length: 8.0 Inches

Appendix C - Sample Train Diagram

USEPA Methods 3A and 320 - Sample Train Diagram



ATD-081A USEPA Method 3/320

Rev. 0.0

4/9/2020

Appendix D - Calculation Nomenclature and Formulas

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