## **1.0 INTRODUCTION**

## **1.1** Identification, location and dates of tests

Erthwrks, Inc. was contracted to conduct the emissions performance test the NHT Stripper in operation at the Marathon Detroit Refinery, located in Detroit, Michigan. The performance test was conducted on April 21, 2021.

## **1.2 Purpose of Testing**

This test program was conducted to determine the nitric oxide (NO<sub>X</sub>) emissions emitted from the NHT Stripper. All testing and audit procedures were conducted in accordance with the requirements set forth in the USEPA Title 40, Code of Federal Regulations (CFR), Part 60, Appendix B which defines the testing procedures.

## **1.3 Description of Source**

The NHT Stripper Reboiler (EU16-NHTSTRIPREBOIL-S1) heats the liquid from the bottom of the Naphtha Hydrotreater stripper column. The vapors that form are returned to the top of the stripper column; the liquid vapor is removed as a product stream. The unit is fired by refinery fuel gas. Emissions are vented to the atmosphere via the NHT Stripper Reboiler Heater Stack where testing was performed.

## **1.4** Contact Information

## Marathon Petroleum Company LP

Aamani Kura Environmental Professional Michigan Refining Division O: (313)551-7963 | C: (734)899-7343 AaKura@marathonpetroleum.com

## Erthwrks, Inc.

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## 2.0 SUMMARY OF RESULTS

Table 2.1: NHT Stripper Emissions Results								
Pollutant Measured	Mass Emission Rate	Applicable Limit	Pass/Fail					
NOx	0.118 lb/MMBtu	0.20 lb/MMBtu	Pass					

 Table 2.1: NHT Stripper Emissions Results

# **3.0 SOURCE DESCRIPTION**

## **3.1 Description of the process**

The Naphtha Hydrotreater unit uses hydrogen to remove sulfur and nitrogen from straightrun and coker naphthas. This process, known as hydrotreating, uses a catalyst to promote the desulfurization reaction. The desulfurized or sweet naphtha is blended into gasoline or used for platformer feed. The NHT unit consists of process vessels (including exchangers, reactors, receivers, separators, and a stripper column), heaters, tanks, containers, pumps, piping, drains, and various components (pump seals, process valves, pressure relief valves, flanges, connectors, etc.).

The NHT Stripper Reboiler (EU16-NHTSTRIPREBOIL-S1) heats the liquid from the bottom of the stripper column. The vapors that form are returned to the top of the stripper column; the liquid vapor is removed as a product stream.

## 3.2 Applicable permit and source designation

The Marathon Detroit Refinery operates the NHT Stripper under the Permit No. MI-ROP-A9831-2012c. The NHT Stripper is also identified as EU16-NHTSTRIPREBOILS1. Under this permit, the Marathon Detroit Refinery is required to conduct an annual compliance test to demonstrate the NO<sub>X</sub> emissions remain below the applicable limit.

## **3.3** Type and quantity of materials processed during tests

During the emission testing on April 21, 2021, at the Marathon Detroit Refinery, the NHT Stripper was tested at the highest achievable rate. The actual load conditions during the testing were documented by facility personnel and are summarized in Appendix A. Raw data records are provided in Appendix F.



## 4.0 SAMPLING AND ANALYTICAL PROCEDURES

## 4.1 Description of sampling and field procedures

Erthwrks completed this compliance test utilizing all applicable test methods specified in the USEPA Title 40 CFR Part 60, Appendix A. EPA Method 3A was used to determine the O<sub>2</sub> concentration and EPA Method 7E was used to determine the NO<sub>x</sub> concentration.

All gaseous sampling was done utilizing three appropriate traverse points. The three traverse points were selected to ensure acquisition of a representative sample over the stack cross section.

## 4.2 Quality Assurance Procedures

As required by EPA Methods 3A and 10, Erthwrks followed all quality assurance and quality control procedures as defined in US EPA 40 CFR 60 Appendix A, Method 7E for the determination of the concentrations of CO and O<sub>2</sub>.

The Calibration Error (CE) Test was conducted as specified in EPA Method 7E §8.2.3. In accordance with this requirement, a three-point analyzer calibration error test was conducted prior to sampling. The CE test was conducted by introducing the low, mid, and high level calibration gasses (as defined in EPA Method 7E §3.3.1-3) sequentially and the response was recorded. The results of the CE test are acceptable if the calculated calibration error is within  $\pm 2.0\%$  of calibration span (or  $\le 0.5$  ppmv).

The NO<sub>2</sub>-NO Conversion Efficiency Test was conducted prior to each field test in accordance with EPA Method 7E §8.2.4.1. This was conducted by introducing the converter efficiency gas (~50 ppm NO<sub>2</sub>) directly to the NOx analyzer and recording the NO value. The NO<sub>2</sub>-NO Conversion Efficiency test was within acceptable limits.

A Stratification Test was conducted at the beginning of the test as described in EPA Method 7E §8.1.2. Three points at 16.7%, 50%, and 83.3% of the stack diameter was used as the traverse line. The highest emitted pollutant was measured at each point for a period of at least twice the sample system response time. The concentration at each point was compared to the average concentration. The exhaust gas stream was considered unstratified because the variance at each point was <5.0% from the average, and the sample was taken the centroid of the stack.

The Initial System Bias and System Calibration Error Check was conducted in accordance with EPA Method 7E §8.2.5. The upscale calibration gas was introduced at the probe upstream of all sample system components and the response was recorded. The procedure was repeated with the low-level gas and the response was recorded. The sample system response time was also recorded. This specification is acceptable if the calculated values of the system calibration error check are within  $\pm 5.0\%$  of the calibration span value (or  $\leq 0.5$  ppmv).





8681.1.B1 Marathon Detroit NHT Stripper (Reboiler) Test Repor JUN 12 92 2021 Version 1 (5/18/21) After each compliance test run, the sample system bias check was conducted to validate the run data. The low-level and upscale drift was calculated using Equation 7E-4. The run data was deemed valid if the calculated drift is within  $\pm 3.0\%$  of the calibration span value (or  $\leq 0.5$  ppmv).

Each test run, the effluent gas concentration was calculated as specified in EPA Method 7E §12.6. The arithmetic average of all valid concentration values was adjusted for bias using Equation 7E-5B.

EPA Method 19 was used for the calculation of the mass emission rates. In accordance with this method, the volumes of combustion components per unit of heat content ( $F_d$ ) was calculated using the comprehensive fuel analysis (Eq. 19-13). Utilizing this "F-Factor", the emission rates were calculated using Equation 19-1. The fuel analysis worksheets are found in Appendix C and the example calculations are found in Appendix E.

## 4.3 Discussion of sampling procedure or operational variances

Erthwrks, Inc. conducted the emission testing with no sampling or procedural variances. The NHT Stripper tested, operated with no operational variances.



# Attachment A Detailed Results of Emission Test

# **Erthwrks Summary of Results**

Date:	4/21/2021
Client:	Marathon
Facility:	Detroit
Unit ID:	NHT Stripper
Erthwrks Tech:	JW, JT, JM

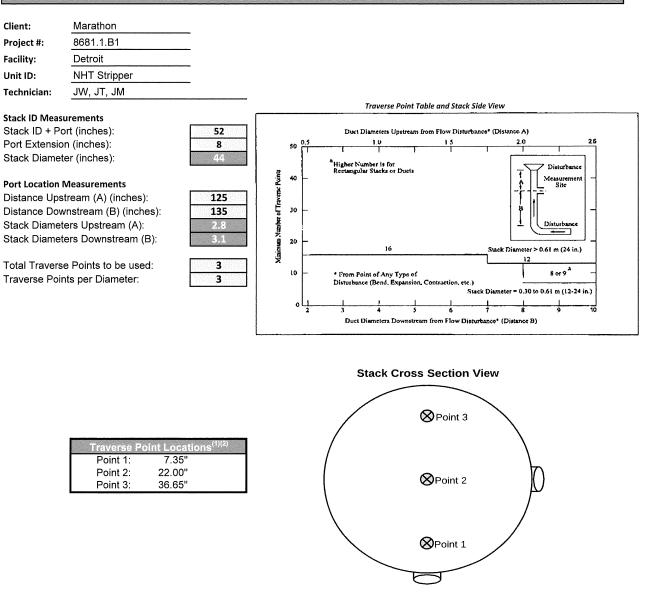
Run Information								
Run Number	Run 1	Run 2	Run 3					
Date	4/21/2021	4/21/2021	4/21/2021					
Run Start Time	8:49	9:57	11:05					
Run End Time	9:49	10:57	12:05					
Operating Conditions								
Unit Charge Rate	47341.1	46778.0	44467.3					
MSCF/D fuel gas	798.3	801.7	733.3					
NHT reboiler duty	33.7	33.4	32.2					
Unit Fuel Flow Data								
Fuel F Factor (F <sub>d</sub> ) (scf/MMBtu)	8586.3	8586.3	8586.3					
Emission Concentrations								
NOx (ppmv)	82.68	85.97	85.55					
O <sub>2</sub> (%)	5.44	5.50	5.53					
Emission Concentrations O2 Co	prrected	Corrected To:	0 %O2					
NOx (ppmv @ %O <sub>2</sub> )	111.76	116.65	116.30					
Emission Rates (Ib/scf)								
NOx (lb/scf)	9.87E-06	1.03E-05	1.02E-05					
Emission Rates (Ib/MMBtu)								
NOx (lb/MMBtu)	0.1146	0.1196	0.1192					

Average 114.90 ppmv

Average 0.1178 lb/MMBtu

# Attachment B Quality Control Documentation

## Erthwrks Method 1 Traverse Point Location Worksheet



<sup>(1)</sup>For stack diameter >4.0" and <2.4 meters, stratification is measured at 16.7%, 50.0%, and 83.3" of stack diameter (M7E, §8.1.2). <sup>(2)</sup> For stack diameter >2.4 meters, stratification is measured at 0.4, 1.2, and 2.0 meters from stack wall (M7E, §8.1.2).

## Erthwrks Gaseous Sample Collection and Quality Assurance Worksheet

Date:	4/21/2021
Client:	Marathon
Facility:	Detroit
Unit ID:	NHT Stripper
Erthwrks Tech:	JW, JT, JM

### **Calibration Gas Verification**

Pollutant	Low-Level Gas Conc. (CV)	Cylinder Serial #	Mid-Level Gas Conc. (CV)	Cylinder Serial #	High-Level Gas Conc. (CV/CS)	Cylinder Serial #	Diluter Root Gas
NOx	NA	NA	50.28	ALM049993	95.02	XC036040B	NA
O2	NA	NA	12.25	CC235646	20.59	EB0013408	NA

Reference	Method	Analyzer	Info

Make	Model	Serial No.
Teledyne	T200H	600
Teledyne	T200H	600

### **Direct Calibration Error Test**

Pollutant	Zero Gas Response (C <sub>Dir</sub> )	Calibration Error (ACE)*	Low-Level Response (C <sub>pir</sub> )	Calibration Error (ACE)*	Mid-Level Response (C <sub>oir</sub> )	Calibration Error (ACE)*	High-Level Response (C <sub>oir</sub> )	Calibration Error (ACE)*
NOx	-0.19	-0.19%	NA	NA	49.70	-0.61%	94.76	-0.28%
02	-0.03	-0.14%	NA	NA	12.30	0.23%	20.61	0.10%
' ACE must either be w	ithin ± 2.0% or ≤ 0.5 ppr	v adsolute difference						

#### Tool 20

Conversion Efficiency Test				Traverse Point	5		No	x Stratification 1	Test
NO <sub>2</sub> Cal Gas Concentration	60.93	Stack ID		% of Stack	inches from ID	inch port ext	Point 1	79.131	0.60%
NO <sub>2</sub> Cal Gas Cyl. Number	CC506641	44	Point 1	16.7%	7.35	15.35	Point 2	79.993	-0.48%
NOx Analyzer Response	59.21	Port Extension	Point 2	50.0%	22.00	30.00	Point 3	79.703	-0.12%
NO2-NO Conv. Efficiency (Eff <sub>NO2</sub> )*	97.18%	8	Point 3	83.3%	36.65	44.65	Average	79.609	
<ul> <li>Eff<sub>NO2</sub> must be ≥ 90%</li> </ul>							*Stratification Test resul	s must be <5%	

### Initial Sample System Bias and Response Time

Pollutant		Upscale Gas Direct (C <sub>Dir</sub> )	Upscale Response (C <sub>s</sub> )		Response Time (sec)	Downscale Response (C <sub>s</sub> )		Response Time (sec)
NOx	50.28	49.70	48.60	-1.16%	45	-0.32	-0.14%	45
	00.20	40.70						
02	12.25	12.30	12.39	0.43%	45	0.11	0.67%	45

### Sample Collection Raw Data--Pre and Post Sample System Calibration (SSC) and Raw Run Results

	Run #: Slart Time: End Time:		Run 1 8:49 9:49			
Pollutant	Initial Zero SSC	Initial Upscale	Raw Results	Final Zero SSC	Final Upscale	
	(C <sub>S/</sub> )	SSC (C <sub>SI</sub> )	(C <sub>Ave</sub> )	(C <sub>sr</sub> )	SSC (C <sub>Sr</sub> )	
NOx	-0.32	48.60	79.98	-0.11	48.50	
O2	0.11	12.39	5.49	0.05	12.15	

	Run #: Start Time: End Time:	Run 2 9:57 10:57		
Initial Zero SSC	Initial Upscale	Raw Results	Final Zero	Final Upscale
(C <sub>si</sub> )	SSC (C <sub>S/</sub> )	(C <sub>Avg</sub> )	SSC (C <sub>st</sub> )	SSC (C <sub>s/</sub> )
-0.11	48.50	82.45	-0.06	47.88
0.05	12.15	5.48	0.05	12.15

Sample Collection Raw Data--Pre and Post Sample System Calibration (SSC) and Raw Run Results

		Run #: Start Time: End Time:	Run 3 11:05 12:05		
Pollutant	Initial Zero SSC	Initial Upscale	Raw Results	Final Zero SSC	Final Upscale
	(C <sub>Sr</sub> )	SSC (C <sub>s/</sub> )	(C <sub>Avg</sub> )	(C <sub>sr</sub> )	SSC (C <sub>sr</sub> )
NOx	-0.06	47.88	81.72	0.08	48.19
O2	0.05	12.15	5.54	0.08	12.26

#### Run 1 Sample Collection Calculations--Pre- and Post-Run Sample System Bias Check, Drift Assessment, Corrected Results

Pollutant	Initial Zero Sys. Bias (SB)*	Initial Upscale Sys. Bias (SB)*	Final Zero Sys. Bias (SB)*	Final Upscale Sys. Blas (SB)*	Avg, Zero Sys. Bias (C <sub>0</sub> )	Avg. Upscale Sys. Bias (C <sub>M</sub> )	Zero Drift Assessment (D) <sup>†</sup>	Upscale Drift Assessment (D) <sup>†</sup>	Corrected Results (C <sub>gas</sub> )
NOx	-0.14%	-1.16%	0.08%	-1.26%	-0.22	48.55	0.22%	0.11%	82.68
02	0.67%	0.43%	0.35%	-0.69%	0.08	12.27	0.31%	1.13%	5.44

\* SB must either be within ± 5.0% or ≤ 0.5 ppmv adsolute difference † D must either be within ± 3.0% or the pre- and post-run bias responses are ≤ 0.5 ppmv adsolute difference

#### Sample Collection Calculations--Pre- and Post-Run Sample System Bias Check, Drift Assessment, Corrected Results Run 2

NOx 0.08% -1.26% 0.13% -1.92% -0.09 48.19 0.05% 0.66% 85.97	Pollutant	Initial Zero Sys. Bias (SB)*	Initial Upscale Sys. Bias (SB)*	Final Zero Sys. Bias (SB)*	Final Upscale Sys. Bias (SB)*	Avg. Zero Sys. Bias (C <sub>o</sub> )	Avg. Upscale Sys. Bias (C <sub>M</sub> )	Zero Drift Assessment (D) <sup>†</sup>	Upscale Drift Assessment (D) <sup>†</sup>	Corrected Results (C <sub>gas</sub> )
	NOx	0.08%	-1.26%	0.13%	-1.92%	-0.09	48.19	0.05%	0.66%	85.97
	02	0.35%	-0.69%	0.35%	-0.70%	0.05	12.15	0.00%	0.00%	5.50

\*SB must either be within ± 5.0% or ≤ 0.5 ppmv adsolute difference † D must either be within ± 3.0% or the pre- and post-run bias responses are ≤ 0.5 ppmv adsolute difference

#### Run 3 Sample Collection Calculations--Pre- and Post-Run Sample System Bias Check, Drift Assessment, Corrected Results

Pollutant	Initial Zero Sys. Bias (SB)*	Initial Upscale Sys. Blas (SB)*	Final Zero Sys. Bias (SB)*	Final Upscale Sys. Blas (SB)*	Avg. Zero Sys. Bias (C <sub>o</sub> )	Avg. Upscale Sys. Blas (C <sub>M</sub> )	Zero Drift Assessment (D) <sup>†</sup>	Upscale Drift Assessment (D)	Corrected Results (C <sub>gas</sub> )
NOx	0.13%	-1.92%	0.27%	-1.59%	0.01	48.03	0.15%	0.33%	85.55
02	0.35%	-0.70%	0.51%	-0.20%	0.06	12.20	0.15%	0.50%	5.53

\* SB must either be within ± 5.0% or ≤ 0.5 ppmv adsolute difference † D must either be within ± 3.0% or the pre- and post-run bias responses are ≤ 0.5 ppmv adsolute difference



JUN 17 2021



# Erthwrks LLOCHR 400 HAR AT BADI VISION Version 1.4 (Rev. 10/22/2020)